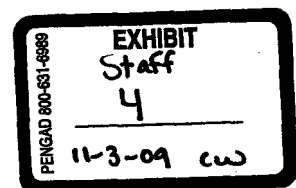


BEFORE THE
PUBLIC UTILITIES COMMISSION
STATE OF SOUTH DAKOTA

KEYSTONE XL PROJECT
DOCKET HP09-001

PREFILED TESTIMONY OF JAMES ARNDT
ON BEHALF OF THE COMMISSION STAFF
SEPTEMBER 2009



BEFORE THE SOUTH DAKOTA PUBLIC UTILITIES COMMISSION

DIRECT TESTIMONY OF JAMES ARNDT

Q: Please state your name and business address.

A: James Arndt, Ph.D., Natural Resource Group, LLC (NRG), 1000 IDS Center, 80 South 8th Street, Minneapolis, MN, 55402.

Q: Describe your educational background.

A: I received my Bachelor of Science Degree in 1980 from the University of Wisconsin – Stevens Point with Majors in Soil Science and Natural Resources Management. I then received my Masters of Science and Doctorate degrees in Soil Science from North Dakota State University in 1987 and 1995, respectively. My educational and research specialties are in soil interpretations, soil pedology and survey, wetland soils, and soil chemistry, physics, and hydrology.

Q: By whom are you now employed?

A: I have been employed by Natural Resource Group, LLC since 2005. I currently hold the position of Senior Consultant.

Q: What work experience have you had that is relevant to your involvement on this project?

A: From 2005 to present, my responsibilities have been to provide NRG clients in the pipeline industry with environmental permitting services, including the preparation of Environmental Assessments and Environmental Impact Statements (EISs) (under the National Environmental Policy Act and/or relevant state programs), and preparation of permit applications under Sections 404 and 401 of the Clean Water Act. I also provide environmental survey and technical support involving the characterization and interpretation of land-use, soils, agricultural issues, wetlands, and hydrologic features along pipeline construction rights-of-way. From 1995 to 2005 I was Vice President of Peterson Environmental Consulting, Inc. I was in direct charge of performing natural

resource assessments along pipeline rights-of-way in the upper Midwest. As a preferred sub-contractor to the U.S. Army Corps of Engineers I provided wetlands and soils support for several large EISs including an assessment of soil salinization hazards associated with the proposed outlet to control flooding in Devils Lake, North Dakota. From 1980 to 1995 I worked in various capacities for North Dakota State University Department of Soil Science. My duties included the collection, processing, evaluation and interpretation of soil and water data. I attended and assisted in Natural Resources Conservation Service (NRCS) field reviews of county soil surveys, collected typifying soil profile descriptions, and soil correlation samples for characterization and presentation in interpretative tables in county soil surveys. As Supervisor of the department's Soils and Water Environmental Laboratory, I provided assistance to private individuals requiring information on soil-water compatibility and interpretation of water and soil analyses from locations throughout the state. A copy of my resume is appended to this testimony as Attachment 1.

Q: What Professional Credentials do you hold?

A: I am certified as a Professional Soil Classifier in the State of North Dakota, and licensed as a Professional Soil Scientist in Minnesota and Wisconsin.

Q. On whose behalf was this testimony prepared?

A. This testimony was prepared on behalf of the Staff of the South Dakota Public Utilities Commission (Staff).

Q: What is the purpose of your testimony?

A: I evaluated the Soils section and the Erosion and Sedimentation section (Sections 5.3.4 and 5.3.5, respectively) of the TransCanada Keystone, LP (Keystone) application to the South Dakota Public Utilities Commission (PUC) for a permit to construct the Keystone XL Project under the Energy Conversion and Transmission Facility Act to determine

whether a sufficient level of detail was provided to characterize the soils in the construction area and assess soil-related limitations and potential hazards associated with pipeline construction consistent with SDAR 20:10:22:13 and 22:10:22:14. I also evaluated portions of Keystone's Construction, Mitigation, and Reclamation Plan (CMRP) to determine whether important soil limitations identified in the application are addressed such that areas affected by construction-related activities would be restored to pre-construction conditions within a reasonable timeframe.

Q: What methodology did you employ?

A: I evaluated Sections 5.3.4 (Soils) and 5.3.5 (Erosion and Sedimentation) of Keystone's application by comparing the information provided in these sections to information typically provided in similar industry-standard applications for federal permits and state permits in the upper Midwest, and in various project-specific construction mitigation plans consistent with the applicable requirements in the appropriate sections of the SDAR. I also utilized my regional knowledge of soil characteristics, soil limitations, soil quality, and land use applicable to the characteristic environment in the Dakotas to assess whether important soil features affected by and affecting pipeline construction were characterized in the application and addressed in appropriate sections of the CMRP. Additionally, I reviewed Keystone's responses to PUC staff's data requests in which Keystone provided additional explanation and information. Keystone's responses to questions and data requests that were not in the original application or revised application but are, in my opinion, a necessary part of the application record and/or should be incorporated into the CMRP are identified and discussed in my testimony.

Q: With respect to soils and erosion/sedimentation information what is your understanding of how South Dakota Rules apply to the information provided in the Application?

A: The following two sub-parts of SDAR 20:10:22 apply directly:

SDAR 20:10:22:13 (Environmental Information) requires that an applicant provide (1) a description of the existing environment at the time of application, (2) estimates of anticipated changes in the environment as a result of construction and operation, and (3) identify potentially irreversible changes in the existing environment. Information should be supplied with sufficient detail to reveal and assess demonstrated or suspected hazards to the health and welfare of human, plant, and animal communities.

SDAR 20:10:22:14(5) (Effect of the Physical Environment) requires a description of the soil type, and SDAR 20:10:22:14(6) requires an analysis of potential erosion or sedimentation that may result from construction and operations and measures that will be taken for their control. An evaluation of applicable components of Keystone's CMRP is assumed to be covered under this rule as well.

Q: With respect to soils and erosion/sedimentation information, what are the commonly accepted industry standards for characterizing the resource and assessing potential project-related impacts?

A: The NRCS provides soil surveys in digital form as spatial map unit polygons (generally at 1:15,540 to 1:24,000 scales) and soil physical, chemical, and interpretation information for individual soil map units in database form as the Soil Survey Geographic Database (Version 2)(SSURGO2) (available at <http://soildatamart.nrcs.usda.gov/>). Digital NRCS information is available for all counties crossed by the Keystone XL Project in South Dakota. This information is also available in hard-copy soils surveys. Soils information is important for the evaluation of the impacts of pipeline construction on agricultural and range productivity, erosion potential, and reclamation potential, and for assessing general constructability and certain soil-related construction hazards. Current practice is to evaluate soil characteristics, properties, and limitations along pipeline

rights-of-way by securing the spatial soil map unit data for the counties crossed by the pipeline. Soil map units are placed into project-specific interpretative groups based on their properties using database queries. Using a geographic information system (GIS), the crossing length of each soil map unit along the pipeline route (and at aboveground facility sites) and its project-specific interpretative group is generally provided in tabular form and is frequently summarized by county for permitting purposes. The resulting information is used to assess site-specific soil characteristics and limitations. Common soil interpretative groups include topsoil thickness, slope class, highly wind and water erodible soils, compaction prone soils, stony and rocky soils, saline, sodic, and saline-sodic soils, prime farmland, and hydric (wetland) soils, land capability classification, and poor reclamation potential.

Q: Is the presentation of the soils and erosion/sedimentation information provided in Keystone's application (1) sufficient under the applicable SDARs, and (2) consistent with industry standards?

A: Keystone's application included a description of the general physical characteristics and the physiographic setting for the soils that adequately provides the environmental setting for soils along the proposed route. However, the presentation of soils and erosion and sedimentation information in Keystone's application does not provide sufficient information or organization to identify the location, magnitude, and type of soil-related limitation sufficient to meet what I believe to be the intent of the SDARs, and does not meet industry standards for presenting soil limitations along the pipeline right-of-way for the reasons described below:

- While the maps contained in the soil map book (provided as Exhibit A of Keystone's application) accurately identify locations of specific soils along the proposed pipeline right-of-way, the maps cannot be used to assess potential project-related soils

impacts without more specific information on soil properties and limitations for specific soils.

- Specific soil limitations addressed in the application include soil compaction, rutting, low reclamation potential, hydric soils, prime farmland soils, and stony/rocky soils. State-level percentages were provided for compaction and rutting prone soils, soils with low reclamation potential, hydric soils, and prime farmland soils. However, the method for calculating these percentages, and the definitions for soils falling into these classifications were not provided. Presenting percentages of soils in these classes for the whole route does not provide enough detail to identify where specific soil-related problems are likely to occur.
- Additional soil-related limitation categories are needed that are appropriate to the environment and climate along the proposed route in South Dakota. Soil salinity and sodicity is described as a potential soil limitation affecting reclamation potential and aspects of constructability, but the quantity of saline and sodic soils is not identified or located. Other important soil limitations for South Dakota would include soils with restrictive layers (lithic/paralithic), steep slopes, high pH, and highly wind and water erodible soils.
- The CMRP is described as providing soil protection measures but applicable sections specific to identified soil limitations are not cited in the application, and mitigation measures for several potential soil limitations (e.g. saline/sodic soils) are not provided.
- The application states that Keystone will “work closely with landowners and soil conservation agencies to identify and implement recommended soil conservation practices in specific areas where they are needed,” but does not provide a procedure or protocol for this process.

- Soil reclamation and seeding prescriptions for land, especially in range, are frequently related to specific soil groups (e.g. NRCS Range Class). No such soil or land use groupings are provided in the Application.

Q: Have these concerns been addressed in other information provided by Keystone? If so, how?

A: Keystone provided additional information on soils and sedimentation/erosion in response to data requests from PUC staff which addressed the general concerns presented above and additional specific requests dealing with Soils and Erosion and Sedimentation.

Q: Please evaluate Keystone's response to PUC staff's request for tables identifying the information on soil limitations available in the SSURGO2 database for the pipeline route, pump station and valve sites, and other work areas.

A: Keystone provided six tables (See Attachment 2 to this testimony) that satisfy the PUC staff's request for specific soil limitation information by soil map unit. The tables provide detailed breakdowns of soil limitation categories by soil map unit and crossing length for the pipeline route (Table 1) and Access Roads (Table 2); and soil map unit and acreage for Facilities (e.g., off right-of-way work areas, aboveground facilities) (Table 3). County Summaries are then provided by total crossing length in each limitation category for the pipeline route (Table 4) and access roads (Table 5) and by acreage in each limitation category for facilities (Table 6).

Q: What soil limitation categories were used, are they adequately defined, and are they appropriate to evaluate the potential limitations, adverse impacts, and construction hazards specific to the environment along the pipeline route in South Dakota?

A: Soil limitations in the tables provided by Keystone (provided in Attachment 2 to this testimony) include soils with shallow bedrock; soils with other shallow restrictive layers;

drought prone soils and soils with low re-vegetation potential; steeply sloping soils; saline, sodic, and saline-sodic soils; low or high pH soils, compaction prone soils; severely wind erodible and severely water erodible soils; stony or rocky soils; hydric soils, and prime farmland soils.

Keystone provided specific definitions for several limitation categories (see Attachment 3 to this testimony) including highly wind and water erodible soils; low reclamation potential soils; saline, sodic, and saline sodic soils; prime farmland; hydric soils; compaction-prone soils; stony/rocky soils; soils with shallow bedrock; and droughty soils. Slope ranges were not provided to identify steeply sloping soils, and the category "all shallow restrictive layers" was not defined.

The limitation categories selected are appropriate to describe the characteristics, construction-related limitations, and potential impacts of pipeline construction on soils and soil productivity. For example, soil with shallow bedrock may substantially increase in volume when backfilled and pose challenges for trenching and handling trench crowning; highly wind and water erodible soils will require best management practices as indicated in the CMRP to prevent excessive erosion and sedimentation; saline, sodic, saline-sodic, droughty soils, soils with restrictive layers, and high and low pH soils may pose difficulties with respect to establishment of suitable vegetative cover and may have poor reclamation potential; steeply sloping soils may be erosive, and present construction hazards if sodic. Maintenance of soil quality, appropriate topsoil stripping, and decompaction may be special issues on prime farmland soils.

The level of detail provided in Tables 1 through 3 allows the evaluation of detailed, site-specific soil limitations when used in context with the soil maps provided as Exhibit A in the application. Tables 4 through 6 appropriately summarize the soil characteristics and limitations by county, and permit the assessment of the presence and magnitude of the

major potential soil-related problems for pipeline construction and post-construction reclamation.

Q: Please evaluate Keystone's response to PUC staff's request to identify specialized construction and/or restoration efforts or mitigation measures that are proposed to maintain soil productivity in areas with saline, sodic, and saline-sodic soils.

A: Keystone proposes to develop site-specific construction/reclamation procedures that are applicable to specific land use/environmental settings prior to construction. Each specific setting (called Construction/Reclamation (Con/Rec) Units) is based on areas with similar pre-construction land-use, slope, soils, and vegetation. Keystone provides examples of Con/Rec Units as including Mixed Grass Prairie, Badlands, Forested Waterway, Crop Field, and Tame Pasture. Keystone's approach indicates an understanding of the need for specific construction and reclamation procedures to deal with the substantial variety of landform and soil conditions experienced along the route. Forested waterways (probable woody draws and river floodplains), while uncommon, are important ecological components whose soil characteristics (steep land in woody draws and potential wet areas adjacent to rivers) will be important in both construction and reclamation.

Keystone's examples of Con/Rec Units, while not a complete list, are appropriate.

However, Con/Rec Units will not be useful until they are developed and implemented. I recommend that the PUC require Keystone to provide its Con/Rec Unit classification system and corresponding pipeline milepost references prior to construction and that this classification system be prepared in consultation with the appropriate state or area NRCS staff as suggested by Keystone in Section 5.3.4 of the application.

With respect to saline, sodic, and saline-sodic soils, Keystone provides the following examples of specific reclamation measures that may be used in areas where these soils are present:

- alteration of soil handling procedures to reduce disturbance of natural soil horizons;
- segregation of topsoil materials conserved to avoid increasing soil quality concerns to unaffected areas;
- discing or harrowing re-spread topsoil only to the depth of the topsoil, to avoid mixing with subsoils;
- selection of a seed mix appropriate for the site; and
- to the extent practicable, avoidance of small saline seeps in agricultural lands, if these seeps do not encroach substantially into the right-of-way.

The sample procedures provided to deal with salinity and sodicity show an understanding of the potential reclamation issues associated with these soils that can vary substantially in soil physical and chemical properties with depth that can require special soil handling procedures and that are suited only to specific adapted plants.

They also recognize that saline seeps can be a significant issue associated with agricultural land. I provide an additional recommendation that pertains to agricultural areas with saline, sodic, and saline-sodic soils later in my testimony.

Q: Please evaluate Keystone's response to PUC staff's request to identify specialized construction and/or restoration efforts to deal with potential trench crowning and excess subsoil and ripped hard (lithic) and soft (paralithic) sandstone and shale bedrock.

A: Keystone provided a table of shallow bedrock locations along the proposed pipeline route and referenced the response to another data request question dealing with rock disposal, which stated: "Rock from construction shall be disposed of using one or more

of the following methods: (a) Windrow neatly along the edge of the ROW within the ROW limits, (b) Remove from the ROW and haul to an approved dump site, and (c) Use as rip-rap to stabilize the banks of watercourses. Rock removal may be carried out with a mechanical rock picker or by manual means, provided that preservation of topsoil is assured. Rocks removal will result in a quantity, size, and distribution of rocks on the ROW equivalent to that found in adjacent lands."

Removal and handling of excess hard bedrock is not expected to be much of a problem based on the information provided in the county soil limitation summary table because only 1.17 miles of the route is projected to have hard bedrock. However, 167 miles (53.3 percent) of the proposed route is projected to have a restrictive layer within 5 feet of the surface. Much of this is in Harding (58.2 miles), Perkins (13.6 miles), Meade (31.8 miles), and Jones (23.4 miles) Counties. While this bedrock is likely weakly indurated shale that is easily ripped and dug through with conventional construction equipment, in some areas the bedrock will underlie subsoils and will be excavated as relatively competent pieces that could be gravel to cobble sized. These bedrock fragments may be loosely packed when backfilled resulting in a "bulking factor" that could result in greater soil volumes and the need to account for extra trench spoil volume during restoration.

Q: You have noted that alternative soil handling techniques might be appropriate in areas containing certain soils. Do you have any recommendations regarding such situations?

There are two soil conditions where alternative soil handling procedures might be appropriate during the trenching and backfill operations: areas where indurated (hard), paralthic shale and sandstone underlie unconsolidated subsoils, and areas where saline subsoils underlie non-saline subsoil horizons. In such areas, mixing of poor quality

subsoils with overlying soil layers could potentially reduce soil productivity and adversely affect crop yields. Because alternative soil handling procedures can be costly and can sometimes require additional workspace, the decision to use such procedures should be made based on consultation with NRCS staff, which has the expertise to evaluate soil conditions and appropriate soil handling methods for the project area. Therefore, I recommend that if the PUC issues a permit for the Keystone XL Project, the permit include a condition requiring Keystone to consult with the state or area NRCS office to identify soils for which alternative handling methods in agricultural lands would be appropriate, develop construction procedures to minimize impacts on such soils, and potentially make those alternative soil handling methods available to landowners to maintain soil productivity in agricultural lands.

Q: Please evaluate Keystone's responses to PUC staff's requests to identify specialized construction and/or restoration efforts or mitigation measures that are proposed to be used in steep areas characterized by the presence of sodium bentonite that have been identified as having potential slump and/or restoration problems, and to maintain a safe workplace when constructing in sodium-affected soils, particularly during wet periods.

A: Steep areas with sodium bentonite at the surface typically exhibit badlands topography, are naturally erosive, and are usually sparsely vegetated to unvegetated under natural conditions. Sodium bentonite is a 2:1 expanding clay mineral that disperses when wet and forms crusts consisting of hard and massive (unstructured) chips when dry. "Slick spots" and wet areas in drainages with adjacent, highly saline soils are frequently associated with this badlands type topography. Keystone accurately and appropriately identifies that the primary goal of post-construction restoration and reclamation is stabilization of the construction right-of-way to prevent erosion. Revegetation is

secondary, and would be considered if adjacent areas are vegetated.

Keystone's construction, reclamation, and mitigation measures are proposed to be applied on an as needed basis depending on site-specific conditions that would be appropriate for a "Badlands" Con/Rec Unit, and they appropriately represent the types of construction procedures and reclamation "tools" that can be specifically applied to appropriate Con/Rec Units. In response to the PUC staff's data request, Keystone indicated that measures that could potentially be applied to steeply-sloping, sodium bentonite "Badlands," depending on site-specific conditions such as slope steepness, include but would not be limited to:

- temporary sediment barriers to retard slope erosion during construction;
- placement of trench plugs to restrict subsurface water flow in the backfilled trench, which could accelerate slope slumping;
- recontouring the right-of-way to match surrounding topography to the extent practicable to minimize concentrating storm water runoff on the right-of-way;
- permanent sediment control structures such as water bars to divert storm water runoff from the regraded right-of-way;
- depending on the amount of naturally occurring rock [stone lag] or woody debris on the reclaimed slope, mulching with materials such as straw on more gentle slopes, wood fiber mulch and tackifier on moderately steep slopes and erosion control matting on extremely steep slopes or at sites where other mulching methods might not be effective; and
- revegetation, if appropriate for the site, with species similar to those found adjacent to the right-of-way.

Keystone recognizes that the dispersed "greasy" nature of sodium bentonite can create construction hazards and has indicated that it would address wet conditions on dispersed wet soils by shutting down construction operations until the soil dries if conditions prevent safe construction operations. Alternatives include securing working equipment to stationary, stable equipment ("dead man") by means of cables, or blading off the slick surface if only a thin surface soil zone is saturated. Storage of the bladed material must be considered, as does the topsoil status and the topsoil stripping protocols. In fine textured soils where the topsoil has been stripped, blading a thin, wet surface to uncover drier material is standard industry practice. I recommend that the PUC require that Keystone include such practices as applicable to specific Con/Rec units when it develops specifications for each unit prior to construction, and that specifications include appropriate construction minimization, mitigation and post construction reclamation procedures for each unit.

Q: Please evaluate Keystone's response to PUC staff's request to identify aboveground facilities that would be built on prime farmland and the acreage of prime farmland to be permanently affected as a result.

A: This information was provided in the detailed soils tables for the facilities (Tables 3 and 6 in Attachment 2). Approximately 13.6 acres of prime farmland and farmland of statewide importance will be permanently removed from actual or potential agricultural use. The majority of the impacts is associated with pump stations proposed in Meade, Haakon, and Tripp counties (13.5 acres). An additional 0.1 acre would cumulatively be affected by the establishment of mainline valves.

Q: Please evaluate Keystone's response to PUC staff's request to provide a more detailed description of soils and potential soil impacts in the Sand Hills region in

southern Tripp County, and to identify and describe any special construction or reclamation methods proposed for restoring soils in this region.

A: Keystone provided the table below in response to PUC staff's request. The table indicates that the pipeline in Tripp County will cross approximately 11.1 miles of areas with soils characteristic of sand dunes. Keystone indicated in the response that construction and restoration measures to be implemented in the sand dune areas are provided in Section 4.15 of the CMRP.

Sand Hills Soils in South Dakota

County	From MP	To MP	Distance Crossed (miles)
South Dakota			
Tripp County	570.2	572.8	2.6
	574.7	575.6	0.9
	576.5	578.7	2.2
	582.8	588.2	5.4

Areas with Temporary Impacts to Sand Hills Soils in South Dakota

County	TYPE	FACILITY	Area Crossed (acres)
South Dakota			
Tripp County	Permanent	Easement	66.8
	Temporary	Easements and ATWS	83.7
		Pipe yards	30.0

Keystone interpreted the high-resolution aerial photographs used in the land use maps to identify sand hill areas that consist of native range/pasture land with characteristic sand hills, ridges and blowouts. Keystone provided entry and exit mileposts for sandhills

areas, but did not identify the specific soils. Specific soils within the mileposted increments tabulated and identified above could be determined using GIS or from the soils maps in Exhibit A of the application. This would identify the locations of specific soils for which the site-specific construction and reclamation procedures provided in Section 4.15 would apply.

Based on Keystone's CMRP, site-specific construction and reclamation procedures applicable to sand hills would involve the identification and avoidance of particularly erosion prone areas, minimizing the width of ground disturbance within the construction right-of-way in these areas, appropriately segregating topsoil, minimizing traffic through sensitive areas where plant root systems would be severely damaged by heavy traffic, restoration using native seed mixes and appropriate weed free mulches, applying proven erosion control best management practices in this highly erosion-susceptible landscape, and accommodating existing land uses.

Keystone's site-specific construction and reclamation procedures are appropriate to minimize and avoid unnecessary adverse impacts and appropriately restore components of the sand dune areas affected by construction. I recommend that the approach Keystone has used to identify specific construction and reclamation procedures to be implemented in Sand Hills Areas be used as a template for the development of construction and reclamation procedures to be incorporated into other proposed Con/Rec Units.

Q: Please evaluate Keystone's response to PUC staff's request to identify NRCS range class equivalents for soils crossed by the pipeline.

A: Keystone recognizes the diversity of environmental settings and land uses along the proposed pipeline route in South Dakota, and also recognizes the utility of project- and use-specific classification systems to develop construction and reclamation procedures

and prescriptions that would minimize adverse impacts. Keystone indicated in response to a staff data request that the Con/Rec classification units will be based on several features including but not limited to soil type, land use, and landform and based on information from a variety of sources including consultation with local and regional NRCS offices. Keystone has indicated that NRCS Ecological Sites and SSURGO2 data may be incorporated into the Con/Rec Units.

To restate my views on the Con/Rec Unit classification proposed by Keystone, I believe that this system has very good potential to appropriately identify situations where site-specific construction and reclamation procedures could be implemented to minimize construction-related impacts and to facilitate the appropriate restoration and reclamation of affected areas. I recommend that the PUC support the development and implementation of the Con/Rec Unit classification for use on the Keystone XL Project by conditioning its permit to require a workable system developed with input from appropriate agency staff prior to construction.

Q: Please evaluate Keystone's response to PUC staff's request to identify the length of the pipeline route that may have agricultural draitiles potentially affected by trenching activities.

A: Draitiles would be rare along the pipeline route with the exception of areas with extensive floodplain soils. Keystone has estimated that approximately 3 miles of the pipeline route in South Dakota have soils that may be tiled, and indicate that this is a conservative estimate. I agree. In the unlikely event that draitiles are encountered, they will be repaired as indicated in the CMRP, with some likely modifications that will bring the draitile repair process to industry standards.

Q: Please evaluate Keystone's response to PUC staff's request to identify where Keystone proposes site-specific erosion control measures due to slope length, magnitude, and soils and to describe those measures.

A: Keystone has not yet identified specific areas requiring site-specific erosion and sediment control plans. However, Keystone has indicated that it will work with landowners and conservation agencies to develop site-specific best management practices as necessary, and has provided detailed tables and maps of soil conditions that identify locations where highly erosive conditions exist. Keystone has indicated that it will implement measures outlined in the CMRP, which includes best management practices that use slope length and magnitude to minimize soil erosion hazards. The final pre-construction design efforts will include site-specific drawings and plans that identify and locate the type of best management practices proposed for specific highly erosive locations that are considered particularly sensitive to erosion.

CURRICULUM VITAE

JAMES L. ARNDT, Ph.D., LPSS, CPSS, PSC

Senior Scientist, Professional Soil Scientist
NATURAL RESOURCE GROUP, INC.

EXPERTISE

- Soil Chemistry, Physics, Genesis and Classification
- Soil Survey, Mapping and Interpretations
- Permafrost (Gelisols) soil description and characteristics
- Urban Soils, Assessment and Interpretation
- Environmental Resource Inventories
- Hydric Soil Identification and Assessment
- Wetland Hydrogeology
- GIS, CAD Applications and Development, Database Creation and Management, Digital Terrain Modeling.
- Wetland Delineation (COE 1987), Wetland Identification (Cowardin, 1979; Shaw and Fredine; 1971; Stewart and Kantrud, 1969)
- Mitigation and Treatment Wetland Planning and Design
- Regulatory Compliance Strategies
- Expert Witness Testimony
- Laboratory Analysis, Interpretation of Soil and Water Laboratory Data, geochemical modeling
- Information Transfer (Report Preparation, Presentation of Pertinent Findings, Teaching)

ACADEMIC BACKGROUND

- Ph.D., Soil Science, ND State University, 1995
- M.S., Soil Science, ND State University, 1987
- B.S., Soil Science, Natural Resource Management, Univ. Wisc. - Stevens Point, 1980
- B.A., Psychology, Anthropology, English, Univ. Wisc.-Milwaukee, 1976

REGISTRATION

- Licensed Professional Soil Scientist, Minnesota #30684
- Licensed Professional Soil Scientist, Wisconsin #112
- Licensed Professional Soil Scientist, North Dakota #64
- Certified Professional Soil Scientist, ARCPACS #24904

PROFESSIONAL AFFILIATIONS

- Minnesota Association of Professional Soil Scientists, President Elect, 2000; President, 2001; Past president, 2002. Chair Professional Practice Committee 2003-2005.
- Soil Science Society of America
- Society of Wetland Scientists
- Minnesota Wetland Delineators Association
- American Geophysical Union
- Reviewer/Referee;
Wetlands,
Soil Survey Horizons,
Soil Science Society of America Journal,
Journal of Hydrology,
National Science Foundation,
Journal of Environmental Quality.

Journal of Vegetation Science/Applied Vegetation Science

SPECIALIZED TRAINING

- *Environmental Compliance Seminar; Regulatory Overview and Guidance Seminar*, Federal Energy Regulatory Commission, July 9-10, 2007, Atlanta Georgia
- *Stormwater Compliance training*. Paradigm Engineering, March 2, 2005.
- *Design Techniques in AutoCAD^{mlt}*, Mr. John Moreira, P.E., 2004.
- *Wetland Plant Identification*, Biotic Consultants, Inc. (Dr. Robert H. Mohlenbrock, Instructor), August 19-22, 2003.
- USACE-approved *Regulatory IV Wetland Delineation Training Course*, with an Introduction to Wisconsin Wetlands Regulation, August 11 - August 15, 2003, UW-La Crosse Extension, La Crosse Wisconsin.
- *Creating and Using Wetlands for Wastewater and Stormwater Treatment and Water Quality Improvement*, 2000 (Drs. RH Kadlec and RL Knight, Instructors), Department of Engineering Professional Development, University of Wisconsin - Madison.
- *Accesssm Fastrack*. Science Museum of Minnesota - Computer education Center. 1999.
- *Wetland Functions and Values Workshop; An In-Depth Look at Today's Methods: WET, WRAM, MNRAM, HGM*, 1998.
- *Soil Landscape-Vegetation Relationships in Arctic Tundra, Advances in Taxonomy and Genesis of Permafrost Soils (Gelisols) with an emphasis on hydric permafrost soils*, University of Alaska Fairbanks, 1999
- *Power Arcviewsm, Advanced techniques in Arcview GIS*, Rowekamp and Associates, 1998.
- *Wetlands Conservation Act Administrative Training*, Minn. Board of Water and Soil Resources, Minn. Assoc. Soil and Watershed Districts, 1997, 1998, 2001.
- *Project Management Skills: The Complete Curriculum*. University of St. Thomas, Minnesota. 1996.

WORKSHOPS TAUGHT

- Hydrology of Shallow Aquifers in Soil Landscapes. Hydric Soil Identification for Wetland Soils Workshop, 1995 Annual Meeting Soil Science Society of America, St. Louis, MO, 1994 Annual Meeting Soil Science Society of America, Seattle, Washington.
- Hydric Soils and Hydrology, Wetland Field Methodologies Workshop, Franklin Svoboda and Associates, July 12-15; September 20-21, 1994 Minneapolis, Minnesota.
- For symposia see invited presentations below.

CURRICULUM VITAE

PROJECT-RELATED EXPERIENCE

Dr. Arndt has worked in soil science for over 25 years. He specializes in pedology research, including wetland biogeochemistry, the genesis and morphology of hydric soils, soil survey and interpretations, applications of IT methods to natural resource evaluation, and the preparation of reports in support of NEPA compliance. He has worked on several large interstate pipeline projects in support of the preparation of FERC resource reports, pre-application filings, and pre-construction resource evaluation. He has provided expert witness testimony and technical expert assistance on various soils issues.

He has authored many refereed and outreach publications and frequently speaks on soils, natural resource, and technology application issues. Dr. Arndt's skills include the applications of GIS/GPS/remote sensing/terrain modeling technologies to resource assessments emphasizing interstate gas and oil pipeline projects, applications of hydrology and hydric soils research to the delineation of wetlands and the assessment of wetland functions. He has developed procedures that integrate GIS/GPS/database technology to evaluate wetland and soil resources for large natural resource inventory projects and has worked on several complex components of third-party EIS projects for the USACE and MnDOT.

For Natural Resource Group, Inc.

- Task Manager. In association with Ms. Linda Fisher, Esq. (Larkin Hoffman Daly & Lindgren Law Firm) prepare documentation in support of a Section 404 Clean Water Act and Section 10 Rivers and Harbors Act Individual Permit Application and supporting NEPA documentation for Enbridge Partners, combined Alberta Clipper and Southern Lights Diluent pipeline projects. Project Ongoing.
- Task Manager. In association with Ms. Linda Fisher, Esq. (Larkin Hoffman Daly & Lindgren Law Firm) prepare Supplemental Clean Water 4041b permit application materials for Enbridge Partners, Southern Lights pipeline project. Project Complete.
- Prepare Cumulative Impact Analysis Section for the Environmental Assessment (EA) for Enbridge Partners LSR pipeline project. Project Complete.
- Expert Witness: Train county assessors in agricultural impacts resulting from pipeline construction including compaction, topsoil mixing, and other impacts. Provide expert testimony on agricultural impacts to soil and crop productivity at condemnation hearings for the Minnesota Pipe Line Company, MinnCan Project. 2008 - 2009, Project on-going.
- Task Manager: Train and act as technical support for agricultural and soil related construction issues along Minnesota Pipe Line Company's 300-mile MinnCan Project, Minnesota. Project on-going.
- Task Manager. Manage subcontractors performing wetland delineations along the approximate 300-mile proposed MinnCan pipeline route in Minnesota. Minnesota Pipe Line Company. Project on-going.
- Task Manager. Assess and document properties of a calcareous fen along the Enbridge Partners Southern Lights pipeline route, Pennington County, Minnesota. Assist in developing avoidance reroute alternatives and coordinate with MnDNR staff to completely avoid impacts. Project complete 2007.
- Task Manager. Feasibility study modeling soil temperatures along a proposed pipeline right-of-way from Montana to Louisiana. Project involved application of STATSGO soil data, detailed climatic data, and soil temperature modeling to estimate average temperatures at 4.5 foot depths along nodes separated by 100 miles. Anonymous client. Project complete 2006.
- Task Manager. Develop project-specific wetland delineation databases (Microsoft Access™) to facilitate the rapid, economical presentation and GIS-assisted analysis of wetland delineation data. Minnesota Pipe Line MinnCan Project (Minnesota), Gulf South Gulf Crossing Project: (Oklahoma, Texas, Louisiana), Palomar Gas Transmission LLC Palomar Project (Oregon), Enbridge Partners Southern Access/Southern Lights/Alberta Clipper projects (Minnesota, Wisconsin, Illinois). Projects on-going.
- Task Manager: Evaluate aquifer sensitivity to crude oil releases, Troy Buried Valley Aquifer, Mazon Unconfined Aquifer, Illinois. Enbridge Partners Southern Access Stage 2 Project, Illinois. Tasks completed 2006 and 2007.
- Technical Assistance: Assist with development of Pipeline Construction Agricultural Impact Mitigation Plan (AIMP) and Appendix to the AIMP developed to address pipeline construction across Certified Organic farms. Enbridge Partners Southern Access Stage 2 Project. Minnesota Pipe Line MinnCan Project, Minnesota. Complete 2007.
- Technical Assistance. Use of detailed SSURGO2 soil spatial and attribute data to determine soil properties and construction limitations along proposed pipeline rights-of-way. Enbridge Partners (Wisconsin, Illinois, Minnesota, and North Dakota), Minnesota Pipe Line Company (Minnesota), Guardian Pipe Line (Wisconsin), Gulf South (Oklahoma, Texas, Louisiana), Willbros Company (Wyoming). Tasks completed 2006-2008, tasks ongoing.
- Technical Assistance. Develop and employ digital terrain models of digital elevation data to augment existing soils data. Develop project-specific soil property and construction limitation maps, Overland Pass Project, Wyoming. Task on-going.

For Peterson Environmental Consulting, Inc.

- Expert technical assistance, Crowley, Haughey, Hanson, Toole & Dietrich P.L.L.P. and Williston Basin Pipeline Company. Using GIS and Field techniques critically evaluate pipeline-related soil impact issues and reclamation compliance along pipeline right of way in southwest North Dakota. 2004. Project completed through landowner settlement.
- Expert technical assistance, Larkin Hoffman Daly & Lindgren Law Firm, LLP, Gislason and Hunter Law firm, and Hutchinson Utilities Commission. Critically evaluate using GIS and field techniques soil compaction/soil mixing

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- issues, their influence on crop yields, and Agricultural Impact Mitigation Plan compliance along 90 miles of pipeline right of way in south-central central Minnesota. Project complete 2005.
- Project Manager. Determine impacts of proposed TH41 road construction on the ecology, soils, and hydrology of the Seminary Calcareous Fen, Carver County, Minnesota. In support of the DEIS developed for the project. Subcontractor to MnDOT AND SRF Consulting, Inc. Phase 1 of project complete. Technical assistance and document review, Phase 2 on-going.
 - Project Manager 2004-2005. Design, implement, document, and report on a study to evaluate the effects of wetland buffer width on sediment and nutrient load reductions to receiving waters. Project funded by the Metropolitan Council of the Twin Cities, the Builders Association of the Twin Cities, and the National Association of Home Builders.
 - Project Manager. GIS and database support, wetlands along the Alliance Pipeline Corridor, North Dakota, Minnesota, Iowa, and Illinois. Reviewed and consolidated existing data files and data collected by PEC during 1997-1999, cleaned, revised, and consolidated existing spatial (Arcview) and attribute (Access) databases, develop consolidated spatial and attribute databases of wetland location and wetland physical characteristics for incorporation into the Alliance master GIS. Alliance Pipeline Company, Inc. 2003.
 - Project Manager. Evaluate the potential impacts of using non-perforated PVC tile support on the function of repaired drain tile damaged during pipeline construction. Natural Gas Consulting, Inc. 2003.
 - Principal in Charge. Development of a mitigation and monitoring strategy for the proposed Pelican Lake Outlet Alternative to mitigate Devils Lake flooding in North Dakota. Prepared salinity and groundwater effects mitigation strategies. Assisted in development of project GIS. USACE, Project Complete, December 2002
 - Expert Witness Testimony. Provide expert testimony on the extent of historic and current wetlands on a section of land in North Dakota. Case involved review of historic aerial photographs, fieldwork on wetland delineation, forensic soils work, and development of a project GIS. Case involved unauthorized fill activities in wetlands. United States Department of Justice, case settled 2002.
 - Project Manager. Assess impacts to wetland resources of a reduced sulfide zinc/copper shaft mine proposed by Nicolet Minerals Corporation near Crandon, Wisconsin. Prepare Wetland Impacts component of the project EIS. Prepared for the USACE as approved subconsultant to Montgomery Watson. Project complete April 2003.
 - Project Manager. Phase II Assessment of the Soil Salinization Potential of Devils Lake Flood Damage Reduction Alternatives. Team Leader to assess the magnitude of induced soil salinization under Upper Basin Storage and West Bay constructed outlet discharge alternatives. USACE, Project Complete, April 2002.
 - Project Manager. Preparation of Environmental Resource Report 7 (FERC Guidelines) for several pipeline right-of-way projects in North Dakota, Minnesota, Iowa, Wisconsin, Illinois, and Alaska. Used soil spatial and attribute databases (STATSGO, MUIR) to identify specific soil limitations and hazards along the pipeline routes. Complex queries and models on the soil attribute data were developed in Microsoft Access™ to provide more detailed, use specific interpretations than those present in the NRCS database. Natural Resource Group, Inc. 1996-2002.
 - Project Manager. Phase I Assessment of the Soil Salinization Potential of Devils Lake Flood Damage Reduction Alternatives. Team Leader for Literature review and Phase II scope development to assess the magnitude of induced soil salinization under Upper Basin Storage and Peterson Coulee discharge alternatives. USACE, completed 2001.
 - Project Manager. Manage and direct soil documentation fieldwork for the Dodge and Goodhue Counties Order 2 Soil Survey update (MLRA 104). Under contract with the Minnesota Board of Soil and Water Resources (BWSR) and joint cooperation between the University of Minnesota, BWSR, and the NRCS.
 - Project Manager. Perform a geochemical evaluation (PHREEQC-1) of created wetlands to mitigate high groundwater-sulfate levels. Provide a conceptual created wetland design for treatment wetland. Northern States Power and ERG, Inc. 2000-2001, project complete.
 - Project Manager. Restoration of historic wetlands within the Sugarloaf Cove Natural and Scientific Area. Performed detailed assessment of pre-disturbance hydric soils and landforms, and designed and supervised restoration, including excavation and reseeded efforts. Minnesota Department of Natural Resources. 1999-2001.
 - Project Manager. Produced digital Order 1 soil survey of land holdings for the Shakopee Mdewakanton Sioux Community. Tasks include field mapping and verification, digital terrain modeling (Surfer, TAPESG, Arcview, Spatial Analyst), creation of descriptive map legend, production of detailed profile descriptions (NASIS), soil attribute database development (Access™, MUIR, NASIS, SSURGO), and creation of soil data layers for use in GIS (Arcview). Cooperative project between the NRCS, the University of Minnesota, 1999-present.
 - Project Manager. Delineation of over 100 problem and disturbed area wetlands where interpretation of hydrology, landform, and soils were critical to produce an accurate delineation. 1995-Present.
 - Project Manager. Preparation of an informational document on calcareous fens in northeastern South Dakota. The document consisted of a review of calcareous fen characteristics, briefly examined pedologic, hydrologic, geochemical, and floristic characteristics of dome type fens in the area, and assessed values and functions in relation to maintenance of the fen resource. USEPA, 1996-1999.
 - Project Manager. Develop Commitments Database (Microsoft Access) that employs user-friendly forms-input to facilitate error-free data entry, relational tables to organize the data, forms driven logic queries to reduce the dataset, and reports output to facilitate transfer and printing of query results. Database was developed to organize commitments made to local, county state and federal entities involving construction of a 1000-mile pipeline

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through North Dakota, Minnesota, Iowa, and Illinois. Natural Resource Group, Inc. 1998-1999.

- Project Manager. Organized, planned, and supervised the delineation of over a thousand wetlands along an 850 mile length of a proposed, natural-gas pipeline. Delineations made extensive use of GIS (Arcview[™]), GPS (CMT PCGPS), and database (Access[™]) methods developed in-house under my supervision. Digitized polygon, point, and line data were merged with photos and attribute data to automate the production of data forms compliant with 1987 COE Wetland Delineation Manual and NRCS specifications. Digital spatial and attribute data were integrated into environmental worksheets prepared by the project engineer. All reports were produced in html-linked digital (Adobe Reader) format. Natural Resources Group, Inc., 1996-present
- Project Manager. Hydrologic assessment and delineation of partially and effectively drained wetlands on over 1500 acres of sodfarms (drained peatlands) and other historically drained lands in East Central Minnesota. Projects combine geostatistical evaluation (Kriging in Surfer, GEOEAS) and 3-dimensional mathematical modeling (Surfer, Arcview Spatial Analyst) of jurisdictional hydrology in a climatic context to determine the extent of jurisdictional wetlands. Sienna Corporation, Pilot Land Development, Ed Fields and Sons, G.M. Development Inc., Glenn Rehbein Companies, 1997-Present.
- Project Manager. Hydrologic study of the effects of channelization, dredging, and drainage on the jurisdictional status of historic riparian wetlands proposed for development in Coon Rapids, Minnesota. Conceptual and mathematical models (Flownet, Modflow, Scope and Effect spreadsheets) of wetland hydrology were validated with field studies including hydric soil correlation and well and piezometer monitoring. Assisted with wetland permitting process, and wetland mitigation design for the entire project. Robert C. Muir Company, 1995-1996.
- Project Manager. Scope and Effect analysis of municipal well withdrawals and surface ditching on potential wetland drainage in a 32 acre parcel in Blaine, Minnesota. Mr. Doug Bannochie, 1995-1996.
- Project Manager. Perform a field investigation of known and proposed calcareous fens in Yellow Medicine County, Minnesota. The investigation examined pedologic, hydrologic, geochemical, and floristic characteristics of the known and proposed fen areas. Lincoln-Pipestone Rural Water, 1995.
- Project Manager. Perform a field assessment of the potential impacts of pipeline construction on nearby calcareous fens, Kendall County, Illinois. The investigation examined in detail pedologic, hydrologic, and floristic features of the area in the context of listing requirements for inclusion into the Illinois Natural Heritage Inventory and compared observed features to Minnesota Fen Criteria. Natural Resource Group, Inc., 1996
- Project Manager. Evaluate potential water quality and temperature effects of the proposed Farmington Planned Urban Development and Prairie Waterway on cold-water fisheries in the Vermillion River around Farmington, Minnesota. Trout Unlimited, Sienna Corporation, 1995

- Expert Witness Testimony. Inverse condemnation lawsuit involving stormwater and historic wetland issues. Barna, Guzy, and Steffen Ltd. Law Firm, 1996-1997.
- Expert Witness Testimony. Inverse condemnation lawsuit involving stormwater management effects on wetlands, watertables, and salinity in the City of Oakdale Minnesota. Jardine Logan, and Obrien, P.L.L.P. 1997-1998.
- Expert Witness Testimony. Inverse condemnation lawsuit involving the effects of stormwater management practices on land valuation, wetlands, and watertables in Shorewood, Minnesota. Hoff, Barry, and Kuderer, P.A., 1996-1997.
- Project Manager. Supervised and assisted with an inventory of native plant species near the proposed SEP-II Pipeline in McHenry County, Illinois. Natural Resource Group, Inc. 1996.
- Project Manager. Wetland soil and hydrology characterization for wetland-related litigation regarding a restoration of a drained wetland complex near Nicollet, Minnesota. Minnesota DNR-determined ordinary high water levels were correlated to existing soils, hydrology and historic water levels, Larkin-Hoffman Law Firm, 1996-1997.
- Retained Consultant. Provide information on hydrogeology, geochemistry, and soils for the Polk County Sanitary Landfill. Polk County, Minnesota, 1993-2000.

For North Dakota State University

- Research Associate/Instructor, Supervisor, Soil and Water Environmental Laboratory (SWEL), 1991 to 1995.
- Graduate Research Fellow/Supervisor, SWEL, 1987-1991
- Research Assistant/Supervisor, SWEL, 1983-1987
- Research Assistant, SWEL, 1981-1983.
- *Research:* Collect, process, evaluate (QA/QC), and interpret data. Prepare research reports and grant proposals pertinent to wetlands and pedology research specifically and soils research in general (see publications, below). Attend and assist in NRCS field reviews and correlation sampling for ongoing soil surveys (description, sampling, and characterization of over 200 profiles representative of soil series and map units in several counties). Present data and assist with various hydric soils workshops nationwide (see presentations, below). Collect soil samples and pedon descriptions, and install field equipment.
- *Laboratory:* Develop appropriate analytical methods, including computer-assisted data analysis. Supervise hourly employees, maintain laboratory equipment, purchase supplies, and manage operating budget. Provide assistance to private individuals requiring information on soil-water compatibility, interpretation of water and soil analyses. Perform laboratory analyses.
Teaching: As principal instructor.
1987 Soil Judging (Soil Sci. 340)
1993 Soil and The Environment (Soil Sci. 410/610)
1994 Soil and the Environment (Soil Sci. 410/610)
- *Teaching:* As support.
Instructor (1990, 1991, 1992) for sections on hydrology, wetlands, weathering and soil chemistry, and soil

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mineralogy, Soils 440: Soil Genesis, Survey, and
Classification (Dr. J.L. Richardson, Professor).

SELECTED PUBLICATIONS AND PRESENTATIONS

Hydric Soils, Hydrology, and General Soil Science

Arndt, J.L. and J. Flannery. 2007. Land and environmental data integration and management. Proceedings Geospatial Information & Technology Association, GIS for Oil and Gas Conference, September 24-26, 2007. Houston, TX

Richardson, J. L., J. L. Arndt, and J. A. Montgomery. 2000. CH 3: *Hydrology of Wetland and Related Soils*. in Richardson, J.L., and M.J. Vepraskas (eds.). *Wetland Soils: Their Genesis, Morphology, Hydrology, Landscapes, and Classification*. CRC Press. Boca Raton. FL.

Peterson, R.P., and J.L. Arndt. 1998. *Consideration of peat subsidence in wetland delineation activities*. Abstracts, 19th Annual Meeting Society of Wetland Scientists, Anchorage Alaska.

Arndt, J.L. 1994. *Hydrology of shallow aquifers in soil landscapes*. In J.H. Huddleston (ed.) *Hydric Soil Identification for Wetland Soils Workshop*. 1994 Annual Meetings of the Soil Science Society of America. November 12-17, 1994, Seattle WA.

Richardson, J.L., J.L. Arndt, and J.E. Freeland. 1994. *Wetland soils of the prairie potholes*. *Advances in Agronomy* 52:121-171. (invited paper).

Arndt, J.L., and J.L. Richardson. 1994. *Impacts of groundwater flow systems on hydric soils of the glaciated northern prairies of the U.S.* p. 64-84. *Proceed. 37th Ann. Manitoba Soil Science Society Meetings*, Jan. 4-6, 1994, Winnipeg, Manitoba, Canada.

Arndt, J.L., D.O. Rosenberry, and J.W. LaBaugh. 1993. *Effects of ground-water flow systems on hydric soils in two prairie wetlands in North Dakota*. *EOS* 74(43): 273.

Cooperating author in T.D. Searchinger et al., 1992. *How wet is a wetland? The impacts of the proposed revisions to the federal wetlands delineation manual*. Published jointly by the Environmental Defense Fund, New York, and the World Wildlife Fund, Washington, DC. 170pp.

Arndt, J.L., and J.L. Richardson. 1989. *A comparison of soils to wetland hydrology in North Dakota*. *Proc. 32nd Annual Manitoba Soil Science Society Meeting, Dep. Soil Science, Univ. of Manitoba, Winnipeg*. p. 76-90.

Richardson, J.L., and J.L. Arndt. 1988. *Groundwater recharge and discharge as fundamental pedogenic processes in Aquic moisture regimes*. *Agron. Abstr.*, p. 265.

Richardson, J.L., T.J. Malterer, A. Gienke, J.L. Arndt, M.J. Rosek, and A.J. Duxbury. 1987. *Classification problems associated with histic soils of calcareous fens*. *Soil Surv. Horiz.* 28(2):53-55.

Richardson, J.L., and J.L. Arndt. 1987. *Wetland soils in relation to land use*. p. 24-29 In *Proceedings of the North Dakota Wetlands Workshop*. July 13-15. Bismarck, ND. Published jointly by the North Dakota Extension Service and the U.S. Environmental Protection Agency.

Soil and Water Biogeochemistry

Arndt, J.L., and J.L. Richardson. 1993. *Temporal variations in the salinity of shallow groundwaters collected from the periphery of some North Dakota USA wetlands*. *J. Hydrology* 141:75-105.

Arndt, J.L., and J.L. Richardson. 1992. *Carbonate and gypsum chemistry in saturated, neutral pH soil environments*. In *Aquatic Ecosystems in Semi Arid Regions; Implications for Resource Management*, R.D. Robarts and M.L. Bothwell (eds.). N.H.R.I. Symposium Series 7, Environment Canada, Saskatoon, Saskatchewan, Can.

Hanson, M.A., M.G. Butler, J.L. Richardson, and J.L. Arndt. 1990. *Indirect effects of fish predation on calcite supersaturation, precipitation, and turbidity in a shallow prairie lake*. *J. Freshwater Biol.* 24:547-556.

Arndt, J.L., and J.L. Richardson. 1989. *Geochemistry of hydric soil salinity in a recharge-flowthrough-discharge prairie-pothole wetland system*. *Soil Sci. Soc. Am. J.* 53:848-855.

Arndt, J.L., and J.L. Richardson. 1989. *Geochemistry of hydric-soil salinity associated with wetlands in the subhumid prairie-pothole region, North Dakota, USA*. *Proceed 28th Int. Geol. Congr.*, July 9-19, 1989, Washington, DC; p. 1-53 to 1-54.

Arndt, J.L., and J.L. Richardson. 1988. *Hydrology, salinity, and hydric soil development in some North Dakota prairie-pothole wetlands*. *Wetlands* 8:93-108.

D.O. Rosenberry, J.L. Arndt, and J.W. LaBaugh. 1993. *Ground-water flow reversals and near-shore soil mineralization affect chemical characteristics of a prairie wetland in North Dakota*. *EOS* 74(43): 272.

Biondini, M.E., and J.L. Arndt. 1993. *The biogeochemistry of carbon, nitrogen, and sulfur transformations in seasonal and semipermanent wetlands*. Completion Report No. ND90-05. North Dakota Water Resources Research Institute, North Dakota State University, Fargo ND. 83pp.

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Arndt, J.L., and J.L. Richardson. 1993. *Salinity and salinization processes in selected drained and undrained wetlands in North Dakota*. Proceed. 36th Ann. Manitoba Soil Science Society Meetings, Jan. 6-7, 1993, Winnipeg, Manitoba, Canada. p. 84-102.

Richardson, J.L., J.L. Arndt, and J.W. Enz. 1990. *Effects of freezing on sulfate salts in North Dakota soils and wetlands*. p. 212-215. in K.R. Cooley (ed.) Proc. International Symposium Frozen Soil Impacts on Agricultural, Range, and Forest Lands, Spokane, Wash., March 21-22, 1990, CRREL Sp. Rpt. 90-1, U.S. Army Cold Regions Research and Engineering Laboratory, 72 Lyme Road, Hanover, NH.

Arndt, J.L., and J.L. Richardson. 1986. *The effects of groundwater hydrology on salinity in a recharge-flowthrough-discharge wetland system in North Dakota*. p. 269-277. In Proc. Third Canadian Hydrogeological Conf., Saskatoon Sask., 21-23 April 1986. International Assoc. of Hydrogeologists, Canadian National Chapter.

Arndt, J.L., and J.L. Richardson. 1985. *Geochemical controls on the ionic composition of pondwater and groundwater in some brackish-subsaline North Dakota Wetlands*. Agron. Abstr., p. 145.

Arndt, J.L., and J.L. Richardson. 1985. *Winter effects on the salt balance of saline ponds in North Dakota*. North Dakota Acad. Sci. Proc. 39:54.

GIS, Database, and Integrated Natural Resources Information Management

Timpson, M.E., J.L. Arndt, and S.A. Krych. 1998. *Innovative approaches to large-scale wetland delineation projects*. Agron. Abstr., p. 328.

Dignen, D.L., D. Desotelle, J.L. Arndt, and R.P. Peterson. 1998. *Using Access and GIS applications in water resource planning*. Abstracts, 1998 Conference of the Minnesota GIS/LIS Consortium, October 7-9, St. Cloud, Minnesota. p. 76-77.

Arndt, J.L., T. Kearby, S. Krych, and M. DeRuyter. 1998. *Geostatistical assessment of jurisdictional wetlands on a drained Minnesota peatland*. Abstracts, 19th Annual Meeting Society of Wetland Scientists, Anchorage Alaska.

Arndt, J.L., D.L. Krieger and M.E. Timpson. 2000. *Integrated database strategies for wetland and soil resource assessment*. Abstracts 7th International Symposium on Environmental Concerns in Rights-of-Way Management. Elsevier. <http://www.rights-of-way-env.com/index.htm>.

Timpson, M.E., Arndt, J.L., S.A. Krych, and D.L. Krieger. 2000. *Rapid and efficient wetland delineation along pipeline corridors using integrated technologies*. Abstracts 7th International Symposium on Environmental Concerns in Rights-of-Way Management. Elsevier. <http://www.rights-of-way-env.com/index.htm>.

Archaeology

Artz, J.A., E.A. Hayden, C.E. Haury, J.L. Arndt, and D.G. Hopkins. 1991. *Southwest pipeline archeology: The 1987 survey and test excavation programs at prehistoric sites in Mercer and Dunn Counties, North Dakota*. North Dakota State Water Commission, Contribution No. 54. 398pp.

Timpson, M.E., R.G. Thompson, and J.L. Arndt. 1987. *Pedologic investigation of the Dahnke archaeological site: Red River Valley, ND*. Agron. Abstr., p. 233.

Arndt, J.L., and D. Hopkins. 1987. *Report of pedologic investigations at the Marshall, North Dakota archaeological site*. Report subcontracted by the Univ. of North Dakota Anthropology Dept. to investigate archaeological sites along the SW Pipeline right-of-way.

Arndt, J.L., N.D. Prochnow, and J.L. Richardson. 1987. *Estimating weighted soil salinity with an aboveground electromagnetic induction meter*. North Dakota State University, Dept. Soil Sci. Res. Rpt. #30. 6pp.

Timpson, M.E., R.G. Thompson, and J.L. Arndt. 1987. *Geoarchaeological investigation of the Dahnke site: Red River Valley, North Dakota*. North Dakota Acad. Sci. Proc. 41:60.

Foss, J.E., J.L. Richardson, M.E. Timpson, J.L. Arndt, D.G. Hopkins, M.G. Michlovic, S.A. Ahler, and M.L. Gregg. 1986. *Pedological record of the Holocene in the Northern Great Plains as observed in some archaeological sites*. Agron. Abstr., p. 225.

Timpson, M.E., J.L. Arndt, and D.G. Hopkins. 1986. *Pedologic study of an archaeological site in the James River Valley; Stutsman County, North Dakota*. North Dakota State University, Department of Soil Sci. Res. Rpt. #21. 13pp.

Foss, J.E., J.L. Richardson, J.L. Arndt, M.E. Timpson, and M.G. Michlovic. 1985. *Pedologic study of archeological sites along the Red River*. North Dakota Acad. Sci. Proc. 39:51.

Selected Presentations

Invited Presentation: *Guidance for Scope and Effect and Hydrology (Well) Studies to support Wetland Delineation inb Minnesota and the Upper Midwest*. Minnesota Water Resources Conference, October 23-24, 2007. Earle Brown Heritage Center, Brooklyn Center, Minnesota.

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Invited Presentation: Land and Environmental Data Integration and Management. Geospatial information & Technology Association GIS for Oil and Gas Conference, September 24-26, 2007, Marriott Westchase Hotel, Houston TX.

Invited Presentation: Hydrogeology, Pedology, and Botany of the Seminary Calcareous Fen, Carver County, Minnesota. Minnesota Section American Institute of Professional Geologists, September 5, 2006, Minneapolis, Minnesota.

Invited Presentation: Redoximorphic features in hydric soils: Genesis, morphology and use in wetland delineation presented to the Minnesota Wetland Delineators Association Forum Series, January 2006, Wood River Nature Center, Richfield Minnesota

Invited Presentation: Monitoring the Health and Function of Existing, Impacted, and Restored Calcareous Fens. Presenter and member of Planning Committee. Calcareous Fen Forum: Long Term Management and Restoration of Hillslope Calcareous Fens, Rochester, Minnesota, April 13, 2005.

Invited Presentation: GIS Assessment of Soil Salinization Hazards Associated with the Restoration of Drained Wetlands in the Upper Basin of Devils Lake, North Dakota. Presented to the Symposium – Soils and Wetland Assessment II. 2004 Annual Meeting of the Soil Science Society of America, October 31-November 4, 2004, Seattle Washington.

Invited Presentation: Watchin' the Water Rise. Assessment of Soil Salinization Hazards, Devils Lake Flood Reduction Alternatives. University of Minnesota Department of Soil Science Seminar Series, December 9, 2002.

Invited Presentation: Is it Alive? Lessons Learned in Forensic Soil Investigation. 2002 Annual Winter Meeting, Minnesota Association of Professional Soil Scientists, December 6, 2002, Radisson Hotel, St. Cloud Minnesota.

Integrated Database Strategies for Wetland and Resource Assessments. 2000. 7th International Symposium on Environmental Concerns in Rights-of-Way Management. 9-13 September. Calgary, Alberta, Canada.

Invited Presentation: Fresh out-of-the Box: High Technology and the Creation of Detailed, User-friendly Soil Surveys presented to the Technology for Professionals Symposium, Division A-9, Professional Practitioners (Prov.), 2000 Annual Meeting of the Soil Science Society of America, November 5-9, Minneapolis, Minnesota

Teaching and Public Outreach. Invited presentations to address soil hydrology related topics as a guest lecturer for University of Minnesota, Department of Soil Science Wetland Soils class (Soil 5555), 1995 – 2005. Invited presentation to address general soil science issues, University of Minnesota, Department of Landscape Architecture, 2005. Invited presentation to Environmental Assessment Worksheet and Environmental Impact Statement preparation, April 2006, and April 2007.

Invited Presentation on Soil and Groundwater Chemistry in Calcareous Fens to the Minnesota Wetland Delineators Association Forum Series, December 6, 1999, City of Plymouth Council Chambers, Plymouth Minnesota.

Invited Presentation on High Tech Wetland Delineation Using GPS and GIS to the Minnesota Association of Professional Soil Scientists (MAPSS), December 4, 1998, St. Cloud, Minnesota.

Integrated database strategies for wetland and soil resource assessments. 1998 Annual Meeting of the Soil Science Society of America, October 18-22, 1998, Baltimore, Maryland.

Geostatistical assessment of jurisdictional wetlands on a drained Minnesota peatland. 19th Annual Meeting Society of Wetland Scientists, June 6-12, 1998, Anchorage Alaska.

Invited presentation on Problems associated with Salts and Chlorides in Soil, Salts/Chlorides session, Land Application of Biosolids, Residuals, and Effluents Conference, Minnesota Pollution Control Agency, Water Quality Division, Thunderbird Hotel & Convention Center, Bloomington, Minnesota, February 20, 1998.

Invited presentation on the Theory and Use of Drain Spacing equations to Estimate the Extent of Effective Wetland Drainage. Wetland Delineators Association Forum Series "Wetlands, Ditches, and Drainage" Minnesota Valley National Wildlife Refuge Headquarters, Bloomington, Minnesota, February 4, 1998.

Invited presentation on Selection, Use, and Application of Reference Wetlands for Hydrology Studies, Wetland Delineators Association Forum Series "The Role of Reference Wetlands in Wetland Inventories and Hydrology Studies" Maple Grove City Hall Council Chambers, Maple Grove, Minnesota, February 6, 1997.

Invited presentation on Applications of Hydric Soils Information to Jurisdictional Wetland Determinations: Issues and Examples to the 1996 annual winter meeting of The Minnesota Association of Professional Soil Scientists (MAPSS) meeting, Land O' Lakes Inc. Corporate Headquarters, Minneapolis, Minnesota, December 6, 1996.

Invited presentation on Hydric Soils, Wetland Delineators Association Forum Series, "Hydric Soils", Shoreview City Hall Council Chambers, Shoreview, Minnesota.

Invited presentation on Surface and subsurface controls on wetland hydrology to the Hydric Soil Identification for Wetland Soils Workshop, 1994 and 1995 annual meetings, Soil Science Society of America, Seattle WA, November 12-18, 1994, and October 29-November 3, 1995.

Invited presentation on Impacts of Ground Water Flow Systems on Hydric Soils in the Glaciated Northern Prairies of the United States to Hydric Soils Symposium, SSSA, Division S10 (prov.), 1993 Annual Meetings of the ASA-CSSA-SSSA.

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Effects of ground-water flow systems on hydric soils in two prairie wetlands in North Dakota to the Lake-Land Linkages Session, Hydrology Section, American Geophysical Union Annual Meeting held in San Francisco, Dec. 6-10, 1993.

Invited presentation on Geochemistry of hydric-soil salinity associated with wetlands in the subhumid prairie-pothole region, North Dakota, USA, 28th International Geological Congress, Washington, DC, July 9-19, 1989

Invited presentation on Characterizing and Monitoring Hydric Soils of the Pothole Region, EPA-EMAP (Environmental Monitoring and Assessment) workshop for the prairie pothole region, Northern Prairie Wildlife Research Center, Jamestown, ND, July 23-25, 1991.

Developed daylong field trip for the 45 participants of the 1992 meeting of the National Technical Committee for Hydric Soils, August 18, 1992. Prepared trip guidebook and acted as tourguide.

Table 1: Soil Limitations Along the Pipeline Centerline Mileposted by Soil Map Unit (continued)

Harding	290.931	291.031	0.100	529	SD063	355772	PbB	Parchin-Bullock fine sandy loams, 2 to 9 percent slopes	0.10	0.05	0.00	0.00	0.00	0.06	0.09	0.09	0.02			
Harding	291.031	291.187	0.156	823	SD063	355723	BpB	Bullock-Parchin-Slickspots complex, 2 to 9 percent slopes	0.14	0.06				0.12	0.12	0.14	0.00			
Harding	291.187	291.271	0.084	446	SD063	355805	TyC	Twilight-Parchin fine sandy loams, 6 to 15 percent slopes	0.08	0.07	0.00		0.00	0.03	0.03	0.03	0.03			
Harding	291.271	291.414	0.143	754	SD063	355724	BsA	Bullock-Slickspots complex, 0 to 4 percent slopes	0.13	0.02			0.00	0.12	0.13	0.14				
Harding	291.414	291.722	0.308	1,627	SD063	355741	GdA	Gerdrum silt loam, 0 to 4 percent slopes	0.02				0.03	0.28	0.31	0.31				
Harding	291.722	291.883	0.161	850	SD063	355751	Hg	Havre loam					0.15	0.01	0.16	0.16			0.16	0.00
Harding	291.883	292.058	0.174	921	SD063	355742	Ge	Glendive fine sandy loam					0.16	0.02	0.17	0.17			0.17	0.01
Harding	292.058	292.093	0.035	184	SD063	1013843	W	Water												
Harding	292.093	292.122	0.029	156	SD063	355729	CeE	Cabbart-Rock outcrop complex, 15 to 40 percent slopes	0.01	0.03			0.02		0.00	0.00	0.02	0.03	0.01	
Harding	292.122	292.438	0.316	1,670	SD063	355752	Hh	Havre-Harlake complex					0.27	0.03	0.30	0.30			0.32	0.03
Harding	292.438	292.460	0.022	115	SD063	355742	Ge	Glendive fine sandy loam					0.02	0.00	0.02	0.02			0.02	0.00
Harding	292.460	292.584	0.123	651	SD063	355729	CeE	Cabbart-Rock outcrop complex, 15 to 40 percent slopes	0.03	0.12			0.10	0.01	0.01	0.08	0.12	0.03		
Harding	292.584	292.822	0.238	1,258	SD063	355772	PbB	Parchin-Bullock fine sandy loams, 2 to 9 percent slopes	0.24	0.13	0.01		0.01	0.20	0.20	0.22	0.04			
Harding	292.822	293.265	0.443	2,340	SD063	355804	TxE	Twilight-Blackhall fine sandy loams, 9 to 25 percent slopes	0.42	0.29	0.11		0.11	0.04	0.16	0.09	0.18			
Harding	293.265	293.320	0.055	291	SD063	355803	TyC	Twilight fine sandy loam, 6 to 9 percent slopes	0.05	0.05	0.00		0.00	0.00	0.00	0.01	0.01			
Harding	293.320	293.847	0.527	3,312	SD063	355805	TyC	Twilight-Parchin fine sandy loams, 6 to 15 percent slopes	0.60	0.53	0.03		0.03	0.19	0.22	0.25	0.25			
Harding	293.847	293.964	0.116	95	SD063	355729	CeE	Cabbart-Rock outcrop complex, 15 to 40 percent slopes	0.00	0.02			0.01	0.00	0.00	0.02	0.02	0.00		
Harding	293.964	294.010	0.046	244	SD063	355805	TyC	Twilight-Parchin fine sandy loams, 6 to 15 percent slopes	0.04	0.04	0.01		0.00	0.01	0.02	0.02	0.02	0.00		
Harding	294.010	294.113	0.103	543	SD063	355729	CeE	Cabbart-Rock outcrop complex, 15 to 40 percent slopes	0.03	0.10	0.08		0.00	0.01	0.02	0.03	0.02	0.03		
Harding	294.113	294.119	0.006	33	SD063	355772	PbB	Parchin-Bullock fine sandy loams, 2 to 9 percent slopes	0.01	0.00	0.00		0.00	0.01	0.01	0.01	0.01	0.01	0.03	
Harding	294.119	294.204	0.085	450	SD063	355722	BoD	Bullock-Cabbart complex, 6 to 25 percent slopes	0.08	0.00	0.03	0.00		0.04	0.05	0.06	0.06			
Harding	294.204	294.257	0.053	280	SD063	355772	PbB	Parchin-Bullock fine sandy loams, 2 to 9 percent slopes	0.05	0.03	0.00		0.00	0.04	0.05	0.05	0.01			
Harding	294.257	294.288	0.031	164	SD063	355722	BoD	Bullock-Cabbart complex, 6 to 25 percent slopes	0.03		0.01	0.00		0.02	0.02	0.03	0.03			
Harding	294.288	294.351	0.063	333	SD063	355772	PbB	Parchin-Bullock fine sandy loams, 2 to 9 percent slopes	0.06	0.03	0.00		0.00	0.06	0.05	0.08	0.01			
Harding	294.351	294.403	0.051	272	SD063	355722	BoD	Bullock-Cabbart complex, 6 to 25 percent slopes	0.05		0.02	0.00		0.03	0.03	0.05	0.06			
Harding	294.403	294.519	0.116	611	SD063	355772	PbB	Parchin-Bullock fine sandy loams, 2 to 9 percent slopes	0.12	0.06	0.00		0.00	0.08	0.10	0.11	0.02			
Harding	294.519	294.614	0.096	506	SD063	355722	BoD	Bullock-Cabbart complex, 6 to 25 percent slopes	0.09		0.03	0.00		0.05	0.05	0.09	0.09			
Harding	294.614	294.680	0.066	349	SD063	355772	PbB	Parchin-Bullock fine sandy loams, 2 to 9 percent slopes	0.07	0.04	0.00		0.00	0.05	0.06	0.06	0.01			
Harding	294.680	294.997	0.316	1,670	SD063	355772	BoD	Bullock-Cabbart complex, 6 to 25 percent slopes	0.30		0.10	0.02		0.16	0.18	0.31	0.30			
Harding	294.997	295.077	0.081	426	SD063	355772	PbB	Parchin-Bullock fine sandy loams, 2 to 9 percent slopes	0.08	0.04	0.00		0.00	0.07	0.07	0.07	0.01			
Harding	295.077	295.116	0.139	735	SD063	355722	BoD	Bullock-Cabbart complex, 6 to 25 percent slopes	0.13		0.05	0.01		0.07	0.08	0.14	0.13			
Harding	295.116	295.346	0.129	681	SD063	355772	PbB	Parchin-Bullock fine sandy loams, 2 to 9 percent slopes	0.13	0.07	0.01		0.01	0.11	0.11	0.12	0.02			
Harding	295.346	295.423	0.078	411	SD063	355722	BoD	Bullock-Cabbart complex, 6 to 25 percent slopes	0.07		0.03	0.00		0.04	0.04	0.06	0.07			
Harding	295.423	295.545	0.121	641	SD063	355723	BpB	Bullock-Parchin-Slickspots complex, 2 to 9 percent slopes	0.11	0.05				0.10	0.10	0.11	0.00			
Harding	295.545	295.602	0.057	300	SD063	355772	PbB	Parchin-Bullock fine sandy loams, 2 to 9 percent slopes	0.06	0.03	0.00		0.00	0.05	0.05	0.05	0.01			
Harding	295.602	295.757	0.156	833	SD063	355723	BpB	Bullock-Parchin-Slickspots complex, 2 to 9 percent slopes	0.14	0.06				0.12	0.12	0.14	0.00			
Harding	295.757	296.084	0.326	1,724	SD063	355768	MpB	Marmarth-Parchin fine sandy loams, 2 to 6 percent slopes	0.33	0.08	0.02		0.02	0.09	0.11	0.28	0.04			
Harding	296.084	296.384	0.300	1,587	SD063	355772	PbB	Parchin-Bullock fine sandy loams, 2 to 9 percent slopes	0.30	0.16	0.01		0.01	0.25	0.28	0.28	0.05			
Harding	296.384	296.734	0.350	1,848	SD063	355805	TyC	Twilight-Parchin fine sandy loams, 6 to 15 percent slopes	0.33	0.30	0.02		0.02	0.11	0.12	0.14	0.14			
Harding	296.734	297.013	0.279	1,473	SD063	355722	BoD	Bullock-Cabbart complex, 6 to 25 percent slopes	0.26		0.09	0.01		0.14	0.16	0.27	0.26			
Harding	297.013	297.255	0.242	1,277	SD063	355772	PbB	Parchin-Bullock fine sandy loams, 2 to 9 percent slopes	0.24	0.13	0.01		0.01	0.20	0.21	0.23	0.04			
Harding	297.255	297.605	0.349	1,844	SD063	355722	BoD	Bullock-Cabbart complex, 6 to 25 percent slopes	0.33		0.12	0.02		0.16	0.20	0.34	0.33			
Harding	297.605	297.834	0.229	1,209	SD063	355712	AkA	Archin-Bullock fine sandy loams, 0 to 4 percent slopes		0.03			0.03	0.17	0.20	0.22				
Harding	297.834	297.962	0.129	680	SD063	355805	TyC	Twilight-Parchin fine sandy loams, 6 to 15 percent slopes	0.12	0.11	0.01		0.01	0.04	0.05	0.05	0.05			
Harding	297.962	298.037	0.075	397	SD063	355804	TxE	Twilight-Blackhall fine sandy loams, 9 to 25 percent slopes	0.07	0.05	0.02		0.02	0.01	0.03	0.02	0.03			
Harding	298.037	298.200	0.163	859	SD063	355805	TyC	Twilight-Parchin fine sandy loams, 6 to 15 percent slopes	0.15	0.14	0.01		0.01	0.05	0.06	0.07	0.07			
Harding	298.200	298.274	0.074	389	SD063	355768	MpB	Marmarth-Parchin fine sandy loams, 2 to 6 percent slopes	0.07	0.02	0.00		0.00	0.02	0.03	0.06	0.01			
Harding	298.274	298.498	0.224	1,132	SD063	355805	TyC	Twilight-Parchin fine sandy loams, 6 to 15 percent slopes	0.20	0.18	0.01		0.01	0.06	0.08	0.09	0.09			
Harding	298.498	299.094	0.605	3,197	SD063	355772	PbB	Parchin-Bullock fine sandy loams, 2 to 9 percent slopes	0.61	0.32	0.02		0.02	0.50	0.52	0.66	0.09			
Harding	299.094	299.175	0.082	431	SD063	355781	RmB	Rhame-Parchin fine sandy loams, 2 to 6 percent slopes	0.08	0.02	0.01		0.01	0.03	0.04	0.03	0.01			
Harding	299.175	299.605	0.429	2,268	SD063	355772	PbB	Parchin-Bullock fine sandy loams, 2 to 9 percent slopes	0.43	0.23	0.02		0.02	0.35	0.37	0.40	0.06			
Harding	299.605	299.736	0.132	696	SD063	355805	TyC	Twilight-Parchin fine sandy loams, 6 to 15 percent slopes	0.13	0.11	0.01		0.01	0.04	0.05	0.05	0.05			
Harding	299.736	299.782	0.046	241	SD063	355804	TxE	Twilight-Blackhall fine sandy loams, 9 to 25 percent slopes	0.04	0.03	0.01		0.01	0.00	0.02	0.01	0.02			
Harding	299.782	299.829	0.047	246	SD063	355805	TyC	Twilight-Parchin fine sandy loams, 6 to 15 percent slopes	0.04	0.04	0.00		0.00	0.01	0.02	0.02	0.02			
Harding	299.829	299.926	0.098	517	SD063	355781	RmB	Rhame-Parchin fine sandy loams, 2 to 6 percent slopes	0.10	0.02	0.01		0.01	0.03	0.04	0.03	0.01			
Harding	299.926	299.979	0.052	275	SD063	355772	PbB	Parchin-Bullock fine sandy loams, 2 to 9 percent slopes	0.05	0.03	0.00		0.00	0.04	0.04	0.05	0.01			
Harding	299.979	300.010	0.031	166	SD063	355781	RmB	Rhame-Parchin fine sandy loams, 2 to 6 percent slopes	0.03	0.01	0.00		0.00	0.01	0.01	0.01	0.00			
Harding	300.010	300.053	0.043	227	SD063	355772	PbB	Parchin-Bullock fine sandy loams, 2 to 9 percent slopes	0.04	0.02	0.00		0.00	0.04	0.04	0.04	0.01			
Harding	300.053	300.174	0.121	636	SD063	355787	SaA	Sage loam					0.11	0.03	0.12	0.12				0.10
Harding	300.174	300.235	0.061	322	SD063	355805	TyC	Twilight-Parchin fine sandy loams, 6 to 15 percent slopes	0.06	0.05	0.00		0.00	0.02	0.02	0.02	0.02			
Harding	300.235	300.359	0.125	658	SD063	355723	BpB	Bullock-Parchin-Slickspots complex, 2 to 9 percent slopes	0.11	0.05				0.10	0.10	0.11	0.00			
Harding	300.359	300.441	0.082	431	SD063	355787	SaA	Sage loam					0.08	0.00	0.08	0.08				0.07
Harding	300.441	300.744	0.303	1,602	SD063	355805	TyC	Twilight-Parchin fine sandy loams, 6 to 15 percent slopes	0.29	0.28	0.02		0.02	0.08	0.11	0.12	0.12			
Harding	300.744	300.826	0.082	432	SD063	355772	PbB	Parchin-Bullock fine sandy loams, 2 to 9 percent slopes	0.08	0.04	0.00		0.00	0.07	0.07	0.08	0.01			

Table 1: Soil Limitations Along the Pipeline Centerline Mileposted by Soil Map Unit (continued)

Harding	300.826	300.993	0.167	881	SD063	355804	TxE	Twilight-Blackhall fine sandy loams, 9 to 25 percent slopes	0.16	0.11	0.04	0.04	0.02	0.06	0.03	0.07
Harding	300.993	301.214	0.221	1,165	SD063	355805	TyC	Twilight-Parchin fine sandy loams, 6 to 15 percent slopes	0.21	0.19	0.01	0.01	0.07	0.08	0.09	0.09
Harding	301.214	301.276	0.062	328	SD063	355722	BoD	Bullock-Cabbart complex, 6 to 25 percent slopes	0.06	0.02	0.00	0.03	0.03	0.03	0.06	0.06
Harding	301.276	301.450	0.175	922	SD063	355722	PbB	Parchin-Bullock fine sandy loams, 2 to 9 percent slopes	0.17	0.09	0.01	0.01	0.14	0.15	0.16	0.03
Harding	301.450	301.538	0.088	464	SD063	355722	BoD	Bullock-Cabbart complex, 6 to 25 percent slopes	0.08	0.03	0.00	0.04	0.05	0.09	0.09	0.00
Harding	301.538	301.797	0.258	1,363	SD063	355723	BpB	Bullock-Parchin-Slickspots complex, 2 to 9 percent slopes	0.23	0.10			0.21	0.21	0.23	0.01
Harding	301.797	302.019	0.222	1,173	SD063	355781	RmB	Rhame-Parchin fine sandy loams, 2 to 6 percent slopes	0.22	0.06	0.02	0.02	0.08	0.10	0.08	0.02
Harding	302.019	302.214	0.195	1,031	SD063	355804	TxE	Twilight-Blackhall fine sandy loams, 9 to 25 percent slopes	0.19	0.13	0.05	0.05	0.02	0.07	0.04	0.08
Harding	302.214	302.696	0.482	2,546	SD063	355729	CeE	Cabbart-Rock outcrop complex, 15 to 40 percent slopes	0.12	0.47	0.38		0.04	0.04	0.31	0.46
Harding	302.696	302.726	0.029	155	SD063	355722	PbB	Parchin-Bullock fine sandy loams, 2 to 9 percent slopes	0.03	0.02	0.00	0.00	0.02	0.03	0.03	0.00
Harding	302.726	303.245	0.520	2,744	SD063	355805	TyC	Twilight-Parchin fine sandy loams, 6 to 15 percent slopes	0.49	0.44	0.03	0.03	0.18	0.18	0.21	0.21
Harding	303.245	303.396	0.151	798	SD063	355722	BoD	Bullock-Cabbart complex, 6 to 25 percent slopes	0.14	0.05	0.01		0.08	0.08	0.15	0.14
Harding	303.396	303.805	0.409	2,157	SD063	355804	TxE	Twilight-Blackhall fine sandy loams, 9 to 25 percent slopes	0.39	0.27	0.10	0.10	0.04	0.14	0.08	0.16
Harding	303.805	303.893	0.088	466	SD063	355805	TyC	Twilight-Parchin fine sandy loams, 6 to 15 percent slopes	0.08	0.07	0.00	0.00	0.03	0.03	0.04	0.04
Harding	303.893	304.121	0.228	1,205	SD063	355729	CeE	Cabbart-Rock outcrop complex, 15 to 40 percent slopes	0.06	0.22	0.18		0.02	0.02	0.15	0.22
Harding	304.121	304.251	0.130	686	SD063	355722	BoD	Bullock-Cabbart complex, 6 to 25 percent slopes	0.12	0.04	0.01	0.01	0.07	0.07	0.13	0.12
Harding	304.251	304.431	0.179	948	SD063	355722	PbB	Parchin-Bullock fine sandy loams, 2 to 9 percent slopes	0.18	0.10	0.01	0.01	0.15	0.15	0.17	0.03
Harding	304.431	304.601	0.170	898	SD063	355716	ATA	Asinniboine-Archin fine sandy loams, 0 to 3 percent slopes	0.01	0.10			0.06	0.06	0.17	0.01
Harding	304.601	304.668	0.067	356	SD063	355723	BpB	Bullock-Parchin-Slickspots complex, 2 to 9 percent slopes	0.06	0.03			0.05	0.05	0.06	0.00
Harding	304.668	304.869	0.201	1,060	SD063	355722	BoD	Bullock-Cabbart complex, 6 to 25 percent slopes	0.19	0.07	0.01		0.10	0.11	0.19	0.19
Harding	304.869	305.174	0.305	1,610	SD063	355723	BpB	Bullock-Parchin-Slickspots complex, 2 to 9 percent slopes	0.28	0.12			0.24	0.24	0.27	0.01
Harding	305.174	305.283	0.109	575	SD063	355805	TyC	Twilight-Parchin fine sandy loams, 6 to 15 percent slopes	0.10	0.09	0.01	0.01	0.03	0.04	0.04	0.04
Harding	305.283	305.360	0.078	410	SD063	355803	TyC	Twilight fine sandy loam, 6 to 9 percent slopes	0.08	0.07	0.00	0.00	0.00	0.01	0.01	0.01
Harding	305.360	305.474	0.114	601	SD063	355781	RmB	Rhame-Parchin fine sandy loams, 2 to 6 percent slopes	0.11	0.03	0.01	0.01	0.04	0.05	0.04	0.01
Harding	305.474	305.729	0.255	1,344	SD063	355803	TyC	Twilight fine sandy loam, 6 to 9 percent slopes	0.25	0.23	0.01	0.01	0.02	0.02	0.03	0.03
Harding	305.729	306.062	0.333	1,757	SD063	355781	RmB	Rhame-Parchin fine sandy loams, 2 to 6 percent slopes	0.33	0.08	0.03	0.03	0.12	0.15	0.12	0.03
Harding	306.062	306.512	0.451	2,380	SD063	355712	AKA	Archin-Bullock fine sandy loams, 0 to 4 percent slopes	0.06	0.06	0.05		0.34	0.39	0.42	0.00
Harding	306.512	306.541	0.028	150	SD063	355716	ATA	Asinniboine-Archin fine sandy loams, 0 to 3 percent slopes	0.00	0.02			0.01	0.01	0.03	0.00
Harding	306.541	306.717	0.176	932	SD063	355722	BoD	Bullock-Cabbart complex, 6 to 25 percent slopes	0.17	0.02	0.06	0.01	0.09	0.10	0.17	0.17
Harding	306.717	307.079	0.361	1,908	SD063	355781	RmB	Rhame-Parchin fine sandy loams, 2 to 6 percent slopes	0.36	0.09	0.04	0.04	0.13	0.16	0.13	0.04
Harding	307.079	307.185	0.106	562	SD063	355805	TyC	Twilight-Parchin fine sandy loams, 6 to 15 percent slopes	0.10	0.09	0.01	0.01	0.03	0.04	0.04	0.04
Harding	307.185	307.379	0.194	1,023	SD063	355722	PbB	Parchin-Bullock fine sandy loams, 2 to 9 percent slopes	0.19	0.10	0.01	0.01	0.16	0.17	0.18	0.03
Harding	307.379	307.494	0.116	610	SD063	355722	BoD	Bullock-Cabbart complex, 6 to 25 percent slopes	0.11	0.04	0.01	0.01	0.08	0.06	0.11	0.11
Harding	307.494	307.601	0.106	561	SD063	355722	PbB	Parchin-Bullock fine sandy loams, 2 to 9 percent slopes	0.11	0.06	0.00	0.00	0.09	0.09	0.10	0.02
Harding	307.601	307.830	0.229	1,208	SD063	355723	BpB	Bullock-Parchin-Slickspots complex, 2 to 9 percent slopes	0.21	0.09			0.18	0.18	0.20	0.01
Harding	307.830	307.947	0.118	623	SD063	355805	TyC	Twilight-Parchin fine sandy loams, 6 to 15 percent slopes	0.11	0.10	0.01	0.01	0.04	0.04	0.05	0.06
Harding	307.947	308.031	0.084	443	SD063	355722	PbB	Parchin-Bullock fine sandy loams, 2 to 9 percent slopes	0.08	0.04	0.00	0.00	0.07	0.07	0.08	0.01
Harding	308.031	308.108	0.076	403	SD063	355804	TxE	Twilight-Blackhall fine sandy loams, 9 to 25 percent slopes	0.07	0.05	0.02	0.02	0.01	0.03	0.02	0.03
Harding	308.108	308.620	0.512	2,703	SD063	355723	BpB	Bullock-Parchin-Slickspots complex, 2 to 9 percent slopes	0.47	0.20			0.41	0.41	0.45	0.02
Harding	308.620	308.670	0.051	267	SD063	355729	CeE	Cabbart-Rock outcrop complex, 15 to 40 percent slopes	0.01	0.05	0.04		0.00	0.00	0.03	0.05
Harding	308.670	308.772	0.102	536	SD063	355722	BoD	Bullock-Cabbart complex, 6 to 25 percent slopes	0.10	0.03	0.01	0.01	0.05	0.06	0.10	0.10
Harding	308.772	308.963	0.191	1,010	SD063	355768	MpB	Marmarth-Parchin fine sandy loams, 2 to 6 percent slopes	0.19	0.06	0.01	0.01	0.08	0.07	0.17	0.02
Harding	308.963	309.210	0.247	1,304	SD063	355722	BoD	Bullock-Cabbart complex, 6 to 25 percent slopes	0.23	0.08	0.08	0.01	0.13	0.14	0.24	0.23
Harding	309.210	309.420	0.210	1,109	SD063	355723	BpB	Bullock-Parchin-Slickspots complex, 2 to 9 percent slopes	0.19	0.08			0.17	0.17	0.18	0.01
Harding	309.420	309.575	0.155	818	SD063	355729	CeE	Cabbart-Rock outcrop complex, 15 to 40 percent slopes	0.04	0.15	0.12		0.01	0.01	0.10	0.15
Harding	309.575	310.006	0.431	2,274	SD063	355804	TxE	Twilight-Blackhall fine sandy loams, 9 to 25 percent slopes	0.41	0.28	0.11	0.11	0.04	0.15	0.09	0.17
Harding	310.006	310.105	0.100	526	SD063	355729	CeE	Cabbart-Rock outcrop complex, 15 to 40 percent slopes	0.02	0.10	0.08		0.01	0.01	0.06	0.03
Harding	310.105	310.305	0.199	1,053	SD063	355804	TxE	Twilight-Blackhall fine sandy loams, 9 to 25 percent slopes	0.19	0.13	0.05	0.05	0.02	0.07	0.04	0.06
Harding	310.305	310.564	0.260	1,371	SD063	355722	PbB	Parchin-Bullock fine sandy loams, 2 to 9 percent slopes	0.26	0.14	0.01	0.01	0.21	0.22	0.24	0.04
Harding	310.564	310.601	0.037	194	SD063	355718	Ba	Badlands	0.03	0.03	0.00	0.00	0.00	0.00	0.00	0.03
Harding	310.601	310.648	0.047	247	SD063	355723	BpB	Bullock-Parchin-Slickspots complex, 2 to 9 percent slopes	0.04	0.02			0.04	0.04	0.04	0.00
Harding	310.648	310.838	0.191	1,007	SD063	355805	TyC	Twilight-Parchin fine sandy loams, 6 to 15 percent slopes	0.18	0.16	0.01	0.01	0.08	0.07	0.08	0.08
Harding	310.838	311.140	0.301	1,591	SD063	355729	CeE	Cabbart-Rock outcrop complex, 15 to 40 percent slopes	0.08	0.29	0.24		0.02	0.02	0.19	0.08
Harding	311.140	311.419	0.278	1,475	SD063	355805	TyC	Twilight-Parchin fine sandy loams, 6 to 15 percent slopes	0.27	0.24	0.01	0.01	0.08	0.10	0.11	0.11
Harding	311.419	311.600	0.181	955	SD063	355722	PbB	Parchin-Bullock fine sandy loams, 2 to 9 percent slopes	0.18	0.10	0.01	0.01	0.15	0.16	0.17	0.03
Harding	311.600	311.884	0.284	1,500	SD063	355805	TyC	Twilight-Parchin fine sandy loams, 6 to 15 percent slopes	0.27	0.24	0.01	0.01	0.09	0.10	0.11	0.11
Harding	311.884	312.030	0.145	767	SD063	355722	PbB	Parchin-Bullock fine sandy loams, 2 to 9 percent slopes	0.15	0.08	0.01	0.01	0.12	0.12	0.14	0.02
Harding	312.030	312.666	0.636	3,359	SD063	355805	TyC	Twilight-Parchin fine sandy loams, 6 to 15 percent slopes	0.60	0.54	0.03	0.03	0.19	0.22	0.25	0.25
Harding	312.666	312.866	0.200	1,058	SD063	355722	PbB	Parchin-Bullock fine sandy loams, 2 to 9 percent slopes	0.20	0.11	0.01	0.01	0.18	0.17	0.19	0.03
Harding	312.866	313.152	0.286	1,511	SD063	355723	BpB	Bullock-Parchin-Slickspots complex, 2 to 9 percent slopes	0.26	0.11			0.23	0.23	0.25	0.01
Harding	313.152	313.314	0.161	851	SD063	355780	RmB	Rhame fine sandy loam, 2 to 6 percent slopes	0.16	0.01	0.01	0.01	0.02	0.02	0.02	0.01
Harding	313.314	313.372	0.059	310	SD063	355723	BpB	Bullock-Parchin-Slickspots complex, 2 to 9 percent slopes	0.05	0.02			0.05	0.06	0.06	0.00
Harding	313.372	313.514	0.142	749	SD063	355805	TyC	Twilight-Parchin fine sandy loams, 6 to 15 percent slopes	0.13	0.12	0.01	0.01	0.04	0.05	0.06	0.06
Harding	313.514	313.673	0.159	839	SD063	355804	TxE	Twilight-Blackhall fine sandy loams, 9 to 25 percent slopes	0.15	0.10	0.04	0.04	0.02	0.06	0.03	0.06

Table 1: Soil Limitations Along the Pipeline Centerline Mileposted by Soil Map Unit (continued)

Harding	313.673	313.773	0.100	529	SD063	355781	RmB	Rhame-Parchin fine sandy loams, 2 to 6 percent slopes	0.10	0.03	0.01	0.01	0.04	0.05	0.04	0.01			
Harding	313.773	313.869	0.096	504	SD063	355803	TwC	Twilight fine sandy loam, 6 to 9 percent slopes	0.09	0.09	0.00	0.00	0.01	0.01	0.01	0.01			
Harding	313.869	313.970	0.101	532	SD063	355781	RmB	Rhame-Parchin fine sandy loams, 2 to 6 percent slopes	0.10	0.03	0.01	0.01	0.04	0.05	0.04	0.01			
Harding	313.970	314.278	0.308	1,628	SD063	355805	TyC	Twilight-Parchin fine sandy loams, 6 to 15 percent slopes	0.29	0.28	0.02	0.02	0.09	0.11	0.12	0.12			
Harding	314.278	314.406	0.128	674	SD063	355803	TwC	Twilight fine sandy loam, 6 to 9 percent slopes	0.12	0.12	0.00	0.00	0.01	0.01	0.02	0.02			
Harding	314.406	314.696	0.291	1,535	SD063	355801	TtC	Trey-Fleak loamy fine sands, 2 to 15 percent slopes	0.29	0.28			0.05	0.05	0.05	0.22	0.05		
Harding	314.696	314.781	0.085	446	SD063	355805	TyC	Twilight-Parchin fine sandy loams, 6 to 15 percent slopes	0.08	0.07	0.00	0.00	0.03	0.03	0.03	0.03			
Harding	314.781	314.879	0.098	519	SD063	355804	TtE	Twilight-Blackhall fine sandy loams, 9 to 25 percent slopes	0.09	0.06	0.02	0.02	0.01	0.03	0.02	0.04			
Harding	314.879	314.912	0.033	174	SD063	355803	TwC	Twilight fine sandy loam, 6 to 9 percent slopes	0.03	0.03	0.00	0.00	0.00	0.00	0.00	0.00			
Harding	314.912	315.098	0.186	983	SD063	355780	RhB	Rhame fine sandy loam, 2 to 6 percent slopes	0.19	0.01	0.01	0.01	0.02	0.03	0.03	0.01			0.19
Harding	315.098	315.284	0.186	980	SD063	355786	MaB	Marmarth fine sandy loam, 2 to 6 percent slopes	0.19	0.01	0.01	0.01	0.01	0.02	0.17	0.01			0.19
Harding	315.284	315.342	0.058	307	SD063	355781	RmB	Rhame-Parchin fine sandy loams, 2 to 6 percent slopes	0.06	0.01	0.01	0.01	0.02	0.03	0.02	0.01			
Harding	315.342	315.462	0.121	636	SD063	355780	RhB	Rhame fine sandy loam, 2 to 6 percent slopes	0.12	0.01	0.01	0.01	0.01	0.02	0.02	0.01			0.12
Harding	315.462	315.579	0.117	616	SD063	355781	RmB	Rhame-Parchin fine sandy loams, 2 to 6 percent slopes	0.12	0.03	0.01	0.01	0.04	0.05	0.04	0.01			
Harding	315.579	315.866	0.287	1,514	SD063	355715	AsB	Asaninboine fine sandy loam, 3 to 6 percent slopes	0.28	0.24			0.03	0.03	0.29			0.29	
Harding	315.866	315.950	0.084	442	SD063	355772	PbB	Parchin-Bullock fine sandy loams, 2 to 9 percent slopes	0.08	0.04	0.00	0.00	0.07	0.07	0.08	0.01			
Harding	315.950	316.353	0.404	2,132	SD063	355803	TwC	Twilight fine sandy loam, 6 to 9 percent slopes	0.39	0.37	0.01	0.01	0.02	0.04	0.05	0.05			
Harding	316.353	316.591	0.238	1,256	SD063	355781	RmB	Rhame-Parchin fine sandy loams, 2 to 6 percent slopes	0.24	0.06	0.02	0.02	0.08	0.11	0.08	0.02			
Harding	316.591	316.739	0.148	782	SD063	355722	BoD	Bullock-Cabhart complex, 6 to 25 percent slopes	0.14	0.13	0.05	0.01	0.08	0.08	0.14	0.14			
Harding	316.739	317.243	0.504	2,659	SD063	355781	RmB	Rhame-Parchin fine sandy loams, 2 to 6 percent slopes	0.50	0.13	0.05	0.05	0.18	0.23	0.18	0.05			
Harding	317.243	317.508	0.260	1,375	SD063	355722	BoD	Bullock-Cabhart complex, 6 to 25 percent slopes	0.25	0.11	0.09	0.01	0.13	0.15	0.25	0.25			
Harding	317.503	317.780	0.276	1,458	SD063	355723	BpB	Bullock-Parchin-Bullock complex, 2 to 9 percent slopes	0.25	0.11	0.09	0.01	0.13	0.22	0.24	0.01			
Harding	317.780	318.027	0.247	1,306	SD063	355805	TyC	Twilight-Parchin fine sandy loams, 6 to 15 percent slopes	0.23	0.21	0.01	0.01	0.07	0.09	0.10	0.10			
Harding	318.027	318.040	0.014	72	SD063	355746	Ha	Hardy fine sandy loam				0.00	0.00	0.00	0.00				0.00
Harding	318.040	318.143	0.103	543	SD063	355748	Hd	Hardy-Doglegcreek fine sandy loams	0.00			0.04	0.01	0.05	0.02				0.04
Harding	318.143	318.359	0.216	1,142	SD063	355802	TvB	Trey-Parchin-Bullock complex, 2 to 9 percent slopes	0.21	0.18	0.01	0.01	0.09	0.10	0.10	0.10	0.01		
Harding	318.359	318.420	0.060	318	SD063	355819	ZbC	Zeona-Blownout land complex, 2 to 15 percent slopes	0.03	0.04	0.00	0.00	0.00	0.00	0.04	0.00			
Harding	318.420	318.544	0.124	656	SD063	355802	TvB	Trey-Parchin-Bullock complex, 2 to 9 percent slopes	0.12	0.09	0.00	0.00	0.05	0.06	0.06	0.05	0.00		
Harding	318.544	318.602	0.058	309	SD063	355819	ZbC	Zeona-Blownout land complex, 2 to 15 percent slopes	0.03	0.04	0.00	0.00	0.00	0.00	0.04	0.00			
Harding	318.602	318.820	0.217	1,147	SD063	355817	ZaB	Zeona loamy fine sand, 2 to 9 percent slopes	0.03	0.21			0.02	0.02	0.02	0.19	0.02		
Harding	318.820	319.486	0.666	3,518	SD063	355801	TtC	Trey-Fleak loamy fine sands, 2 to 15 percent slopes	0.67	0.61			0.11	0.11	0.50	0.11			
Harding	319.486	319.855	0.369	1,949	SD063	355818	ZaD	Zeona loamy fine sand, 9 to 25 percent slopes	0.07	0.35	0.33		0.04	0.04	0.04	0.31	0.37		
Harding	319.855	319.928	0.072	382	SD063	355801	TtC	Trey-Fleak loamy fine sands, 2 to 15 percent slopes	0.07	0.07			0.01	0.01	0.01	0.05	0.01		
Harding	319.928	320.009	0.081	428	SD063	355818	ZaD	Zeona loamy fine sand, 9 to 25 percent slopes	0.02	0.08	0.07		0.01	0.01	0.01	0.07	0.08		
Harding	320.009	320.064	0.055	293	SD063	355801	TtC	Trey-Fleak loamy fine sands, 2 to 15 percent slopes	0.06	0.05			0.01	0.01	0.01	0.04	0.01		
Harding	320.064	320.607	0.543	2,868	SD063	355818	ZaD	Zeona loamy fine sand, 9 to 25 percent slopes	0.11	0.52	0.49		0.05	0.05	0.05	0.46	0.54		
Harding	320.607	320.725	0.118	624	SD063	355817	ZaB	Zeona loamy fine sand, 2 to 9 percent slopes	0.02	0.11			0.01	0.01	0.01	0.11	0.01		
Harding	320.725	321.763	1.037	5,476	SD063	355803	TwC	Twilight fine sandy loam, 6 to 9 percent slopes	1.01	0.94	0.03	0.03	0.06	0.08	0.12	0.12	0.12		
Harding	321.763	321.809	0.047	248	SD063	355817	ZaB	Zeona loamy fine sand, 2 to 9 percent slopes	0.01	0.05			0.00	0.00	0.00	0.04	0.00		
Harding	321.809	321.875	0.066	347	SD063	355730	ChA	Chinook fine sandy loam, 0 to 3 percent slopes	0.06	0.06	0.00		0.01	0.01	0.01	0.00	0.07		
Harding	321.875	321.946	0.070	371	SD063	355817	ZaB	Zeona loamy fine sand, 2 to 9 percent slopes	0.01	0.07			0.01	0.01	0.01	0.06	0.01		
Harding	321.946	322.051	0.106	559	SD063	355780	RhB	Rhame fine sandy loam, 2 to 6 percent slopes	0.11	0.01	0.01	0.01	0.01	0.02	0.02	0.01			0.11
Harding	322.051	322.143	0.092	485	SD063	355730	ChA	Chinook fine sandy loam, 0 to 3 percent slopes	0.09	0.08	0.00		0.01	0.01	0.01	0.00	0.09		
Harding	322.143	322.637	0.494	2,608	SD063	355780	RhB	Rhame fine sandy loam, 2 to 6 percent slopes	0.49	0.02	0.02	0.02	0.05	0.07	0.07	0.02	0.00	0.49	
Harding	322.637	322.797	0.160	844	SD063	355731	ChA	Chinook-Ardin fine sandy loams, 0 to 3 percent slopes	0.10	0.02	0.05		0.06	0.06	0.07	0.01			
Harding	322.797	323.017	0.219	1,158	SD063	355730	ChA	Chinook fine sandy loam, 0 to 3 percent slopes	0.20	0.01	0.02		0.02	0.02	0.03	0.01	0.22		
Harding	323.017	323.108	0.092	486	SD063	355748	Hd	Hardy-Doglegcreek fine sandy loams	0.00			0.04	0.01	0.05	0.02				0.03
Harding	323.108	323.209	0.100	529	SD063	355817	ZaB	Zeona loamy fine sand, 2 to 9 percent slopes	0.02	0.10			0.01	0.01	0.01	0.09	0.01		
Harding	323.209	323.290	0.042	220	SD063	355819	ZbC	Zeona-Blownout land complex, 2 to 15 percent slopes	0.02	0.03			0.00	0.00	0.02	0.00			
Harding	323.290	323.315	0.065	343	SD063	355802	TvB	Trey-Parchin-Bullock complex, 2 to 9 percent slopes	0.06	0.05	0.00	0.00	0.03	0.03	0.03	0.00			
Harding	323.315	323.478	0.162	857	SD063	355749	He	Hardy-Slickspots complex	0.03	0.10		0.02	0.05	0.06	0.06	0.10			0.00
Harding	323.478	323.547	0.069	364	SD063	355817	ZaB	Zeona loamy fine sand, 2 to 9 percent slopes	0.01	0.07			0.01	0.01	0.06	0.01			
Harding	323.547	323.740	0.193	1,019	SD063	355740	FtE	Fleak-Trey-Rock outcrop complex, 15 to 50 percent slopes	0.04	0.19	0.14	0.15	0.02	0.02	0.12	0.17	0.04		
Harding	323.740	324.028	0.288	1,522	SD063	355800	TrB	Trey loamy fine sand, 2 to 9 percent slopes	0.28	0.28			0.02	0.02	0.27	0.02			
Harding	324.028	324.561	0.534	2,817	SD063	355740	FtE	Fleak-Trey-Rock outcrop complex, 15 to 50 percent slopes	0.11	0.53	0.37	0.43	0.05	0.05	0.05	0.32	0.48	0.11	
Harding	324.561	324.956	0.395	2,085	SD063	355819	ZbC	Zeona-Blownout land complex, 2 to 15 percent slopes	0.18	0.28			0.02	0.02	0.24	0.02			
Harding	324.956	325.176	0.220	1,160	SD063	355801	TtC	Trey-Fleak loamy fine sands, 2 to 15 percent slopes	0.22	0.20			0.04	0.04	0.16	0.04			
Harding	325.176	325.481	0.305	1,609	SD063	355740	FtE	Fleak-Trey-Rock outcrop complex, 15 to 50 percent slopes	0.06	0.30	0.21	0.24	0.03	0.03	0.03	0.18	0.27	0.06	
Harding	325.481	325.567	0.086	454	SD063	355803	TwC	Twilight fine sandy loam, 6 to 9 percent slopes	0.08	0.08	0.00	0.00	0.01	0.01	0.01	0.01			
Harding	325.567	325.619	0.052	273	SD063	355781	RmB	Rhame-Parch											

Table 1: Soil Limitations Along the Pipeline Centerline Mileposted by Soil Map Unit (continued)

Harding	326.416	326.663	0.248	1,309	SD063	355716	ALA	Assiniboine-Archin fine sandy loams, 0 to 3 percent slopes	0.01	0.14			0.09	0.09	0.25			0.02
Harding	326.663	326.702	0.039	205	SD063	355781	RmB	Rhame-Parchin fine sandy loams, 2 to 6 percent slopes	0.04	0.01	0.00		0.00	0.01	0.02	0.01		0.00
Harding	326.702	326.875	0.172	911	SD063	355715	AsB	Assiniboine fine sandy loam, 3 to 6 percent slopes		0.15				0.02	0.02	0.17		0.17
Harding	326.875	326.908	0.033	174	SD063	355716	ALA	Assiniboine-Archin fine sandy loams, 0 to 3 percent slopes	0.00	0.02				0.01	0.01	0.03		0.00
Harding	326.908	327.167	0.259	1,368	SD063	355772	PbB	Parchin-Bullock fine sandy loams, 2 to 9 percent slopes	0.26	0.14	0.01		0.01	0.21	0.22	0.24		0.04
Harding	327.167	327.366	0.199	1,050	SD063	355781	RmB	Rhame-Parchin fine sandy loams, 2 to 6 percent slopes	0.20	0.05	0.02		0.02	0.07	0.09	0.07		0.02
Harding	327.366	327.625	0.259	1,367	SD063	355780	RhB	Rhame fine sandy loam, 2 to 6 percent slopes	0.26	0.01	0.01		0.01	0.03	0.04	0.04		0.26
Harding	327.625	327.724	0.099	525	SD063	355772	PbB	Parchin-Bullock fine sandy loams, 2 to 9 percent slopes	0.10	0.05	0.00		0.00	0.06	0.09	0.09		0.01
Harding	327.724	328.152	0.428	2,261	SD063	355780	RhB	Rhame fine sandy loam, 2 to 6 percent slopes	0.43	0.02	0.02		0.02	0.04	0.06	0.06		0.43
Harding	328.152	328.202	0.050	265	SD063	355712	AKA	Archin-Bullock fine sandy loams, 0 to 4 percent slopes		0.01		0.01		0.04	0.04	0.05		
Harding	328.202	328.373	0.170	898	SD063	355741	GdA	Gerdrum silt loam, 0 to 4 percent slopes	0.01				0.02	0.15	0.17	0.17		
Harding	328.373	328.390	0.018	94	SD063	355712	AKA	Archin-bullock fine sandy loams, 0 to 4 percent slopes		0.00		0.00		0.01	0.02	0.02		
Harding	328.390	328.397	0.007	38	SD063	355741	GdA	Gerdrum silt loam, 0 to 4 percent slopes	0.00				0.00	0.01	0.01	0.01		
Harding	328.397	328.514	0.117	617	SD063	355722	BoD	Bullock-Cabbart complex, 6 to 25 percent slopes	0.11		0.04		0.01	0.06	0.07	0.11		0.11
Harding	328.514	328.581	0.067	355	SD063	355756	Xe	Korchea loam		0.06			0.00	0.01	0.01	0.07		0.07
Harding	328.581	328.945	0.363	1,918	SD063	355722	BoD	Bullock-Cabbart complex, 6 to 25 percent slopes	0.35		0.02		0.02	0.19	0.20	0.35		0.35
Harding	328.945	329.068	0.123	651	SD063	355729	CeE	Cabbart-Rock outcrop complex, 15 to 40 percent slopes	0.03	0.12		0.10		0.01	0.01	0.08	0.12	0.03
Harding	329.068	329.131	0.063	331	SD063	355772	PbB	Parchin-Bullock fine sandy loams, 2 to 9 percent slopes	0.06	0.03	0.00		0.00	0.05	0.05	0.06		0.01
Harding	329.131	329.207	0.076	401	SD063	355729	CeE	Cabbart-Rock outcrop complex, 15 to 40 percent slopes	0.02	0.07		0.06		0.01	0.01	0.05		0.02
Harding	329.207	329.335	0.128	677	SD063	355723	BpB	Bullock-Parchin-Slickspots complex, 2 to 9 percent slopes	0.12	0.05				0.10	0.10	0.11		0.00
Harding	329.335	329.483	0.148	782	SD063	355772	PbB	Parchin-Bullock fine sandy loams, 2 to 9 percent slopes	0.15	0.08	0.01		0.01	0.12	0.13	0.14		0.02
Harding	329.483	329.646	0.164	863	SD063	355723	BpB	Bullock-Parchin-Slickspots complex, 2 to 9 percent slopes	0.15	0.06				0.13	0.13	0.14		0.00
Harding	329.646	329.693	0.047	247	SD063	355772	PbB	Parchin-Bullock fine sandy loams, 2 to 9 percent slopes	0.05	0.02	0.00		0.00	0.04	0.04	0.04		0.01
Harding	329.693	329.761	0.068	360	SD063	355723	BpB	Bullock-Parchin-Slickspots complex, 2 to 9 percent slopes	0.06	0.03				0.05	0.05	0.06		0.00
Harding	329.761	329.839	0.078	411	SD063	355772	PbB	Parchin-Bullock fine sandy loams, 2 to 9 percent slopes	0.08	0.04	0.00		0.00	0.06	0.07	0.07		0.01
Harding	329.839	330.339	0.500	2,638	SD063	355723	BpB	Bullock-Parchin-Slickspots complex, 2 to 9 percent slopes	0.45	0.19				0.40	0.40	0.44		0.01
Harding	330.339	330.405	0.067	352	SD063	355805	TyC	Twilight-Parchin fine sandy loams, 6 to 15 percent slopes	0.06	0.06	0.00		0.00	0.02	0.02	0.03		0.03
Harding	330.405	330.429	0.023	122	SD063	355712	AKA	Archin-Bullock fine sandy loams, 0 to 4 percent slopes		0.00		0.00		0.02	0.02	0.02		
Harding	330.429	330.457	0.029	152	SD063	355723	BpB	Bullock-Parchin-Slickspots complex, 2 to 9 percent slopes	0.03	0.01				0.02	0.02	0.03		0.00
Harding	330.457	330.628	0.171	904	SD063	355712	AKA	Archin-Bullock fine sandy loams, 0 to 4 percent slopes		0.02		0.02		0.13	0.15	0.16		
Harding	330.628	330.731	0.103	543	SD063	355722	BoD	Bullock-Cabbart complex, 6 to 25 percent slopes	0.10		0.03			0.05	0.06	0.10		0.10
Harding	330.731	330.854	0.123	650	SD063	355712	AKA	Archin-Bullock fine sandy loams, 0 to 4 percent slopes		0.02		0.01		0.09	0.11	0.12		
Harding	330.854	330.948	0.093	492	SD063	355727	CeE	Cabbart loam, 6 to 60 percent slopes, extremely stony	0.09	0.00	0.07	0.07		0.01	0.08	0.09		0.09
Harding	330.948	331.053	0.105	554	SD063	355768	MpB	Marmarth-Parchin fine sandy loams, 2 to 6 percent slopes	0.10	0.03	0.01	0.01	0.01	0.03	0.04	0.09		0.01
Harding	331.053	331.539	0.486	2,567	SD063	355773	BpB	Bullock-Parchin-Slickspots complex, 2 to 9 percent slopes	0.44	0.19				0.39	0.39	0.43		0.01
Harding	331.539	331.846	0.308	1,624	SD063	355722	BoD	Bullock-Cabbart complex, 6 to 25 percent slopes	0.29		0.10	0.02		0.16	0.17	0.30		0.29
Harding	331.846	332.259	0.412	2,177	SD063	355799	ToC	Tanna-Rhoades complex, 2 to 9 percent slopes	0.41				0.33	0.14	0.37	0.41		0.41
Harding	332.259	332.524	0.265	1,399	SD063	355772	PbB	Parchin-Bullock fine sandy loams, 2 to 9 percent slopes	0.26	0.14	0.01		0.01	0.22	0.23	0.25		0.04
Harding	332.524	332.577	0.053	280	SD063	355722	BoD	Bullock-Cabbart complex, 6 to 25 percent slopes	0.05		0.02	0.00		0.03	0.03	0.05		0.05
Harding	332.577	333.068	0.491	2,593	SD063	355723	BpB	Bullock-Parchin-Slickspots complex, 2 to 9 percent slopes	0.45	0.19				0.39	0.39	0.43		0.01
Harding	333.068	333.101	0.033	174	SD063	355772	PbB	Parchin-Bullock fine sandy loams, 2 to 9 percent slopes	0.03	0.02	0.00		0.00	0.03	0.03	0.03		0.00
Harding	333.101	333.131	0.031	161	SD063	355723	BpB	Bullock-Parchin-Slickspots complex, 2 to 9 percent slopes	0.03	0.01				0.02	0.02	0.03		0.00
Harding	333.131	333.339	0.208	1,098	SD063	355772	PbB	Parchin-Bullock fine sandy loams, 2 to 9 percent slopes	0.21	0.11	0.01		0.01	0.17	0.18	0.19		0.03
Harding	333.339	333.589	0.249	1,316	SD063	355768	MpB	Marmarth-Parchin fine sandy loams, 2 to 6 percent slopes	0.25	0.07	0.01		0.01	0.07	0.08	0.22		0.03
Harding	333.589	333.659	0.071	374	SD063	355723	BpB	Bullock-Parchin-Slickspots complex, 2 to 9 percent slopes	0.06	0.03				0.06	0.06	0.06		0.00
Harding	333.659	333.745	0.086	453	SD063	355768	MpB	Marmarth-Parchin fine sandy loams, 2 to 6 percent slopes	0.09	0.02	0.00		0.00	0.02	0.03	0.07		0.01
Harding	333.745	333.901	0.155	821	SD063	355770	MtD	Marmarth-Twilight fine sandy loams, 9 to 15 percent slopes	0.16	0.06	0.01		0.01	0.02	0.06	0.09		0.11
Harding	333.901	334.072	0.172	906	SD063	355805	TyC	Twilight-Parchin fine sandy loams, 6 to 15 percent slopes	0.16	0.15	0.01		0.01	0.05	0.06	0.07		0.07
Harding	334.072	334.170	0.098	516	SD063	355729	CeE	Cabbart-Rock outcrop complex, 15 to 40 percent slopes	0.02	0.09		0.08		0.01	0.01	0.06		0.03
Harding	334.170	334.235	0.065	341	SD063	355781	RmB	Rhame-Parchin fine sandy loams, 2 to 6 percent slopes	0.06	0.02	0.01		0.01	0.02	0.03	0.02		0.01
Harding	334.235	334.389	0.154	813	SD063	355723	BpB	Bullock-Parchin-Slickspots complex, 2 to 9 percent slopes	0.14	0.06				0.12	0.14	0.20		0.00
Harding	334.389	334.489	0.101	532	SD063	355805	TyC	Twilight-Parchin fine sandy loams, 6 to 15 percent slopes	0.10	0.09	0.01		0.01	0.03	0.04	0.04		0.04
Harding	334.489	334.537	0.048	252	SD063	355772	PbB	Parchin-Bullock fine sandy loams, 2 to 9 percent slopes	0.05	0.03	0.00		0.00	0.04	0.04	0.04		0.01
Harding	334.537	335.651	1.114	5,881	SD063	355805	TyC	Twilight-Parchin fine sandy loams, 6 to 15 percent slopes	1.06	0.95	0.06		0.06	0.33	0.38	0.45		0.45
Harding	335.651	335.747	0.096	508	SD063	355804	TxE	Twilight-Blackhall fine sandy loams, 9 to 25 percent slopes	0.09	0.06	0.02		0.02	0.01	0.03	0.02		0.04
Harding	335.747	335.884	0.137	724	SD063	355805	TyC	Twilight-Parchin fine sandy loams, 6 to 15 percent slopes	0.13	0.12	0.01		0.01	0.04	0.05	0.06		0.06
Harding	335.884	336.030	0.146	770	SD063	355804	TxE	Twilight-Blackhall fine sandy loams, 9 to 25 percent slopes	0.14	0.09	0.04		0.04	0.01	0.05	0.03		0.06
Harding	336.030	336.193	0.162	857	SD063	355805	TyC	Twilight-Parchin fine sandy loams, 6 to 15 percent slopes	0.15	0.14	0.01		0.01	0.05	0.06	0.06		0.06
Harding	336.193	336.348	0.156	821	SD063	355772	PbB	Parchin-Bullock fine sandy loams, 2 to 9 percent slopes	0.16	0.08	0.01		0.01	0.13	0.13	0.14		0.02
Harding	336.348	336.526	0.178	938	SD063	355773	BpB	Bullock-Parchin-Slickspots complex, 2 to 9 percent slopes	0.16	0.07				0.14	0.14	0.18		0.01
Harding	336.526	336.626	0.100	530	SD063	355804	TxE	Twilight-Blackhall fine sandy loams, 9 to 25 percent slopes	0.10	0.07	0.03		0.03	0.01	0.04	0.02		0.04
Harding	336.626	336.792	0.165	873	SD063	355805	TyC	Twilight-Parchin fine sandy loams, 6 to 15 percent slopes	0.16	0.14	0.01		0.					

Table 1: Soil Limitations Along the Pipeline Centerline Mileposted by Soil Map Unit (continued)

Harding	337.122	337.207	0.084	446	SD063	355768	MpB	Marmarth-Parchin fine sandy loams, 2 to 6 percent slopes	0.08	0.02	0.00	0.00	0.02	0.03	0.07	0.01			
Harding	337.207	337.346	0.140	737	SD063	355772	PbB	Parchin-Bullock fine sandy loams, 2 to 9 percent slopes	0.14	0.07	0.01	0.01	0.11	0.12	0.13	0.02			
Harding	337.346	337.425	0.079	418	SD063	355768	MpB	Marmarth-Parchin fine sandy loams, 2 to 6 percent slopes	0.08	0.02	0.00	0.00	0.02	0.03	0.07	0.01			
Harding	337.425	337.546	0.120	635	SD063	355772	PbB	Parchin-Bullock fine sandy loams, 2 to 9 percent slopes	0.12	0.06	0.00	0.00	0.10	0.10	0.11	0.02			
Harding	337.546	337.973	0.427	2,256	SD063	355741	GdA	Gerdrum silt loam, 0 to 4 percent slopes	0.02			0.04	0.38	0.43	0.43				
Harding	337.973	338.069	0.096	508	SD063	355805	TyC	Twilight-Parchin fine sandy loams, 6 to 15 percent slopes	0.09	0.08	0.00	0.00	0.03	0.03	0.04	0.04			
Harding	338.069	338.237	0.168	887	SD063	355741	GdA	Gerdrum silt loam, 0 to 4 percent slopes	0.01			0.02	0.15	0.17	0.17				
Harding	338.237	338.405	0.168	885	SD063	355772	PbB	Parchin-Bullock fine sandy loams, 2 to 9 percent slopes	0.17	0.09	0.01	0.01	0.14	0.14	0.16	0.03			
Harding	338.405	338.544	0.139	735	SD063	355728	CdE	Cabbart-DeRidge loams, 15 to 40 percent slopes	0.14	0.00	0.11		0.01	0.01	0.12	0.13	0.00		
Harding	338.544	338.714	0.171	901	SD063	355757	Kg	Korchea loam, channelled				0.02	0.01	0.03	0.16				0.01
Harding	338.714	338.814	0.099	523	SD063	355781	RmB	Rhame-Parchin fine sandy loams, 2 to 6 percent slopes	0.10	0.02	0.01	0.01	0.03	0.04	0.03	0.01			
Harding	338.814	338.952	0.139	731	SD063	355723	BpB	Bullock-Parchin-Slickspots complex, 2 to 9 percent slopes	0.13	0.05			0.11	0.11	0.12	0.01			
Harding	338.952	339.045	0.093	492	SD063	355781	RmB	Rhame-Parchin fine sandy loams, 2 to 6 percent slopes	0.09	0.02	0.01	0.01	0.03	0.04	0.03	0.01			
Harding	339.045	339.251	0.205	1,084	SD063	355716	AsA	Assiniboine-Archin fine sandy loams, 0 to 3 percent slopes	0.01	0.12			0.06	0.08	0.21		0.01		
Harding	339.251	339.440	0.189	1,000	SD063	355741	GdA	Gerdrum silt loam, 0 to 4 percent slopes	0.01			0.02	0.17	0.19	0.19				
Harding	339.440	339.527	0.087	459	SD063	355714	AsA	Assiniboine fine sandy loam, 0 to 3 percent slopes		0.07		0.00	0.01	0.01	0.09			0.09	
Harding	339.527	339.630	0.103	546	SD063	355752	Hh	Havre-Marlake complex				0.09	0.01	0.10	0.10			0.10	0.01
Harding	339.630	339.710	0.080	421	SD063	355781	RmB	Rhame-Parchin fine sandy loams, 2 to 6 percent slopes	0.08	0.02	0.01	0.01	0.03	0.04	0.03	0.01			
Harding	339.710	340.008	0.298	1,573	SD063	355716	AsA	Assiniboine-Archin fine sandy loams, 0 to 3 percent slopes	0.02	0.17			0.11	0.11	0.30			0.02	
Harding	340.008	340.190	0.182	962	SD063	355712	AsA	Archin-Bullock fine sandy loams, 0 to 4 percent slopes	0.02	0.02		0.02	0.14	0.16	0.17				
Harding	340.190	340.440	0.250	1,320	SD063	355722	BoD	Bullock-Cabbart complex, 6 to 25 percent slopes	0.24		0.06	0.01	0.13	0.14	0.24				0.24
Harding	340.440	340.577	0.137	722	SD063	355805	TyC	Twilight-Parchin fine sandy loams, 6 to 15 percent slopes	0.13	0.12	0.01	0.01	0.04	0.05	0.05	0.05			0.05
Harding	340.577	340.610	0.033	174	SD063	355772	PbB	Parchin-Bullock fine sandy loams, 2 to 9 percent slopes	0.03	0.02	0.00	0.00	0.03	0.03	0.03	0.00			0.00
Harding	340.610	340.658	0.048	253	SD063	355805	TyC	Twilight-Parchin fine sandy loams, 6 to 15 percent slopes	0.05	0.04	0.00	0.00	0.01	0.02	0.02	0.02			0.02
Harding	340.658	340.718	0.061	319	SD063	355772	PbB	Parchin-Bullock fine sandy loams, 2 to 9 percent slopes	0.06	0.03	0.00	0.00	0.05	0.05	0.06	0.01			0.01
Harding	340.718	340.773	0.055	291	SD063	355712	AsA	Archin-Bullock fine sandy loams, 0 to 4 percent slopes	0.01	0.01		0.01	0.04	0.05	0.06				
Harding	340.773	340.881	0.106	568	SD063	355772	PbB	Parchin-Bullock fine sandy loams, 2 to 9 percent slopes	0.11	0.06	0.00	0.00	0.09	0.09	0.10	0.02			0.02
Harding	340.881	341.605	0.724	3,822	SD063	355712	AsA	Archin-Bullock fine sandy loams, 0 to 4 percent slopes	0.09			0.09	0.54	0.63	0.68				
Harding	341.605	341.664	0.059	310	SD063	355716	AsA	Assiniboine-Archin fine sandy loams, 0 to 3 percent slopes	0.00	0.03			0.02	0.02	0.06			0.00	
Harding	341.664	341.727	0.063	333	SD063	355712	AsA	Archin-Bullock fine sandy loams, 0 to 4 percent slopes	0.01	0.01		0.01	0.05	0.05	0.06				
Harding	341.727	341.830	0.109	545	SD063	355714	AsA	Assiniboine fine sandy loam, 0 to 3 percent slopes	0.09			0.01	0.01	0.02	0.10				0.10
Harding	341.830	341.993	0.163	861	SD063	355712	AsA	Archin-Bullock fine sandy loams, 0 to 4 percent slopes	0.02	0.02		0.02	0.12	0.14	0.15				
Harding	341.993	342.073	0.080	421	SD063	355723	BpB	Bullock-Parchin-Slickspots complex, 2 to 9 percent slopes	0.07	0.03			0.06	0.06	0.07	0.00			
Harding	342.073	342.156	0.083	440	SD063	355712	AsA	Archin-Bullock fine sandy loams, 0 to 4 percent slopes	0.01			0.01	0.06	0.07	0.08				
Harding	342.156	342.271	0.116	610	SD063	355722	BoD	Bullock-Cabbart complex, 6 to 25 percent slopes	0.11		0.04	0.01	0.06	0.06	0.11	0.11			
Harding	342.271	342.380	0.108	572	SD063	355724	BsA	Bullock-Slickspots complex, 0 to 4 percent slopes	0.10	0.01		0.00	0.09	0.10	0.10				
Harding	342.380	342.570	0.190	1,003	SD063	355768	MpB	Marmarth-Parchin fine sandy loams, 2 to 6 percent slopes	0.19	0.08	0.01	0.01	0.06	0.06	0.17				0.02
Harding	342.570	342.819	0.250	1,318	SD063	355772	PbB	Parchin-Bullock fine sandy loams, 2 to 9 percent slopes	0.25	0.13	0.01	0.01	0.20	0.21	0.23				0.04
Harding	342.819	342.938	0.118	625	SD063	355723	BpB	Bullock-Parchin-Slickspots complex, 2 to 9 percent slopes	0.11	0.05			0.08	0.09	0.10				0.00
Harding	342.938	343.150	0.213	1,123	SD063	355772	PbB	Parchin-Bullock fine sandy loams, 2 to 9 percent slopes	0.21	0.11	0.01	0.01	0.17	0.18	0.20	0.03			
Harding	343.150	343.277	0.126	668	SD063	355805	TyC	Twilight-Parchin fine sandy loams, 6 to 15 percent slopes	0.12	0.11	0.01	0.01	0.04	0.04	0.05	0.05			0.05
Harding	343.277	343.690	0.413	2,182	SD063	355716	AsA	Assiniboine-Archin fine sandy loams, 0 to 3 percent slopes	0.02	0.24			0.16	0.15	0.41			0.03	
Harding	343.690	343.749	0.059	313	SD063	355772	PbB	Parchin-Bullock fine sandy loams, 2 to 9 percent slopes	0.06	0.03	0.00	0.00	0.05	0.05	0.06	0.01			0.01
Harding	343.749	343.836	0.087	458	SD063	355781	RmB	Rhame-Parchin fine sandy loams, 2 to 6 percent slopes	0.09	0.02	0.01	0.01	0.03	0.04	0.03	0.01			
Harding	343.836	344.091	0.255	1,346	SD063	355723	BpB	Bullock-Parchin-Slickspots complex, 2 to 9 percent slopes	0.23	0.10			0.20	0.20	0.22	0.01			0.01
Harding	344.091	344.149	0.058	306	SD063	355803	TwC	Twilight fine sandy loam, 6 to 9 percent slopes	0.06	0.05	0.00	0.00	0.00	0.01	0.01	0.01			
Harding	344.149	344.414	0.265	1,398	SD063	355772	PbB	Parchin-Bullock fine sandy loams, 2 to 9 percent slopes	0.26	0.14	0.01	0.01	0.22	0.23	0.25	0.04			0.04
Harding	344.414	344.423	0.010	51	SD063	355723	BpB	Bullock-Parchin-Slickspots complex, 2 to 9 percent slopes	0.01	0.00			0.01	0.01	0.01	0.00			
Harding	344.423	344.625	0.202	1,067	SD063	355772	PbB	Parchin-Bullock fine sandy loams, 2 to 9 percent slopes	0.20	0.11	0.01	0.01	0.17	0.17	0.19	0.03			0.03
Harding	344.625	344.684	0.059	310	SD063	355803	TwC	Twilight fine sandy loam, 6 to 9 percent slopes	0.06	0.05	0.00	0.00	0.00	0.01	0.01	0.01			
Harding	344.684	344.917	0.233	1,232	SD063	355772	PbB	Parchin-Bullock fine sandy loams, 2 to 9 percent slopes	0.23	0.12	0.01	0.01	0.19	0.20	0.22	0.03			0.03
Harding	344.917	344.999	0.082	432	SD063	355781	RmB	Rhame-Parchin fine sandy loams, 2 to 6 percent slopes	0.08	0.02	0.01	0.01	0.03	0.04	0.03	0.01			
Harding	344.999	345.192	0.193	1,021	SD063	355805	TyC	Twilight-Parchin fine sandy loams, 6 to 15 percent slopes	0.18	0.16	0.01	0.01	0.06	0.07	0.08	0.08			0.08
Harding	345.192	345.338	0.146	771	SD063	355730	ChA	Chinook fine sandy loam, 0 to 3 percent slopes	0.13			0.00	0.01	0.02	0.02			0.01	0.15
Harding	345.338	345.468	0.129	682	SD063	355805	TyC	Twilight-Parchin fine sandy loams, 6 to 15 percent slopes	0.12	0.11	0.01	0.01	0.04	0.05	0.05	0.05			0.05
Harding	345.468	346.286	0.818	4,321	SD063	355781	RmB	Rhame-Parchin fine sandy loams, 2 to 6 percent slopes	0.82	0.20	0.08	0.08	0.29	0.37	0.29	0.06			0.06
Harding	346.286	346.338	0.052	273	SD063	355723	BpB	Bullock-Parchin-Slickspots complex, 2 to 9 percent slopes	0.05	0.02			0.04	0.04	0.05	0.00			
Harding	346.338	346.362	0.024	126	SD063	355724	BsA	Bullock-Slickspots complex, 0 to 4 percent slopes	0.02	0.00		0.00	0.02	0.02	0.02				
Harding	346.362	346.514	0.153	806	SD063	355723	BpB	Bullock-Parchin-Slickspots complex, 2 to 9 percent slopes	0.14	0.08			0.12	0.12	0.13	0.00			
Harding	346.514	346.649	0.135	714	SD063	355724	BsA	Bullock-Slickspots complex, 0 to 4 percent slopes	0.13	0.01		0.00	0.11	0.12	0.13				

Table 1: Soil Limitations Along the Pipeline Centerline Mileposted by Soil Map Unit (continued)

Butte	354.948	355.240	0.292	1,541	SD019	353147	Bd	badland		0.27	0.03	0.24		0.01	0.01		0.02	0.05		0.27	0.22	
Butte	355.240	355.653	0.412	2,178	SD019	353242	SnB	Sorum fine sandy loam, 0 to 6 percent slopes			0.04				0.35		0.35	0.37				
Butte	355.653	355.716	0.063	332	SD019	353141	AnA	Archin-Slickspots complex, 0 to 3 percent slopes		0.02	0.00				0.06		0.06	0.06				
Butte	355.716	355.913	0.197	1,042	SD019	353249	TYD	Twilight fine sandy loam, 3 to 25 percent slopes		0.15	0.16	0.14	0.02	0.01		0.03		0.04	0.04		0.17	
Butte	355.913	356.233	0.320	1,690	SD019	353242	SnB	Sorum fine sandy loam, 0 to 6 percent slopes			0.03					0.27		0.27	0.29			
Butte	356.233	356.292	0.059	313	SD019	353251	ThD	Twilight-Blackhall fine sandy loams, 6 to 18 percent slopes		0.05	0.03	0.03	0.00	0.02		0.00		0.02	0.01		0.06	
Butte	356.292	356.408	0.116	610	SD019	353242	SnB	Sorum fine sandy loam, 0 to 6 percent slopes			0.01				0.10		0.10	0.10				
Butte	356.408	356.505	0.097	513	SD019	353178	Ha	Many loamy fine sand,			0.09		0.00			0.00		0.00	0.01	0.09		0.00
Butte	356.505	357.481	0.976	5,152	SD019	353257	ZeB	Zeona loamy fine sand, 0 to 6 percent slopes		0.05	0.78				0.20		0.20	0.20	0.78			0.00
Butte	357.481	357.542	0.061	324	SD019	353141	AnA	Archin-Slickspots complex, 0 to 3 percent slopes		0.02	0.00				0.06		0.06	0.06				
Butte	357.542	357.607	0.065	344	SD019	353147	Bd	badland		0.06	0.01	0.05		0.00	0.00		0.01	0.01		0.08	0.05	
Butte	357.607	357.638	0.030	160	SD019	353249	TYD	Twilight fine sandy loam, 3 to 25 percent slopes		0.02	0.02	0.02	0.00	0.00	0.00		0.01	0.01		0.03		
Perkins	357.638	357.669	0.032	167	SD105	354666	TcD	Twilight-Marmarth-Parthin association, gently rolling		0.03	0.02	0.00	0.00	0.00	0.01		0.01	0.01	0.02			0.00
Perkins	357.669	357.762	0.093	491	SD105	354608	AbC	Bullock-Slickspots complex, 0 to 15 percent slopes		0.09	0.00	0.01			0.00	0.08		0.08	0.09		0.01	
Perkins	357.762	358.199	0.436	2,304	SD105	354666	TcD	Twilight-Marmarth-Parthin association, gently rolling		0.43	0.28	0.02	0.01	0.01	0.12		0.14	0.25		0.14		0.00
Perkins	358.199	358.378	0.180	949	SD105	354608	AbC	Bullock-Slickspots complex, 0 to 15 percent slopes		0.18	0.01	0.01			0.01	0.15		0.18	0.17		0.02	
Perkins	358.378	358.416	0.037	197	SD105	354666	TcD	Twilight-Marmarth-Parthin association, gently rolling		0.04	0.02	0.00	0.00	0.00	0.01		0.01	0.02		0.01		0.00
Perkins	358.416	358.454	0.038	202	SD105	354608	AbC	Bullock-Slickspots complex, 0 to 15 percent slopes		0.04	0.00	0.00			0.00	0.03		0.03	0.04		0.00	
Perkins	358.454	358.570	0.116	614	SD105	354666	TcD	Twilight-Marmarth-Parthin association, gently rolling		0.12	0.08	0.00	0.00	0.00	0.03		0.04	0.07		0.04		0.00
Perkins	358.570	359.498	0.928	4,897	SD105	354608	AbC	Bullock-Slickspots complex, 0 to 15 percent slopes		0.93	0.03	0.07		0.04	0.79		0.83	0.86		0.11		0.00
Perkins	359.498	359.763	0.266	1,403	SD105	354666	TcD	Twilight-Marmarth-Parthin association, gently rolling		0.26	0.17	0.01	0.01	0.01	0.07		0.09	0.15		0.08		0.00
Perkins	359.763	359.836	0.073	383	SD105	354608	AbC	Bullock-Slickspots complex, 0 to 15 percent slopes		0.07	0.00	0.01			0.00	0.05		0.06	0.07		0.01	
Perkins	359.836	360.034	0.198	1,046	SD105	354607	AaB	Bullock-Parthin loams, 0 to 9 percent slopes		0.20	0.06				0.19		0.19	0.20				
Perkins	360.034	360.063	0.029	153	SD105	354666	TcD	Twilight-Marmarth-Parthin association, gently rolling		0.03	0.02	0.00	0.00	0.00	0.01		0.01	0.02		0.01		0.00
Perkins	360.063	360.154	0.091	479	SD105	354607	AaB	Bullock-Parthin loams, 0 to 9 percent slopes		0.09	0.03				0.09		0.09	0.09				
Perkins	360.154	360.563	0.409	2,161	SD105	354666	TcD	Twilight-Marmarth-Parthin association, gently rolling		0.41	0.27	0.02	0.01	0.01	0.11		0.14	0.24		0.13		0.00
Perkins	360.563	360.647	0.083	441	SD105	354607	AaB	Bullock-Parthin loams, 0 to 9 percent slopes		0.08	0.03				0.08		0.08	0.08				
Perkins	360.647	360.656	0.009	49	SD105	354666	TcD	Twilight-Marmarth-Parthin association, gently rolling		0.01	0.01	0.00	0.00	0.00	0.00		0.00	0.01		0.00		0.00
Perkins	360.656	360.695	0.039	208	SD105	354607	AaB	Bullock-Parthin loams, 0 to 9 percent slopes		0.04	0.01				0.04		0.04	0.04				
Perkins	360.695	360.930	0.235	1,240	SD105	354666	TcD	Twilight-Marmarth-Parthin association, gently rolling		0.23	0.15	0.01	0.01	0.00	0.07		0.08	0.14		0.07		0.00
Perkins	360.930	360.958	0.028	146	SD105	354607	AaB	Bullock-Parthin loams, 0 to 9 percent slopes		0.03	0.01				0.03		0.03	0.03				
Perkins	360.958	361.115	0.157	828	SD105	354666	TcD	Twilight-Marmarth-Parthin association, gently rolling		0.16	0.10	0.01	0.00	0.00	0.04		0.06	0.09		0.06		0.00
Perkins	361.115	361.370	0.256	1,351	SD105	354607	AaB	Bullock-Parthin loams, 0 to 9 percent slopes		0.26	0.08				0.24		0.24	0.26				
Perkins	361.370	361.398	0.028	146	SD105	354666	TcD	Twilight-Marmarth-Parthin association, gently rolling		0.03	0.02	0.00	0.00	0.00	0.01		0.01	0.02		0.01		0.00
Perkins	361.398	361.510	0.112	593	SD105	354607	AaB	Bullock-Parthin loams, 0 to 9 percent slopes		0.11	0.03				0.11		0.11	0.11				
Perkins	361.510	361.532	0.021	112	SD105	354608	AbC	Bullock-Slickspots complex, 0 to 15 percent slopes		0.02	0.00	0.00			0.00	0.02		0.02	0.02		0.00	
Perkins	361.532	361.577	0.045	240	SD105	354607	AaB	Bullock-Parthin loams, 0 to 9 percent slopes		0.05	0.01				0.04		0.04	0.05				
Perkins	361.577	361.685	0.108	569	SD105	354608	AbC	Bullock-Slickspots complex, 0 to 15 percent slopes		0.11	0.00	0.01			0.00	0.09		0.10	0.10		0.01	
Perkins	361.685	361.834	0.149	785	SD105	354607	AaB	Bullock-Parthin loams, 0 to 9 percent slopes		0.15	0.04				0.14		0.14	0.15				
Perkins	361.834	361.974	0.140	742	SD105	354661	Sd	Shambo loam, channeled		0.00	0.00		0.01		0.01		0.01	0.01		0.01		0.00
Perkins	361.974	362.248	0.274	1,448	SD105	354607	AaB	Bullock-Parthin loams, 0 to 9 percent slopes		0.27	0.08				0.26		0.26	0.27				
Perkins	362.248	362.433	0.185	977	SD105	354666	TcD	Twilight-Marmarth-Parthin association, gently rolling		0.18	0.12	0.01	0.01	0.00	0.05		0.06	0.11		0.06		0.00
Perkins	362.433	362.660	0.227	1,196	SD105	354607	AaB	Bullock-Parthin loams, 0 to 9 percent slopes		0.23	0.07				0.22		0.22	0.23				
Perkins	362.660	362.759	0.099	523	SD105	354608	AbC	Bullock-Slickspots complex, 0 to 15 percent slopes		0.10	0.00		0.01	0.00	0.08		0.09	0.09		0.01		
Perkins	362.759	362.849	0.089	472	SD105	354607	AaB	Bullock-Parthin loams, 0 to 9 percent slopes		0.08	0.03				0.09		0.09	0.09				
Perkins	362.849	362.889	0.041	215	SD105	354608	AbC	Bullock-Slickspots complex, 0 to 15 percent slopes		0.04	0.00	0.00		0.00	0.03		0.04	0.04		0.00		
Perkins	362.889	363.097	0.208	1,097	SD105	354607	AaB	Bullock-Parthin loams, 0 to 9 percent slopes		0.21	0.06				0.20		0.20	0.21				
Perkins	363.097	363.340	0.243	1,282	SD105	354608	AbC	Bullock-Slickspots complex, 0 to 15 percent slopes		0.24	0.01	0.02		0.01	0.21		0.22	0.23		0.03		
Perkins	363.340	363.836	0.497	2,622	SD105	354607	AaB	Bullock-Parthin loams, 0 to 9 percent slopes		0.50	0.16				0.47		0.47	0.50				
Perkins	363.836	364.060	0.224	1,180	SD105	354670	WaD	Wabek sandy loam, 9 to 35 percent slopes		0.01	0.21	0.20						0.20	0.21			
Perkins	364.060	364.295	0.235	1,240	SD105	354663	Sh	Lohler-Trembles complex		0.01	0.00	0.17				0.17	0.16	0.01	0.01	0.23	0.00	
Perkins	364.295	364.352	0.057	302	SD105	354664	Ta	Trembles fine sandy loam		0.00	0.00				0.00		0.00	0.00		0.06	0.00	
Perkins	364.352	364.484	0.132	695	SD105	354613	bb	Banks loamy fine sand		0.13	0.13				0.13		0.13	0.13		0.00	0.00	
Perkins	364.484	364.519	0.035	187	SD105	354664	Ta	Trembles fine sandy loam		0.00	0.00				0.00		0.00	0.00		0.04	0.00	
Perkins	364.519	364.677	0.159	837	SD105	354663	Sh	Lohler-Trembles complex		0.01	0.11				0.11		0.11	0.11	0.01	0.01	0.16	0.00
Perkins	364.677	365.087	0.410	2,164	SD105	354618	BhE	Blackhall-Cabbart complex, 15 to 40 percent slopes		0.39	0.02	0.33		0.16	0.04		0.20	0.23		0.35		
Perkins	365.087	365.175	0.088	463	SD105	354607	AaB	Bullock-Parthin loams, 0 to 9 percent slopes		0.09	0.03				0.0							

Table 1: Soil Limitations Along the Pipeline Centerline Mileposted by Soil Map Unit (continued)

Haakon	429.141	429.562	0.421	2,225	SD055	354141	PkE	Pierre-Samsil clays, 15 to 25 percent slopes	0.39	0.02	0.41	0.18	0.01	0.03	0.01	0.18	0.39	0.41	0.03		
Haakon	429.562	429.707	0.145	767	SD055	354157	SdF	Samsil-Rock outcrop complex, 15 to 60 percent slopes	0.13	0.01	0.15	0.08				0.08	0.09	0.15	0.06		
Haakon	429.707	429.863	0.155	819	SD055	354162	SfF	Schamber-Samsil complex, 6 to 60 percent slopes	0.07	0.08	0.15	0.06				0.06	0.07	0.16	0.09		
Haakon	429.863	430.008	0.145	766	SD055	354152	Rh	Ree-Haven complex	0.12	0.00				0.03		0.03	0.15			0.15	0.02
Haakon	430.008	431.762	1.754	9,261	SD055	354148	ReA	Ree loam, 0 to 2 percent slopes		1.87		0.04		0.05		0.05	1.75			1.75	0.02
Haakon	431.762	431.951	0.189	1,000	SD055	354151	RfC	Ree-Canning loams, 6 to 9 percent slopes	0.02	0.17						0.17	0.09	0.19			
Haakon	431.951	432.158	0.207	1,093	SD055	354149	ReB	Ree loam, 2 to 6 percent slopes		0.19		0.01		0.01		0.01	0.21			0.21	0.01
Haakon	432.158	432.975	0.817	4,315	SD055	354148	ReA	Ree loam, 0 to 2 percent slopes		0.78		0.02		0.02		0.02	0.82			0.82	0.01
Haakon	432.975	435.130	2.155	11,377	SD055	354101	KmB	Kirley-Ottumwa complex, 2 to 6 percent slopes	0.22			0.19		0.19		0.19	2.15			2.15	0.02
Haakon	435.130	435.164	0.034	178	SD055	354155	SbF	Samsil clay, 25 to 60 percent slopes	0.03	0.00	0.03	0.03		0.00		0.03	0.03	0.03	0.00		
Haakon	435.164	435.574	0.411	2,169	SD055	354101	KmB	Kirley-Ottumwa complex, 2 to 6 percent slopes	0.04			0.04		0.04		0.04	0.41			0.41	0.00
Haakon	435.574	435.696	0.122	644	SD055	354095	ReB	Kirley clay loam, 2 to 6 percent slopes	0.01			0.00		0.00		0.00	0.12			0.12	0.00
Haakon	435.696	435.815	0.118	625	SD055	354133	OvA	Ottumwa-Capa complex, 0 to 3 percent slopes	0.00					0.04		0.04	0.12			0.12	0.00
Haakon	435.815	436.760	0.945	4,989	SD055	354101	KmB	Kirley-Ottumwa complex, 2 to 6 percent slopes	0.09			0.09		0.09		0.09	0.94			0.94	0.01
Haakon	436.760	436.934	0.174	920	SD055	354083	CbA	Capa silt loam, 0 to 6 percent slopes	0.01			0.01		0.16		0.17	0.17			0.17	0.00
Haakon	436.934	437.152	0.218	1,151	SD055	354101	KmB	Kirley-Ottumwa complex, 2 to 6 percent slopes	0.02			0.02		0.02		0.02	0.22			0.22	0.00
Haakon	437.152	437.237	0.085	448	SD055	354133	OvA	Ottumwa-Capa complex, 0 to 3 percent slopes	0.00					0.03		0.03	0.08			0.08	0.00
Haakon	437.237	437.329	0.092	486	SD055	354134	DwB	Ottumwa-Lakoma silty clays, 3 to 6 percent slopes	0.03			0.00		0.00		0.00	0.09			0.09	0.00
Haakon	437.329	437.595	0.266	1,403	SD055	354133	OvA	Ottumwa-Capa complex, 0 to 3 percent slopes	0.01					0.09		0.09	0.27			0.27	0.01
Haakon	437.595	437.821	0.227	1,197	SD055	354132	OvB	Ottumwa silty clay, 3 to 6 percent slopes	0.01					0.01		0.01	0.23			0.23	0.01
Haakon	437.821	437.922	0.101	534	SD055	354133	OvA	Ottumwa-Capa complex, 0 to 3 percent slopes	0.00					0.04		0.04	0.10			0.10	0.00
Haakon	437.922	438.008	0.085	450	SD055	354135	OwC	Ottumwa-Lakoma silty clays, 6 to 9 percent slopes	0.03			0.00		0.01		0.01	0.09	0.08		0.08	0.00
Haakon	438.008	438.368	0.360	1,902	SD055	354132	OvB	Ottumwa silty clay, 3 to 6 percent slopes	0.02					0.02		0.02	0.36			0.36	0.02
Haakon	438.368	438.583	0.215	1,135	SD055	354109	LaD	Lakoma silty clay, 6 to 15 percent slopes		0.01	0.01	0.01				0.02	0.21	0.20		0.20	0.01
Haakon	438.583	438.952	0.369	1,950	SD055	354132	OvB	Ottumwa silty clay, 3 to 6 percent slopes	0.02					0.02		0.02	0.37			0.37	0.02
Haakon	438.952	439.293	0.341	1,801	SD055	354135	OwC	Ottumwa-Lakoma silty clays, 6 to 9 percent slopes	0.12			0.02		0.03		0.03	0.34	0.31		0.31	0.02
Haakon	439.293	440.256	0.963	5,083	SD055	354134	DwB	Ottumwa-Lakoma silty clays, 3 to 6 percent slopes	0.29			0.02		0.04		0.04	0.96			0.96	0.01
Haakon	440.256	440.611	0.355	1,875	SD055	354135	OwC	Ottumwa-Lakoma silty clays, 6 to 9 percent slopes	0.12			0.02		0.02		0.02	0.32	0.32		0.32	0.01
Haakon	440.611	440.876	0.266	1,402	SD055	354131	OvA	Ottumwa silty clay, 0 to 3 percent slopes						0.00		0.00	0.27			0.27	0.02
Haakon	440.876	440.906	0.030	156	SD055	354134	DwB	Ottumwa-Lakoma silty clays, 3 to 6 percent slopes	0.01			0.00		0.00		0.00	0.03			0.03	0.00
Haakon	440.906	441.016	0.110	580	SD055	354131	OvA	Ottumwa silty clay, 0 to 3 percent slopes						0.01		0.01	0.11			0.11	0.01
Haakon	441.016	441.056	0.041	214	SD055	354133	DvA	Ottumwa-Capa complex, 0 to 3 percent slopes	0.00					0.01		0.01	0.04			0.04	0.00
Haakon	441.056	441.149	0.092	488	SD055	354166	WvD	Wendite-Herdcamp silty clays, channelled				0.04		0.00		0.04	0.09			0.09	0.03
Haakon	441.149	441.181	0.032	167	SD055	354133	OvA	Ottumwa-Capa complex, 0 to 3 percent slopes	0.00					0.01		0.01	0.03			0.03	0.00
Haakon	441.181	441.230	0.049	259	SD055	354132	OvB	Ottumwa silty clay, 3 to 6 percent slopes	0.00					0.00		0.00	0.05			0.05	0.00
Haakon	441.230	442.739	1.510	7,972	SD055	354134	DwB	Ottumwa-Lakoma silty clays, 3 to 6 percent slopes	0.45			0.03		0.06		0.06	1.51			1.51	0.02
Haakon	442.739	442.800	0.060	319	SD055	354104	Ko	Kolls clay						0.01		0.01	0.06			0.06	0.05
Haakon	442.800	443.255	0.455	2,404	SD055	354134	DwB	Ottumwa-Lakoma silty clays, 3 to 6 percent slopes	0.14			0.01		0.02		0.02	0.46			0.46	0.00
Haakon	443.255	443.399	0.144	759	SD055	354135	OwC	Ottumwa-Lakoma silty clays, 6 to 9 percent slopes	0.05			0.01		0.01		0.01	0.14	0.15		0.15	0.01
Haakon	443.399	443.582	0.183	966	SD055	354109	LaD	Lakoma silty clay, 6 to 15 percent slopes	0.16		0.01	0.01		0.01		0.01	0.18	0.17		0.17	0.04
Haakon	443.582	443.694	0.112	593	SD055	354166	WvD	Wendite-Herdcamp silty clays, channelled				0.04		0.01		0.04	0.11			0.11	0.01
Haakon	443.694	443.805	0.111	586	SD055	354141	PkE	Pierre-Samsil clays, 15 to 25 percent slopes	0.10	0.00	0.11	0.05	0.00	0.00	0.00	0.05	0.10	0.11	0.01	0.11	0.01
Haakon	443.805	443.999	0.194	1,025	SD055	354108	Lac	Lakoma silty clay, 6 to 9 percent slopes	0.18			0.00		0.01		0.01	0.19	0.18		0.18	0.00
Haakon	443.999	444.019	0.020	105	SD055	354132	OvB	Ottumwa silty clay, 3 to 6 percent slopes	0.00					0.00		0.00	0.02			0.02	0.00
Haakon	444.019	444.039	0.020	105	SD055	354108	Lac	Lakoma silty clay, 6 to 9 percent slopes	0.02			0.00		0.00		0.00	0.02	0.02		0.02	0.00
Haakon	444.039	444.353	0.314	1,659	SD055	354132	OvB	Ottumwa silty clay, 3 to 6 percent slopes	0.02					0.02		0.02	0.31			0.31	0.02
Haakon	444.353	444.781	0.428	2,258	SD055	354108	Lac	Lakoma silty clay, 6 to 9 percent slopes	0.39		0.01	0.01		0.01		0.02	0.43	0.41		0.41	0.01
Haakon	444.781	444.993	0.212	1,118	SD055	354132	OvB	Ottumwa silty clay, 3 to 6 percent slopes	0.01					0.01		0.01	0.21			0.21	0.01
Haakon	444.993	445.091	0.098	518	SD055	354108	Lac	Lakoma silty clay, 6 to 9 percent slopes	0.09		0.00	0.00		0.00		0.00	0.10	0.09		0.09	0.00
Haakon	445.091	446.243	1.152	6,081	SD055	354132	OvB	Ottumwa silty clay, 3 to 6 percent slopes	0.06					0.06		0.06	1.15			1.15	0.06
Haakon	446.243	446.282	0.040	210	SD055	354131	OvA	Ottumwa silty clay, 0 to 3 percent slopes						0.00		0.00	0.04			0.04	0.00
Haakon	446.282	446.773	0.491	2,591	SD055	354132	OvB	Ottumwa silty clay, 3 to 6 percent slopes	0.02					0.02		0.02	0.49			0.49	0.02
Haakon	446.773	447.229	0.456	2,405	SD055	354137	OyC	Ottumwa-Razor-saw complex, 6 to 15 percent slopes	0.16			0.05		0.05		0.05	0.46	0.43		0.43	0.02
Haakon	447.229	447.348	0.119	630	SD055	354132	OvB	Ottumwa silty clay, 3 to 6 percent slopes	0.01					0.01		0.01	0.12			0.12	0.01
Haakon	447.348	447.417	0.069	365	SD055	354135	OwC	Ottumwa-Lakoma silty clays, 6 to 9 percent slopes	0.02			0.00		0.01		0.01	0.07	0.08		0.08	0.01
Haakon	447.417	447.628	0.211	1,112	SD055	354134	DwB	Ottumwa-Lakoma silty clays, 3 to 6 percent slopes	0.06			0.00		0.01		0.01	0.21			0.21	0.00
Haakon	447.628	447.881	0.253	1,335	SD055	354109	LaD	Lakoma silty clay, 6 to 15 percent slopes	0.22		0.01	0.01		0.01		0.02	0.25	0.24		0.24	0.01
Haakon	447.881	448.154	0.274	1,446	SD055	354108	Lac	Lakoma silty clay, 6 to 9 percent slopes	0.25		0.01	0.01		0.01		0.0					

Table 1: Soil Limitations Along the Pipeline Centerline Mileposted by Soil Map Unit (continued)

Haakon	448.783	448.861	0.078	412	SD055	354109	LaD	Lakoma silty clay, 6 to 15 percent slopes		0.07		0.00	0.00	0.00	0.01	0.08		0.07		0.00
Haakon	448.861	449.136	0.275	1,455	SD055	354134	OwB	Ottumwa-Lakoma silty clays, 3 to 6 percent slopes		0.08		0.01	0.01	0.01	0.01	0.28			0.28	0.00
Haakon	449.136	449.247	0.110	583	SD055	354109	LaD	Lakoma silty clay, 6 to 15 percent slopes		0.10		0.00	0.00	0.00	0.01	0.11		0.10		0.00
Haakon	449.247	449.425	0.179	943	SD055	354134	OwB	Ottumwa-Lakoma silty clays, 3 to 6 percent slopes		0.05		0.00	0.00	0.01	0.01	0.18			0.18	0.00
Haakon	449.425	449.529	0.104	550	SD055	354109	LaD	Lakoma silty clay, 6 to 15 percent slopes		0.09		0.00	0.00	0.00	0.01	0.10		0.10		0.00
Haakon	449.529	449.701	0.172	909	SD055	354134	OwB	Ottumwa-Lakoma silty clays, 3 to 6 percent slopes		0.05		0.00	0.00	0.01	0.01	0.17			0.17	0.00
Haakon	449.701	449.906	0.204	1,078	SD055	354109	LaD	Lakoma silty clay, 6 to 15 percent slopes		0.18		0.01	0.01	0.01	0.01	0.20		0.18		0.01
Haakon	449.906	449.963	0.058	305	SD055	354108	LaC	Lakoma silty clay, 6 to 9 percent slopes		0.05		0.00	0.00	0.00	0.00	0.06		0.05		0.00
Haakon	449.963	450.451	0.487	2,573	SD055	354132	OtB	Ottumwa silty clay, 3 to 6 percent slopes		0.02			0.02	0.02	0.02	0.48			0.48	0.02
Haakon	450.451	450.692	0.242	1,276	SD055	354134	OwB	Ottumwa-Lakoma silty clays, 3 to 6 percent slopes		0.07		0.00	0.00	0.01	0.01	0.24			0.24	0.00
Haakon	450.692	450.752	0.060	317	SD055	354135	OwC	Ottumwa-Lakoma silty clays, 6 to 9 percent slopes		0.02		0.00	0.00	0.01	0.01	0.06		0.05		0.00
Haakon	450.752	451.187	0.434	2,294	SD055	354134	OwB	Ottumwa-Lakoma silty clays, 3 to 6 percent slopes		0.13		0.01	0.01	0.02	0.02	0.43			0.43	0.00
Haakon	451.187	451.565	0.379	1,999	SD055	354101	KmB	Kirley-Ottumwa complex, 2 to 6 percent slopes		0.04		0.03	0.03	0.03	0.03	0.38			0.38	0.00
Haakon	451.565	451.619	0.053	280	SD055	354132	OtB	Ottumwa silty clay, 3 to 6 percent slopes		0.00			0.00	0.00	0.00	0.05			0.05	0.00
Haakon	451.619	451.760	0.142	747	SD055	354135	OwC	Ottumwa-Lakoma silty clays, 6 to 9 percent slopes		0.05		0.01	0.01	0.01	0.01	0.14		0.13		0.00
Haakon	451.760	452.046	0.286	1,509	SD055	354134	OwB	Ottumwa-Lakoma silty clays, 3 to 6 percent slopes		0.09		0.01	0.01	0.01	0.01	0.29			0.29	0.00
Haakon	452.046	452.499	0.453	2,393	SD055	354132	OtB	Ottumwa silty clay, 3 to 6 percent slopes		0.02			0.02	0.02	0.02	0.45			0.45	0.02
Haakon	452.499	452.591	0.092	487	SD055	354109	LaD	Lakoma silty clay, 6 to 15 percent slopes		0.08		0.00	0.00	0.00	0.01	0.09		0.09		0.00
Haakon	452.591	453.578	0.987	5,210	SD055	354101	KmB	Kirley-Ottumwa complex, 2 to 6 percent slopes		0.10		0.08	0.09	0.09	0.09	0.99			0.99	0.01
Haakon	453.578	453.754	0.175	926	SD055	354131	OtA	Ottumwa silty clay, 0 to 3 percent slopes					0.01	0.01	0.01	0.18			0.18	0.01
Haakon	453.754	453.857	0.103	546	SD055	354101	KmB	Kirley-Ottumwa complex, 2 to 6 percent slopes		0.01		0.01	0.01	0.01	0.01	0.10			0.10	0.00
Haakon	453.857	454.055	0.198	1,045	SD055	354134	OwB	Ottumwa-Lakoma silty clays, 3 to 6 percent slopes		0.06		0.00	0.00	0.01	0.01	0.20			0.20	0.00
Haakon	454.055	454.520	0.465	2,455	SD055	354135	OwC	Ottumwa-Lakoma silty clays, 6 to 9 percent slopes		0.18		0.02	0.02	0.05	0.05	0.46		0.42		0.00
Haakon	454.520	454.690	0.170	899	SD055	354107	LaB	Lakoma silty clay, 3 to 6 percent slopes		0.15			0.01	0.01	0.01	0.17			0.17	0.00
Haakon	454.690	454.957	0.267	1,411	SD055	354135	OwC	Ottumwa-Lakoma silty clays, 6 to 9 percent slopes		0.08		0.01	0.01	0.03	0.03	0.27		0.24		0.00
Haakon	454.957	455.131	0.173	916	SD055	354109	LaD	Lakoma silty clay, 6 to 15 percent slopes		0.15		0.01	0.01	0.01	0.01	0.17		0.16		0.01
Haakon	455.131	455.247	0.116	612	SD055	354085	Ct	Capa-Wendte, channelled, complex		0.01		0.01	0.01	0.06	0.07	0.12			0.12	0.01
Haakon	455.247	455.285	0.039	204	SD055	354109	LaD	Lakoma silty clay, 6 to 15 percent slopes		0.03		0.00	0.00	0.00	0.00	0.04			0.04	0.00
Haakon	455.285	455.370	0.085	447	SD055	354135	OwC	Ottumwa-Lakoma silty clays, 6 to 9 percent slopes		0.03		0.00	0.00	0.01	0.01	0.08			0.08	0.00
Haakon	455.370	455.700	0.330	1,742	SD055	354109	LaD	Lakoma silty clay, 6 to 15 percent slopes		0.29		0.01	0.01	0.01	0.02	0.33			0.33	0.01
Haakon	455.700	455.803	0.103	542	SD055	354134	OwB	Ottumwa-Lakoma silty clays, 3 to 6 percent slopes		0.03		0.00	0.00	0.00	0.00	0.10		0.10		0.00
Haakon	455.803	456.026	0.224	1,181	SD055	354135	OwC	Ottumwa-Lakoma silty clays, 6 to 9 percent slopes		0.08		0.01	0.01	0.02	0.02	0.22		0.20		0.00
Haakon	456.026	456.148	0.122	642	SD055	354132	OtB	Ottumwa silty clay, 3 to 6 percent slopes		0.01			0.01	0.01	0.01	0.12			0.12	0.01
Haakon	456.148	456.248	0.100	526	SD055	354127	OeB	Opal-Promise clays, 3 to 6 percent slopes		0.05		0.09	0.09	0.01	0.09	0.10			0.10	0.00
Haakon	456.248	456.329	0.082	431	SD055	354132	OtB	Ottumwa silty clay, 3 to 6 percent slopes		0.00			0.00	0.00	0.00	0.08			0.08	0.00
Haakon	456.329	456.515	0.186	982	SD055	354107	LaB	Lakoma silty clay, 3 to 6 percent slopes		0.17			0.01	0.01	0.01	0.19			0.19	0.00
Haakon	456.515	456.566	0.051	267	SD055	354135	OwC	Ottumwa-Lakoma silty clays, 6 to 9 percent slopes		0.02		0.00	0.01	0.01	0.01	0.05		0.05		0.00
Haakon	456.566	456.626	0.060	319	SD055	354107	LaB	Lakoma silty clay, 3 to 6 percent slopes		0.05			0.00	0.00	0.00	0.06			0.06	0.00
Haakon	456.626	456.850	0.223	1,180	SD055	354135	OwC	Ottumwa-Lakoma silty clays, 6 to 9 percent slopes		0.08		0.01	0.01	0.02	0.02	0.22		0.20		0.00
Haakon	456.850	457.073	0.223	1,177	SD055	354107	LaB	Lakoma silty clay, 3 to 6 percent slopes		0.20			0.01	0.01	0.01	0.22			0.22	0.00
Haakon	457.073	457.387	0.314	1,659	SD055	354109	LaD	Lakoma silty clay, 6 to 15 percent slopes		0.28		0.01	0.01	0.01	0.02	0.31		0.29		0.01
Haakon	457.387	457.536	0.150	790	SD055	354135	OwC	Ottumwa-Lakoma silty clays, 6 to 9 percent slopes		0.05		0.01	0.01	0.01	0.01	0.15		0.13		0.00
Haakon	457.536	457.663	0.126	668	SD055	354132	OtB	Ottumwa silty clay, 3 to 6 percent slopes		0.01			0.01	0.01	0.01	0.13			0.13	0.01
Haakon	457.663	457.718	0.055	292	SD055	354135	OwC	Ottumwa-Lakoma silty clays, 6 to 9 percent slopes		0.02		0.00	0.01	0.01	0.01	0.06		0.05		0.00
Haakon	457.718	457.946	0.228	1,204	SD055	354134	OwB	Ottumwa-Lakoma silty clays, 3 to 6 percent slopes		0.07		0.00	0.01	0.01	0.01	0.23		0.23		0.00
Haakon	457.946	457.989	0.043	225	SD055	354135	OwC	Ottumwa-Lakoma silty clays, 6 to 9 percent slopes		0.01		0.00	0.00	0.00	0.00	0.04		0.04		0.00
Haakon	457.989	458.237	0.248	1,309	SD055	354134	OwB	Ottumwa-Lakoma silty clays, 3 to 6 percent slopes		0.07		0.00	0.01	0.01	0.01	0.25			0.25	0.00
Haakon	458.237	458.380	0.144	759	SD055	354135	OwC	Ottumwa-Lakoma silty clays, 6 to 9 percent slopes		0.05		0.01	0.01	0.01	0.01	0.14		0.13		0.00
Haakon	458.380	458.462	0.082	433	SD055	354134	OwB	Ottumwa-Lakoma silty clays, 3 to 6 percent slopes		0.02		0.00	0.00	0.00	0.00	0.08			0.08	0.00
Haakon	458.462	458.485	0.022	116	SD055	354135	OwC	Ottumwa-Lakoma silty clays, 6 to 9 percent slopes		0.01		0.00	0.00	0.00	0.00	0.02		0.02		0.00
Haakon	458.485	458.527	0.043	226	SD055	354134	OwB	Ottumwa-Lakoma silty clays, 3 to 6 percent slopes		0.01		0.00	0.00	0.00	0.00	0.04			0.04	0.00
Haakon	458.527	458.580	0.053	278	SD055	354135	OwC	Ottumwa-Lakoma silty clays, 6 to 9 percent slopes		0.02		0.00	0.00	0.01	0.05	0.05		0.05		0.00
Haakon	458.580	459.000	0.420	2,219	SD055	354109	LaD	Lakoma silty clay, 6 to 15 percent slopes		0.37		0.02	0.01	0.02	0.03	0.42		0.39		0.01
Haakon	459.000	459.016	0.016	86	SD055	354170	W	Water												
Haakon	459.016	459.321	0.304	1,607	SD055	354109	LaD	Lakoma silty clay, 6 to 15 percent slopes		0.27		0.01	0.01	0.01	0.02	0.30		0.28		0.01
Haakon	459.321	459.425	0.104	551	SD055	354134	OwB	Ottumwa-Lakoma silty clays, 3 to 6 percent slopes		0.03		0.00	0.00	0.00	0.00	0.10		0.10		0.00
Haakon	459.425	459.789	0.364	1,922	SD055	354108	LaC	Lakoma silty clay, 6 to 9 percent slopes		0.33		0.01	0.01	0.01	0.02	0.36		0.35		0.01
Haakon	459.789	460.285	0.496	2,620	SD055	354134	OwB	Ottumwa-Lakoma silty clays, 3 to 6 percent slopes		0.15		0.01	0.01	0.02	0.02	0.50			0.50	0.00
Haakon	460.285	460.660	0.374	1,976	SD055	354094	KeA	Kirley clay loam, 0 to 2 percent slopes		0.02		0.02	0.02	0.02	0.02	0.37			0.37	0.02
Haakon	460.660	460.708	0.049	256	SD055	354103	KnD	Kirley-Vivian complex, 6 to 15 percent slopes		0.02		0.00				0.03		0.03	0.01	0.00
Haakon	460.708	460.766	0.058	304	SD055	354085	Ct	Capa-Wendte, channelled, complex		0.00		0.00	0.03	0.03	0.03	0.06			0.06	0.00
Haakon	460.766	461.005	0.239	1,264	SD055	354135	OwC	Ottumwa-Lakoma silty clays, 6 to 9 percent slopes		0.08		0.01	0.01	0.02	0.02	0.24		0.22		0.00
Haakon	461.005	461.034	0.029	152	SD055	354134	OwB	Ottumwa-Lakoma silty clays, 3 to 6 percent slopes		0.01		0.00	0.00	0.00	0.00	0.03			0.03	0.00
Haakon	461.034	461.101	0.067	353	SD055	354103	KnD	Kirley-Vivian complex, 6 to 15 percent slopes		0.03		0.00				0.05		0.06	0.02	0.00

Table 1: Soil Limitations Along the Pipeline Centerline Mileposted by Soil Map Unit (continued)

Haakon	461.101	461.208	0.107	563	SD055	354134	OwB	Ottumwa-Lakoma silty clays, 3 to 6 percent slopes		0.03		0.00	0.00	0.00	0.00	0.11	0.03
Haakon	461.208	461.259	0.051	270	SD055	354094	KeA	Kirley clay loam, 0 to 2 percent slopes				0.00	0.00	0.00	0.00	0.05	0.00
Haakon	461.259	461.375	0.116	612	SD055	354134	OwB	Ottumwa-Lakoma silty clays, 3 to 6 percent slopes		0.03		0.00	0.00	0.00	0.00	0.12	0.00
Haakon	461.375	461.493	0.119	627	SD055	354109	LaD	Lakoma silty clay, 6 to 15 percent slopes		0.11		0.00	0.00	0.00	0.01	0.12	0.00
Haakon	461.493	461.573	0.079	418	SD055	354107	LaB	Lakoma silty clay, 3 to 6 percent slopes		0.07			0.00	0.00	0.00	0.08	0.00
Haakon	461.573	461.584	0.011	59	SD055	354109	LaD	Lakoma silty clay, 6 to 15 percent slopes		0.01		0.00	0.00	0.00	0.00	0.01	0.00
Haakon	461.584	461.958	0.374	1,976	SD055	354107	LaB	Lakoma silty clay, 3 to 6 percent slopes		0.34			0.02	0.02	0.02	0.37	0.00
Haakon	461.958	462.120	0.162	854	SD055	354131	OtA	Ottumwa silty clay, 0 to 3 percent slopes					0.01	0.01	0.01	0.18	0.01
Haakon	462.120	462.149	0.029	153	SD055	354132	OtB	Ottumwa silty clay, 3 to 6 percent slopes		0.00			0.00	0.00	0.00	0.03	0.00
Haakon	462.149	462.199	0.050	264	SD055	354131	OtA	Ottumwa silty clay, 0 to 3 percent slopes					0.00	0.00	0.00	0.05	0.00
Haakon	462.199	462.432	0.233	1,229	SD055	354132	OtB	Ottumwa silty clay, 3 to 6 percent slopes					0.01	0.01	0.01	0.23	0.00
Haakon	462.432	462.655	0.224	1,181	SD055	354107	LaB	Lakoma silty clay, 3 to 6 percent slopes		0.20			0.01	0.01	0.01	0.22	0.01
Haakon	462.655	462.694	0.038	201	SD055	354132	OtB	Ottumwa silty clay, 3 to 6 percent slopes		0.00			0.00	0.00	0.00	0.04	0.00
Haakon	462.694	462.766	0.072	382	SD055	354107	LaB	Lakoma silty clay, 3 to 6 percent slopes		0.07			0.00	0.00	0.00	0.07	0.00
Haakon	462.766	462.912	0.146	769	SD055	354108	LaC	Lakoma silty clay, 6 to 9 percent slopes		0.13		0.00	0.00	0.00	0.01	0.15	0.00
Haakon	462.912	462.943	0.031	166	SD055	354109	LaD	Lakoma silty clay, 6 to 15 percent slopes		0.03		0.00	0.00	0.00	0.00	0.03	0.00
Haakon	462.943	463.485	0.542	2,864	SD055	354108	LaC	Lakoma silty clay, 6 to 9 percent slopes		0.50		0.01	0.01	0.02	0.03	0.54	0.01
Haakon	463.485	463.747	0.261	1,380	SD055	354134	OwB	Ottumwa-Lakoma silty clays, 3 to 6 percent slopes		0.08			0.01	0.01	0.01	0.28	0.00
Haakon	463.747	463.997	0.250	1,318	SD055	354108	LaC	Lakoma silty clay, 6 to 9 percent slopes		0.23		0.00	0.00	0.01	0.01	0.25	0.00
Haakon	463.997	464.418	0.421	2,225	SD055	354134	OwB	Ottumwa-Lakoma silty clays, 3 to 6 percent slopes		0.13			0.00	0.00	0.02	0.42	0.00
Haakon	464.418	464.617	0.199	1,048	SD055	354135	DwC	Ottumwa-Lakoma silty clays, 6 to 9 percent slopes		0.07		0.01	0.01	0.02	0.02	0.20	0.00
Haakon	464.617	464.779	0.163	860	SD055	354132	OtB	Ottumwa silty clay, 3 to 6 percent slopes		0.01			0.01	0.01	0.01	0.16	0.01
Haakon	464.779	464.916	0.136	719	SD055	354087	Eg	Egas silty clay loam				0.13	0.01	0.01	0.01	0.13	0.12
Haakon	464.916	465.086	0.171	903	SD055	354109	LaD	Lakoma silty clay, 6 to 15 percent slopes		0.15		0.01	0.01	0.01	0.01	0.17	0.01
Haakon	465.086	465.211	0.125	659	SD055	354135	OwC	Ottumwa-Lakoma silty clays, 6 to 9 percent slopes		0.04		0.01	0.01	0.01	0.01	0.12	0.00
Haakon	465.211	465.372	0.160	847	SD055	354132	OtB	Ottumwa silty clay, 3 to 6 percent slopes		0.01			0.01	0.01	0.01	0.16	0.01
Haakon	465.372	465.501	0.130	685	SD055	354107	LaB	Lakoma silty clay, 3 to 6 percent slopes		0.12			0.01	0.01	0.01	0.13	0.00
Haakon	465.501	465.564	0.063	330	SD055	354134	OwB	Ottumwa-Lakoma silty clays, 3 to 6 percent slopes		0.02		0.00	0.00	0.00	0.00	0.06	0.00
Haakon	465.564	465.787	0.223	1,177	SD055	354109	LaD	Lakoma silty clay, 6 to 15 percent slopes		0.20		0.01	0.01	0.01	0.02	0.22	0.01
Haakon	465.787	465.853	0.066	346	SD055	354107	LaB	Lakoma silty clay, 3 to 6 percent slopes		0.06			0.00	0.00	0.00	0.07	0.00
Haakon	465.853	466.503	0.651	3,436	SD055	354109	LaD	Lakoma silty clay, 6 to 15 percent slopes		0.58		0.03	0.02	0.03	0.05	0.65	0.02
Haakon	466.503	466.567	0.064	337	SD055	354107	LaB	Lakoma silty clay, 3 to 6 percent slopes		0.06			0.00	0.00	0.00	0.06	0.00
Haakon	466.567	466.644	0.077	404	SD055	354134	OwB	Ottumwa-Lakoma silty clays, 3 to 6 percent slopes		0.02		0.00	0.00	0.00	0.00	0.08	0.00
Haakon	466.644	466.992	0.349	1,840	SD055	354107	LaB	Lakoma silty clay, 3 to 6 percent slopes		0.31			0.02	0.02	0.02	0.35	0.00
Haakon	466.992	468.096	1.104	5,827	SD055	354132	OtB	Ottumwa silty clay, 3 to 6 percent slopes		0.06			0.06	0.06	1.10	0.06	0.00
Haakon	468.096	468.110	0.014	76	SD055	354107	LaB	Lakoma silty clay, 3 to 6 percent slopes		0.01			0.00	0.00	0.00	0.01	0.00
Haakon	468.110	468.233	0.123	650	SD055	354109	LaD	Lakoma silty clay, 6 to 15 percent slopes		0.11		0.00	0.00	0.00	0.01	0.12	0.00
Haakon	468.233	468.272	0.039	204	SD055	354085	Ct	Capa-Wendte, channelled, complex		0.00			0.00	0.02	0.02	0.04	0.00
Haakon	468.272	468.461	0.189	1,000	SD055	354109	LaD	Lakoma silty clay, 6 to 15 percent slopes		0.17		0.01	0.01	0.01	0.01	0.19	0.01
Haakon	468.461	468.705	0.244	1,288	SD055	354103	Knd	Kirley-Vivian complex, 9 to 25 percent slopes		0.11		0.02			0.01	0.17	0.07
Haakon	468.705	468.959	0.254	1,340	SD055	354132	OtB	Ottumwa silty clay, 3 to 6 percent slopes		0.01				0.01	0.01	0.25	0.01
Haakon	468.959	469.013	0.054	287	SD055	354108	LaC	Lakoma silty clay, 6 to 9 percent slopes		0.05		0.00	0.00	0.00	0.00	0.05	0.00
Haakon	469.013	469.220	0.207	1,090	SD055	354109	LaD	Lakoma silty clay, 6 to 15 percent slopes		0.18		0.01	0.01	0.01	0.01	0.19	0.01
Haakon	469.220	469.289	0.069	366	SD055	354108	LaC	Lakoma silty clay, 6 to 9 percent slopes		0.05		0.00	0.00	0.00	0.00	0.07	0.00
Haakon	469.289	469.584	0.294	1,555	SD055	354109	LaD	Lakoma silty clay, 6 to 15 percent slopes		0.28		0.01	0.01	0.01	0.02	0.29	0.01
Haakon	469.584	469.915	0.331	1,750	SD055	354108	LaC	Lakoma silty clay, 6 to 9 percent slopes		0.30		0.01	0.01	0.01	0.02	0.33	0.01
Haakon	469.915	469.976	0.061	323	SD055	354131	OtA	Ottumwa silty clay, 0 to 3 percent slopes					0.00	0.00	0.00	0.06	0.00
Haakon	469.976	470.216	0.240	1,266	SD055	354132	OtB	Ottumwa silty clay, 3 to 6 percent slopes		0.01			0.01	0.01	0.01	0.24	0.01
Haakon	470.216	470.500	0.284	1,501	SD055	354108	LaC	Lakoma silty clay, 6 to 9 percent slopes		0.28		0.01	0.01	0.01	0.01	0.28	0.01
Haakon	470.500	470.613	0.113	594	SD055	354109	LaD	Lakoma silty clay, 6 to 15 percent slopes		0.10		0.00	0.00	0.00	0.01	0.10	0.00
Haakon	470.613	470.710	0.097	513	SD055	354132	OtB	Ottumwa silty clay, 3 to 6 percent slopes		0.00			0.00	0.00	0.00	0.10	0.00
Haakon	470.710	470.870	0.160	843	SD055	354109	LaD	Lakoma silty clay, 6 to 15 percent slopes		0.14		0.01	0.00	0.01	0.01	0.16	0.00
Haakon	470.870	471.050	0.180	952	SD055	354108	LaC	Lakoma silty clay, 6 to 9 percent slopes		0.17		0.00	0.00	0.01	0.01	0.17	0.00
Haakon	471.050	471.325	0.275	1,451	SD055	354132	OtB	Ottumwa silty clay, 3 to 6 percent slopes		0.01			0.01	0.01	0.01	0.27	0.01
Haakon	471.325	471.401	0.076	401	SD055	354102	KmC	Kirley-Ottumwa complex, 6 to 9 percent slopes		0.01			0.00	0.00	0.00	0.08	0.00
Haakon	471.401	471.673	0.272	1,437	SD055	354095	KeB	Kirley clay loam, 2 to 6 percent slopes		0.01			0.01	0.01	0.01	0.27	0.00
Haakon	471.673	471.851	0.178	940	SD055	354122	ObE	Ottumwa-Lakoma silty clays, 15 to 40 percent slopes		0.17		0.17	0.01	0.01	0.01	0.17	0.01
Haakon	471.851	471.874	0.023	122	SD055	354110	LbE	Lakoma-Vivian complex, 9 to 25 percent slopes		0.02		0.00	0.01	0.01	0.01	0.02	0.01
Haakon	471.874	472.128	0.254	1,341	SD055	354095	KeB	Kirley clay loam, 2 to 6 percent slopes		0.01			0.01	0.01	0.01	0.25	0.00
Haakon	472.128	472.357	0.139	679	SD055	354094	KeA	Kirley clay loam, 0 to 2 percent slopes					0.01	0.01	0.01	0.13	0.01
Haakon	472.357	472.333	0.076	401	SD055	354110	LbE	Lakoma-Vivian complex, 9 to 25 percent slopes		0.07		0.00	0.03	0.01	0.01	0.07	0.00
Haakon	472.333	472.514	0.181	954	SD055	354109	LaD	Lakoma silty clay, 6 to 15 percent slopes		0.16		0.01	0.01	0.01	0.01	0.18	0.01
Haakon	472.514	472.562	0.048	254	SD055	354085	Ct	Capa-Wendte, channelled, complex		0.00			0.00	0.00	0.03	0.05	0.00
Haakon	472.562	472.594	0.032	171	SD055	354109	LaD	Lakoma silty clay, 6 to 15 percent slopes		0.03		0.00	0.00	0.00	0.00	0.03	0.00

Table 1: Soil Limitations Along the Pipeline Centerline Mileposted by Soil Map Unit (continued)

Haakon	472.594	472.649	0.055	291	SD055	354135	OwC	Ottumwa-Lakoma silty clays, 6 to 9 percent slopes	0.02		0.00	0.01	0.01	0.06		0.05			
Haakon	472.649	472.926	0.277	1,460	SD055	354109	LaD	Lakoma silty clay, 6 to 15 percent slopes	0.25		0.01	0.01	0.01	0.02	0.26	0.26			0.01
Haakon	472.926	473.050	0.124	654	SD055	354110	LbE	Lakoma-Vivian complex, 9 to 25 percent slopes	0.11	0.01	0.05			0.09		0.12	0.04		
Haakon	473.050	473.137	0.087	459	SD055	354095	KeB	Kirley clay loam, 2 to 6 percent slopes	0.00			0.00	0.00	0.00	0.09			0.09	0.00
Haakon	473.137	473.550	0.413	2,181	SD055	354094	KeA	Kirley clay loam, 0 to 2 percent slopes	0.02			0.02	0.02	0.02	0.41			0.41	0.02
Haakon	473.550	473.774	0.224	1,183	SD055	354110	LbE	Lakoma-Vivian complex, 9 to 25 percent slopes	0.19	0.01	0.08			0.16		0.22	0.07		
Haakon	473.774	473.928	0.154	814	SD055	354138	PeC	Pierre clay, 6 to 9 percent slopes	0.15		0.01	0.02		0.02	0.15		0.15		
Haakon	473.928	474.150	0.222	1,174	SD055	354109	LaD	Lakoma silty clay, 6 to 15 percent slopes	0.20		0.01	0.01	0.01	0.02	0.21				0.01
Haakon	474.150	474.207	0.057	302	SD055	354110	LbE	Lakoma-Vivian complex, 9 to 25 percent slopes	0.05	0.00	0.02			0.04		0.06	0.02		
Haakon	474.207	474.414	0.207	1,091	SD055	354095	KeB	Kirley clay loam, 2 to 6 percent slopes	0.01			0.01	0.01	0.01	0.21			0.21	0.00
Haakon	474.414	474.677	0.263	1,388	SD055	354122	ObE	Okaton-Lakoma silty clays, 15 to 40 percent slopes	0.24		0.24	0.01	0.01	0.01	0.25	0.24	0.01		
Haakon	474.677	474.889	0.212	1,122	SD055	354097	KfB	Kirley-Canning complex, 2 to 6 percent slopes	0.01	0.08				0.20		0.10	0.21		
Haakon	474.889	474.922	0.033	175	SD055	354122	ObE	Okaton-Lakoma silty clays, 15 to 40 percent slopes	0.03		0.03	0.00	0.00	0.03		0.03	0.00		
Haakon	474.922	475.420	0.497	2,626	SD055	354097	KfB	Kirley-Canning complex, 2 to 6 percent slopes	0.02	0.20				0.47		0.22	0.50		
Haakon	475.420	476.205	0.785	4,144	SD055	354094	KeA	Kirley clay loam, 0 to 2 percent slopes				0.04	0.04	0.04	0.78			0.78	0.04
Haakon	476.205	476.279	0.074	391	SD055	354097	KfB	Kirley-Canning complex, 2 to 6 percent slopes	0.00	0.03				0.07		0.03	0.07		
Haakon	476.279	476.421	0.143	753	SD055	354094	KeA	Kirley clay loam, 0 to 2 percent slopes				0.01	0.01	0.01	0.14			0.14	0.01
Haakon	476.421	476.515	0.094	495	SD055	354097	KfB	Kirley-Canning complex, 2 to 6 percent slopes	0.00	0.04				0.09		0.04	0.09		
Haakon	476.515	476.606	0.090	477	SD055	354094	KeA	Kirley clay loam, 0 to 2 percent slopes				0.00	0.00	0.00	0.09			0.09	0.00
Haakon	476.606	476.885	0.280	1,477	SD055	354098	KfA	Kirley-Moshier complex, 0 to 2 percent slopes				0.08	0.11	0.28					0.01
Haakon	476.885	477.028	0.142	751	SD055	354097	KfB	Kirley-Canning complex, 2 to 6 percent slopes	0.01	0.06				0.14		0.06	0.14		
Haakon	477.028	477.169	0.142	749	SD055	354094	KeA	Kirley clay loam, 0 to 2 percent slopes				0.01	0.01	0.01	0.14			0.14	0.01
Haakon	477.169	477.347	0.178	939	SD055	354115	Mo	Moshier silt loam				0.15	0.16	0.16	0.18				
Haakon	477.347	477.478	0.131	690	SD055	354094	KeA	Kirley clay loam, 0 to 2 percent slopes				0.01	0.01	0.01	0.13			0.13	0.01
Haakon	477.478	477.613	0.135	711	SD055	354093	Hv	Hoven silt loam					0.13	0.13	0.13				0.12
Haakon	477.613	478.012	0.400	2,131	SD055	354094	KeA	Kirley clay loam, 0 to 2 percent slopes				0.02	0.02	0.02	0.40			0.40	0.02
Haakon	478.012	478.324	0.312	1,645	SD055	354103	KnD	Kirley-Vivian complex, 6 to 15 percent slopes	0.14		0.02			0.22		0.22	0.09		
Haakon	478.324	478.621	0.297	1,568	SD055	354110	LbE	Lakoma-Vivian complex, 9 to 25 percent slopes	0.28	0.02	0.11			0.21		0.30	0.09		
Haakon	478.621	478.798	0.177	935	SD055	354109	LaD	Lakoma silty clay, 6 to 15 percent slopes	0.18		0.01	0.01	0.01	0.01	0.18		0.16		0.01
Haakon	478.798	478.908	0.110	579	SD055	354133	OvA	Ottumwa-Casa complex, 0 to 3 percent slopes	0.00				0.04	0.04	0.11				0.00
Haakon	478.908	479.091	0.183	968	SD055	354117	Nc	Nimbro silty clay loam, channelled				0.01	0.01	0.01	0.18				0.00
Haakon	479.091	479.126	0.036	188	SD055	354116	Nb	Nimbro silty clay loam				0.00	0.00	0.00	0.04			0.04	0.00
Haakon	479.126	479.260	0.133	702	SD055	354143	PrB	Promise clay, 3 to 6 percent slopes				0.12	0.01	0.13	0.13			0.13	0.00
Haakon	479.260	479.554	0.294	1,554	SD055	354122	ObE	Okaton-Lakoma silty clays, 15 to 40 percent slopes	0.27		0.27	0.01	0.01	0.01	0.28	0.27	0.01		
Haakon	479.554	479.690	0.137	721	SD055	354110	LbE	Lakoma-Vivian complex, 9 to 25 percent slopes	0.12	0.01	0.05			0.10		0.14	0.04		
Haakon	479.690	480.065	0.375	1,980	SD055	354103	KnD	Kirley-Vivian complex, 6 to 15 percent slopes	0.17		0.03			0.26		0.26	0.11		
Haakon	480.065	480.275	0.209	1,105	SD055	354162	SfF	Schamber-Samsil complex, 6 to 60 percent slopes	0.10	0.11	0.20	0.06		0.08	0.10		0.21	0.12	
Haakon	480.275	480.702	0.427	2,257	SD055	354158	SoE	Sansarc-Opal clays, 9 to 40 percent slopes	0.38		0.38	0.13	0.03	0.15	0.43	0.38			0.01
Haakon	480.702	480.756	0.054	287	SD055	354069	Ab	Albaton silty clay, depressional						0.05					0.05
Haakon	480.756	480.858	0.102	539	SD055	354117	Nc	Nimbro silty clay loam, channelled				0.01	0.00	0.01	0.10				0.00
Haakon	480.858	481.289	0.430	2,273	SD055	354116	Nb	Nimbro silty clay loam				0.03		0.03	0.43			0.43	0.00
Haakon	481.289	481.348	0.059	311	SD055	354117	Nc	Nimbro silty clay loam, channelled				0.00	0.00	0.00	0.06			0.06	0.00
Haakon	481.348	481.544	0.196	1,037	SD055	354077	Bu	Bulireek clay, 0 to 6 percent slopes				0.19	0.17	0.20	0.20				0.01
Haakon	481.544	482.009	0.465	2,453	SD055	354158	SoE	Sansarc-Opal clays, 9 to 40 percent slopes	0.42		0.42	0.14	0.09	0.16	0.48	0.42			0.01
Haakon	482.009	482.386	0.377	1,993	SD055	354122	ObE	Okaton-Lakoma silty clays, 15 to 40 percent slopes	0.35		0.36	0.02	0.02	0.02	0.37	0.35	0.01		
Haakon	482.386	482.486	0.100	526	SD055	354097	KfB	Kirley-Canning complex, 2 to 6 percent slopes	0.00	0.04				0.09		0.04	0.10		
Haakon	482.486	482.604	0.118	623	SD055	354122	ObE	Okaton-Lakoma silty clays, 15 to 40 percent slopes	0.11		0.11	0.00	0.00	0.00	0.11		0.11	0.00	
Haakon	482.604	482.690	0.086	455	SD055	354109	LaD	Lakoma silty clay, 6 to 15 percent slopes	0.08		0.00	0.00	0.00	0.01	0.08				0.00
Haakon	482.690	482.701	0.011	60	SD055	354122	ObE	Okaton-Lakoma silty clays, 15 to 40 percent slopes	0.01		0.01	0.00	0.00	0.00	0.01		0.01	0.00	
Haakon	482.701	482.797	0.096	507	SD055	354158	SoE	Sansarc-Opal clays, 9 to 40 percent slopes	0.09		0.09	0.03	0.01	0.03	0.10	0.09			0.00
Haakon	482.797	483.033	0.236	1,245	SD055	354122	ObE	Okaton-Lakoma silty clays, 15 to 40 percent slopes	0.22		0.22	0.01	0.01	0.01	0.23		0.22	0.01	
Haakon	483.033	483.396	0.363	1,916	SD055	354107	LaB	Lakoma silty clay, 3 to 6 percent slopes	0.33					0.02	0.36				
Haakon	483.396	483.427	0.030	160	SD055	354122	ObE	Okaton-Lakoma silty clays, 15 to 40 percent slopes	0.03		0.03	0.00	0.00	0.00	0.03		0.03	0.00	
Haakon	483.427	484.135	0.709	3,743	SD055	354107	LaB	Lakoma silty clay, 3 to 6 percent slopes	0.64					0.04	0.71				
Haakon	484.135	484.245	0.110	579	SD055	354110	LbE	Lakoma-Vivian complex, 9 to 25 percent slopes	0.10	0.01	0.04			0.08		0.11	0.03		
Haakon	484.245	484.300	0.055	293	SD055	354095	KeB	Kirley clay loam, 2 to 6 percent slopes	0.00			0.00	0.00	0.00	0.06			0.06	0.00
Haakon	484.300	484.353	0.052	276	SD055	354096	KeD	Kirley clay loam, 6 to 15 percent slopes	0.00			0.00	0.00	0.00	0.05		0.05		
Haakon	484.353	484.484	0.131	693	SD055	354103	KnD	Kirley-Vivian complex, 6 to 15 percent slopes	0.06		0.01			0.09		0.09	0.04		
Haakon	484.484	484.797	0.313	1,654	SD055	354095	KeB	Kirley clay loam, 2 to 6 percent slopes	0.02		0.01	0.01	0.01	0.01	0.31			0.31	0.00
Haakon	484.797	484.874	0.076	403	SD055	354096	KeD	Kirley clay loam, 6 to 15 percent slopes	0.00		0.00	0.00	0.00	0.00	0.07			0.07	
Haakon	484.874	484.931	0.057	301	SD055	354103	KnD	Kirley-Vivian complex, 6 to 15 percent slopes	0.03		0.00			0.04		0.04	0.02		
Jones	484.931	484.953	0.023	119	SD075	353640	KnD	Kirley-Vivian complex, 9 to 25 percent slopes	0.01		0.01			0.02		0.02	0.01		
Jones	484.953	485.092	0.139	732	SD075	353637	KfB	Kirley-Mosh											

Table 1: Soil Limitations Along the Pipeline Centerline Mileposted by Soil Map Unit (continued)

Jones	523.089	523.209	0.114	601	SD075	353643	LaB	Lakoma silty clay, 3 to 6 percent slopes		0.11		0.00		0.01	0.11			0.11	0.00	
Jones	523.203	523.371	0.168	885	SD075	353650	MIB	Millboro silty clay loam, 3 to 6 percent slopes				0.16		0.00	0.16	0.17			0.11	0.00
Jones	523.371	523.392	0.021	309	SD075	353649	MIA	Millboro silty clay loam, 0 to 3 percent slopes				0.02		0.00	0.02	0.02			0.02	0.00
Jones	523.392	523.769	0.378	1,993	SD075	353684	Wt	Witten silty clay				0.37		0.01	0.37	0.38			0.38	0.00
Jones	523.769	523.887	0.118	622	SD075	353650	MIB	Millboro silty clay loam, 3 to 6 percent slopes				0.12		0.00	0.12	0.12			0.12	0.00
Jones	523.887	524.126	0.239	1,261	SD075	353651	MKC	Millboro silty clay loam, 6 to 9 percent slopes	0.01			0.23		0.01	0.23	0.24	0.22		0.38	0.00
Jones	524.126	524.605	0.480	2,532	SD075	353650	MIB	Millboro silty clay loam, 3 to 6 percent slopes				0.47		0.01	0.47	0.48			0.12	0.00
Jones	524.605	525.017	0.412	2,176	SD075	353668	PrA	Promise clay, 0 to 3 percent slopes				0.39		0.02	0.40	0.41				0.48
Jones	525.017	525.662	0.645	3,406	SD085	355608	PoA	Promise clay, 0 to 3 percent slopes		0.02		0.63		0.04	0.65	0.65				0.41
Lyman	525.662	525.718	0.056	296	SD085	355591	MmB	Millboro silty clay, 3 to 6 percent slopes		0.00		0.05		0.00	0.05	0.06			0.05	0.01
Lyman	525.718	526.245	0.527	2,784	SD085	355590	MmA	Millboro silty clay, 0 to 3 percent slopes		0.02		0.49		0.02	0.51	0.53			0.65	0.01
Lyman	526.245	526.300	0.054	287	SD085	355591	MmB	Millboro silty clay, 3 to 6 percent slopes		0.00		0.05		0.00	0.05	0.05			0.06	0.00
Lyman	526.300	526.380	0.080	421	SD085	355590	MmA	Millboro silty clay, 0 to 3 percent slopes		0.00		0.07		0.00	0.08	0.08			0.63	0.02
Lyman	526.380	526.487	0.108	569	SD085	355591	MmB	Millboro silty clay, 3 to 6 percent slopes		0.00		0.10		0.00	0.10	0.11			0.06	0.00
Lyman	526.487	526.488	0.000	2	SD085	355626	Wt	Witten silty clay		0.00		0.00		0.00	0.00	0.00			0.08	0.00
Lyman	526.488	526.600	0.113	595	SD085	355574	Ko	Kolls silty clay				0.01		0.01	0.01	0.11			0.11	0.00
Lyman	526.600	526.714	0.114	599	SD085	355591	MmB	Millboro silty clay, 3 to 6 percent slopes		0.00		0.11		0.00	0.11	0.11			0.00	0.00
Lyman	526.714	527.008	0.294	1,554	SD085	355626	Wt	Witten silty clay		0.01		0.28		0.02	0.29	0.29			0.29	0.01
Lyman	527.008	527.250	0.242	1,279	SD085	355591	MmB	Millboro silty clay, 3 to 6 percent slopes		0.01		0.23		0.01	0.23	0.24			0.24	0.01
Lyman	527.250	527.525	0.274	1,449	SD085	355626	Wt	Witten silty clay		0.01		0.26		0.02	0.27	0.27			0.27	0.01
Lyman	527.525	528.156	0.631	3,320	SD085	355591	MmB	Millboro silty clay, 3 to 6 percent slopes		0.03		0.59		0.03	0.61	0.63			0.63	0.02
Lyman	528.156	528.234	0.079	416	SD085	355608	PoA	Promise clay, 0 to 3 percent slopes		0.00		0.08		0.00	0.08	0.08			0.08	0.00
Lyman	528.234	528.245	0.011	57	SD085	355626	Wt	Witten silty clay		0.00		0.01		0.00	0.01	0.01			0.01	0.00
Lyman	528.245	528.644	0.399	2,107	SD085	355591	MmB	Millboro silty clay, 3 to 6 percent slopes		0.02		0.37		0.02	0.39	0.40			0.40	0.01
Lyman	528.644	528.796	0.151	799	SD085	355593	MnC	Millboro-Boro silty clays, 6 to 9 percent slopes		0.02		0.08			0.08	0.15		0.15		0.01
Lyman	528.796	529.697	0.901	4,758	SD085	355591	MmB	Millboro silty clay, 3 to 6 percent slopes		0.04		0.84		0.04	0.87	0.90		0.15		0.03
Lyman	529.697	529.832	0.135	713	SD085	355593	MnC	Millboro-Boro silty clays, 6 to 9 percent slopes		0.02		0.07			0.07	0.14		0.14		0.00
Lyman	529.832	529.948	0.116	614	SD085	355563	BuA	Bulcreek clay, 0 to 6 percent slopes		0.01		0.11		0.10	0.11	0.12				0.00
Lyman	529.948	530.611	0.662	3,498	SD085	355591	MmB	Millboro silty clay, 3 to 6 percent slopes		0.03		0.62		0.03	0.64	0.65			0.66	0.02
Lyman	530.611	530.721	0.111	584	SD085	355563	BuA	Bulcreek clay, 0 to 6 percent slopes		0.01		0.10		0.10	0.11	0.11				0.00
Lyman	530.721	530.752	0.031	163	SD085	355577	LaC	Lakoma silty clay, 6 to 9 percent slopes		0.03		0.00			0.00	0.03		0.03		0.00
Lyman	530.752	531.321	0.569	3,004	SD085	355591	MmB	Millboro silty clay, 3 to 6 percent slopes		0.02		0.53		0.02	0.55	0.57			0.57	0.02
Lyman	531.321	531.536	0.215	1,136	SD085	355590	MmA	Millboro silty clay, 0 to 3 percent slopes		0.01		0.20		0.01	0.21	0.22			0.22	0.01
Lyman	531.536	532.026	0.490	2,587	SD085	355591	MmB	Millboro silty clay, 3 to 6 percent slopes		0.02		0.46		0.02	0.48	0.49			0.49	0.01
Lyman	532.026	532.419	0.393	2,073	SD085	355590	MmA	Millboro silty clay, 0 to 3 percent slopes		0.02		0.37		0.02	0.38	0.39			0.39	0.01
Lyman	532.419	532.556	0.137	726	SD085	355591	MmB	Millboro silty clay, 3 to 6 percent slopes		0.01		0.13		0.01	0.13	0.14			0.14	0.00
Lyman	532.556	532.786	0.229	1,212	SD085	355593	MnC	Millboro-Boro silty clays, 6 to 9 percent slopes		0.03		0.12			0.12	0.23		0.23		0.00
Lyman	532.786	532.965	0.179	946	SD085	355619	SpE	Sansarc-Opal silty clays, 9 to 40 percent slopes	0.17	0.08		0.01		0.08	0.17		0.17	0.01		0.00
Lyman	532.965	533.041	0.077	405	SD085	355563	BuA	Bulcreek clay, 0 to 6 percent slopes		0.01		0.07		0.07	0.07	0.08			0.08	0.00
Lyman	533.041	533.216	0.174	919	SD085	355619	SpE	Sansarc-Opal silty clays, 9 to 40 percent slopes	0.17	0.08	0.18	0.08	0.01	0.08	0.17		0.17	0.01		0.00
Lyman	533.216	533.443	0.228	1,203	SD085	355578	LbD	Lakoma-Oxaton silty clays, 6 to 15 percent slopes		0.21		0.03			0.03	0.23		0.23		0.00
Lyman	533.443	533.681	0.238	1,255	SD085	355593	MnC	Millboro-Boro silty clays, 6 to 9 percent slopes		0.04		0.12			0.12	0.24		0.24		0.00
Lyman	533.681	533.738	0.057	301	SD085	355591	MmB	Millboro silty clay, 3 to 6 percent slopes		0.00		0.06		0.00	0.06	0.08		0.08		0.00
Lyman	533.738	533.863	0.125	659	SD085	355619	SpE	Sansarc-Opal silty clays, 9 to 40 percent slopes		0.12	0.12	0.06		0.00	0.06	0.12		0.12	0.00	0.00
Lyman	533.863	533.995	0.133	700	SD085	355578	LbD	Lakoma-Oxaton silty clays, 6 to 15 percent slopes		0.12		0.02			0.02	0.13		0.13		0.00
Lyman	533.995	534.124	0.128	678	SD085	355593	MnC	Millboro-Boro silty clays, 6 to 9 percent slopes		0.02		0.07			0.07	0.13		0.13		0.00
Lyman	534.124	534.283	0.159	841	SD085	355578	LbD	Lakoma-Oxaton silty clays, 6 to 15 percent slopes		0.15		0.02			0.02	0.16		0.16		0.00
Lyman	534.283	534.651	0.368	1,941	SD085	355593	MnC	Millboro-Boro silty clays, 6 to 9 percent slopes		0.06		0.19			0.19	0.37		0.37		0.00
Lyman	534.651	535.246	0.595	3,142	SD085	355591	MmB	Millboro silty clay, 3 to 6 percent slopes		0.02		0.56		0.02	0.58	0.60			0.60	0.02
Lyman	535.246	535.500	0.254	1,343	SD085	355572	HrA	Cape silt loam, 0 to 6 percent slopes		0.01		0.04		0.23	0.25	0.25				0.60
Lyman	535.500	535.586	0.086	454	SD085	355591	MmB	Millboro silty clay, 3 to 6 percent slopes		0.00		0.08		0.00	0.08	0.09			0.09	0.00
Lyman	535.586	535.774	0.188	992	SD085	355597	OhE	Oxaton-Lakoma silty clays, 15 to 40 percent slopes	0.18	0.01	0.19	0.01		0.01	0.18		0.19	0.01		0.00
Lyman	535.774	535.821	0.047	250	SD085	355619	SpE	Sansarc-Opal silty clays, 9 to 40 percent slopes	0.05	0.00	0.04	0.02	0.00	0.02	0.05		0.05	0.00		0.00
Lyman	535.821	535.834	0.013	70	SD085	355597	OhE	Oxaton-Lakoma silty clays, 15 to 40 percent slopes	0.01	0.00	0.01	0.00		0.00	0.01		0.01	0.00		0.00
Lyman	535.834	535.926	0.092	484	SD085	355619	SpE	Sansarc-Opal silty clays, 9 to 40 percent slopes	0.09	0.00	0.09	0.04	0.00	0.04	0.09		0.09	0.00		0.00
Lyman	535.926	536.025	0.099	521	SD085	355597	OhE	Oxaton-Lakoma silty clays, 15 to 40 percent slopes	0.09	0.00	0.10	0.04		0.00	0.09		0.10	0.00		0.00
Lyman	536.025	536.612	0.587	3,102	SD085	355619	SpE	Sansarc-Opal silty clays, 9 to 40 percent slopes	0.58	0.00	0.55	0.28	0.02	0.28	0.57		0.57	0.02		0.01
Lyman	536.612	536.668	0.055	293	SD085	355563	BuA	Bulcreek clay, 0 to 6 percent slopes		0.00		0.05		0.05	0.05	0.06			0.06	0.00
Lyman	536.668	536.749	0.081	428	SD085	355608	PoA	Promise clay, 0 to 3 percent slopes		0.00		0.08		0.00	0.08	0.08			0.08	0.00
Lyman	536.749	536.814	0.065	345	SD085	355570	Hm	Hillmoes silty clay		0.00		0.06			0.06	0.06				

Table 1: Soil Limitations Along the Pipeline Centerline Mileposted by Soil Map Unit (continued)

Tripp	563.649	563.778	0.129	682	SD123	354406	LoD	Lakoma-Okaton silty clays, 9 to 15 percent slopes	0.11	0.01	0.01			0.01	0.12	0.01			0.00
Tripp	563.778	563.879	0.101	531	SD123	354378	CbD	Canning-Murdo loams, 6 to 15 percent slopes		0.09				0.09	0.09	0.09			0.00
Tripp	563.879	563.954	0.075	395	SD123	354377	CaB	Canning loam, 2 to 5 percent slopes		0.07				0.07	0.07	0.07		0.07	0.00
Tripp	563.954	563.962	0.008	44	SD123	354378	CbD	Canning-Murdo loams, 6 to 15 percent slopes		0.01				0.01	0.01	0.01			0.00
Tripp	563.962	563.983	0.021	110	SD123	354377	CaB	Canning loam, 2 to 5 percent slopes		0.02				0.02	0.02	0.02		0.02	0.00
Tripp	563.983	564.051	0.068	361	SD123	354378	CbD	Canning-Murdo loams, 6 to 15 percent slopes		0.06				0.06	0.06	0.06		0.06	0.00
Tripp	564.051	564.303	0.252	1,328	SD123	354406	LoD	Lakoma-Okaton silty clays, 9 to 15 percent slopes	0.21	0.01	0.02		0.02	0.24	0.24	0.01			0.00
Tripp	564.303	564.535	0.232	1,224	SD123	354405	LkC	Lakoma-Millboro silty clays, 5 to 9 percent slopes	0.12		0.09	0.00		0.09	0.23	0.21			0.00
Tripp	564.535	564.567	0.033	172	SD123	354406	LoD	Lakoma-Okaton silty clays, 9 to 15 percent slopes	0.03	0.00	0.00		0.00	0.03	0.03	0.03		0.00	
Tripp	564.567	564.619	0.051	771	SD123	354378	CbD	Canning-Murdo loams, 6 to 15 percent slopes		0.04				0.05	0.04	0.04			0.00
Tripp	564.619	564.759	0.140	741	SD123	354406	LoD	Lakoma-Okaton silty clays, 9 to 15 percent slopes	0.12	0.01	0.01		0.01	0.13	0.13	0.01			0.00
Tripp	564.759	564.858	0.099	520	SD123	354405	LkC	Lakoma-Millboro silty clays, 5 to 9 percent slopes	0.05		0.04	0.00		0.04	0.10	0.09			0.00
Tripp	564.858	565.049	0.191	1,009	SD123	354413	MoB	Millboro silty clay, 3 to 6 percent slopes	0.01	0.00	0.17	0.02		0.18	0.19	0.19		0.00	0.00
Tripp	565.049	565.299	0.250	1,322	SD123	354405	LkC	Lakoma-Millboro silty clays, 5 to 9 percent slopes	0.13		0.10	0.00		0.10	0.25	0.22		0.19	0.00
Tripp	565.299	565.395	0.096	506	SD123	354413	MoB	Millboro silty clay, 3 to 6 percent slopes	0.00	0.00	0.09	0.01		0.09	0.09	0.00		0.10	0.00
Tripp	565.395	565.452	0.058	305	SD123	354412	MoA	Millboro silty clay, 0 to 3 percent slopes		0.06	0.00			0.06	0.06	0.06		0.06	0.00
Tripp	565.452	565.554	0.101	533	SD123	354413	MoB	Millboro silty clay, 3 to 6 percent slopes	0.00	0.00	0.09	0.01		0.09	0.10	0.09		0.10	0.00
Tripp	565.554	565.623	0.070	368	SD123	354405	LkC	Lakoma-Millboro silty clays, 5 to 9 percent slopes	0.04		0.03	0.00		0.03	0.07	0.06		0.10	0.00
Tripp	565.623	565.721	0.098	517	SD123	354400	Ic	Inavle complex, channelled		0.08				0.01	0.01	0.08			0.00
Tripp	565.721	566.083	0.362	1,913	SD123	354375	Bp	Bridgeport complex	0.01		0.10	0.05	0.00	0.10	0.35			0.38	0.00
Tripp	566.083	566.108	0.025	132	SD123	354370	AvA	Anselmo-Vetal fine sandy loams, 0 to 3 percent slopes	0.00	0.02	0.00	0.00	0.00	0.00	0.00			0.03	0.00
Tripp	566.108	566.245	0.136	720	SD123	354375	Bp	Bridgeport complex		0.00	0.04	0.02	0.00	0.04	0.13			0.14	0.00
Tripp	566.245	566.534	0.289	1,526	SD123	354370	AvA	Anselmo-Vetal fine sandy loams, 0 to 3 percent slopes	0.01	0.19	0.01	0.01	0.01	0.01	0.01			0.29	0.01
Tripp	566.534	566.659	0.126	663	SD123	354375	Bp	Bridgeport complex		0.00	0.04	0.02	0.00	0.04	0.12			0.13	0.00
Tripp	566.659	566.965	0.305	1,612	SD123	354465	Wn	Written silty clay		0.30	0.02			0.30	0.31			0.31	0.01
Tripp	566.965	567.171	0.206	1,089	SD123	354412	MoA	Millboro silty clay, 0 to 3 percent slopes	0.20		0.01	0.00		0.20	0.21			0.21	0.00
Tripp	567.171	567.255	0.084	445	SD123	354465	Wn	Written silty clay		0.08	0.00			0.08	0.08			0.08	0.00
Tripp	567.255	567.418	0.163	859	SD123	354412	MoA	Millboro silty clay, 0 to 3 percent slopes	0.01		0.16	0.01		0.16	0.16			0.16	0.00
Tripp	567.418	567.689	0.271	1,433	SD123	354413	MoB	Millboro silty clay, 3 to 6 percent slopes		0.00	0.24	0.02		0.25	0.27		0.00	0.27	0.00
Tripp	567.689	567.847	0.157	831	SD123	354412	MoA	Millboro silty clay, 0 to 3 percent slopes	0.00	0.00	0.16	0.01		0.16	0.16			0.16	0.00
Tripp	567.847	567.860	0.013	68	SD123	354413	MoB	Millboro silty clay, 3 to 6 percent slopes	0.04		0.03	0.00		0.03	0.01			0.01	0.00
Tripp	567.860	567.930	0.071	372	SD123	354405	LkC	Lakoma-Millboro silty clays, 5 to 9 percent slopes		0.59	0.03	0.04		0.04	0.66		0.06	0.03	0.00
Tripp	567.930	568.619	0.689	3,639	SD123	354406	LoD	Lakoma-Okaton silty clays, 9 to 15 percent slopes	0.01	0.01	0.01	0.01	0.01	0.27	0.25	0.01		0.27	0.01
Tripp	568.619	568.894	0.274	1,448	SD123	354434	RaC	Ree loam, 6 to 9 percent slopes	0.00	0.00	0.02	0.00	0.00	0.02	0.02	0.00		0.02	0.00
Tripp	568.894	569.013	0.020	104	SD123	354414	MoC	Millboro silty clay, 6 to 9 percent slopes	0.01	0.01	0.01	0.01	0.01	0.37	0.33	0.01		0.37	0.01
Tripp	569.013	569.279	0.265	1,939	SD123	354434	RaC	Ree loam, 6 to 9 percent slopes	0.04		0.03	0.00	0.00	0.03	0.06	0.07		0.03	0.00
Tripp	569.279	569.361	0.082	433	SD123	354405	LkC	Lakoma-Millboro silty clays, 5 to 9 percent slopes	0.01	0.01	0.01	0.01	0.01	0.18	0.17	0.01		0.18	0.01
Tripp	569.361	569.546	0.185	975	SD123	354434	RaC	Ree loam, 6 to 9 percent slopes	0.01	0.01	0.01	0.01	0.01	0.09	0.10	0.01		0.10	0.01
Tripp	569.546	569.647	0.101	534	SD123	354435	RaD	Ree loam, 9 to 15 percent slopes	0.00	0.00	0.00	0.00	0.00	0.15	0.14	0.00		0.15	0.01
Tripp	569.647	569.801	0.154	815	SD123	354434	RaC	Ree loam, 6 to 9 percent slopes	0.00	0.00	0.00	0.00	0.00	0.14	0.14	0.00		0.14	0.00
Tripp	569.801	569.944	0.143	753	SD123	354438	PrC	Promise clay, 6 to 9 percent slopes	0.00	0.00	0.13	0.00		0.14	0.14			0.14	0.00
Tripp	569.944	570.016	0.073	384	SD123	354414	MoC	Millboro silty clay, 6 to 9 percent slopes	0.00	0.00	0.06	0.00		0.06	0.07	0.07		0.00	0.00
Tripp	570.016	570.101	0.084	446	SD123	354569	ALD	Anselmo-Lonsipine fine sandy loams, 10 to 20 percent slopes	0.00	0.03	0.07	0.00		0.07	0.07	0.01		0.07	0.02
Tripp	570.101	570.518	0.418	2,205	SD123	354434	RaC	Ree loam, 6 to 9 percent slopes	0.01	0.01	0.01	0.01	0.01	0.42	0.38	0.01		0.42	0.02
Tripp	570.518	570.641	0.123	647	SD123	354409	MaB	Manter fine sandy loam, 3 to 9 percent slopes	0.01	0.12				0.00	0.00			0.00	0.12
Tripp	570.641	570.732	0.092	483	SD123	354408	MaA	Manter fine sandy loam, 0 to 3 percent slopes		0.09				0.00	0.09			0.09	0.00
Tripp	570.732	570.882	0.150	792	SD123	354409	MaB	Manter fine sandy loam, 3 to 9 percent slopes	0.01	0.14				0.00	0.00			0.00	0.15
Tripp	570.882	571.093	0.211	1,112	SD123	354365	AbB	Anselmo fine sandy loam, 3 to 6 percent slopes	0.01	0.21				0.01	0.01			0.21	0.00
Tripp	571.093	571.197	0.104	548	SD123	354370	AvA	Anselmo-Vetal fine sandy loams, 0 to 3 percent slopes	0.01	0.07	0.00	0.00	0.00	0.00	0.00			0.10	0.00
Tripp	571.197	571.326	0.129	680	SD123	354385	OgB	Dogier loamy fine sand, 0 to 6 percent slopes	0.00	0.00	0.12	0.00	0.00	0.00	0.00			0.00	0.00
Tripp	571.326	571.399	0.003	16	SD123	354388	DuC	Dunday-Dogier loamy fine sands, 3 to 9 percent slopes		0.00				0.00	0.00			0.00	0.00
Tripp	571.399	571.390	0.002	325	SD123	354385	OgB	Dogier loamy fine sand, 0 to 6 percent slopes	0.00	0.00	0.06	0.00	0.00	0.00	0.00			0.00	0.00
Tripp	571.390	571.439	0.049	259	SD123	354388	DuC	Dunday-Dogier loamy fine sands, 3 to 9 percent slopes		0.05				0.05	0.05			0.05	0.00
Tripp	571.439	571.609	0.170	895	SD123	354364	AA82	Anselmo loamy fine sand, 0 to 9 percent slopes, eroded		0.15				0.15	0.15			0.15	0.00
Tripp	571.609	572.182	0.573	3,025	SD123	354454	VdC	Valentine-Dunday complex, 3 to 9 percent slopes	0.01	0.02	0.56			0.64	0.64	0.02		0.60	0.01
Tripp	572.182	572.241	0.060	316	SD123	354385	DmA	Dogier-Elmire complex, 0 to 3 percent slopes		0.00	0.03	0.00	0.00	0.00	0.00	0.03		0.00	0.00
Tripp	572.241	572.354	0.113	596	SD123	354454	VdC	Valentine-Dunday complex, 3 to 9 percent slopes	0.00	0.00	0.11			0.11	0.11			0.00	0.00
Tripp	572.354	572.541	0.187	989	SD123	354385	DmA	Dogier-Elmire complex, 0 to 3 percent slopes	0.00	0.10		0.00	0.00	0.00	0.01	0.10		0.00	0.01
Tripp	572.541	572.657	0.116	613	SD123	354405	LkC	Lakoma-Millboro silty clays, 5 to 9 percent slopes		0.06		0.05		0.05	0.12		0.10		0.00
Tripp	572.657	573.083	0.426	2,348	SD123	354462	WgB	Wewilla fine sandy loam, 3 to 6 percent slopes	0.38	0.02	0.00	0.00	0.00	0.39				0.00	0.00
Tripp	573.083	573.338																	

Table 1: Soil Limitations Along the Pipeline Centerline Mileposted by Soil Map Unit (continued)

Tripp	574.070	574.175	0.105	555	SD123	354387	DnC2	Dunday loamy fine sand, 3 to 9 percent slopes, eroded	0.00	0.00	0.10							0.10		0.00	0.00		
Tripp	574.175	574.244	0.069	365	SD123	354454	VdC	Valentine-Dunday complex, 3 to 9 percent slopes	0.00	0.00	0.07								0.07		0.00	0.00	
Tripp	574.244	574.315	0.071	374	SD123	354386	DmA	Doger-Elsmere complex, 0 to 3 percent slopes	0.00	0.00	0.04			0.00	0.00	0.00	0.00	0.00	0.04			0.00	
Tripp	574.315	574.387	0.071	376	SD123	354387	DnC2	Dunday loamy fine sand, 3 to 9 percent slopes, eroded	0.00	0.00	0.07								0.07		0.00	0.00	
Tripp	574.387	574.547	0.160	847	SD123	354389	Em	Elsmere fine sandy loam			0.01			0.01	0.01	0.01	0.01	0.01	0.01		0.16	0.01	
Tripp	574.547	574.613	0.066	349	SD123	354387	DnC2	Dunday loamy fine sand, 3 to 9 percent slopes, eroded	0.00	0.00	0.06								0.06		0.00	0.00	
Tripp	574.613	574.686	0.073	383	SD123	354386	DmA	Doger-Elsmere complex, 0 to 3 percent slopes			0.04			0.00	0.00	0.00	0.00	0.00	0.04			0.00	
Tripp	574.686	575.191	0.505	2,668	SD123	354455	VnD	Valentine-Longline complex, 6 to 15 percent slopes	0.01	0.11	0.50								0.39		0.11	0.00	
Tripp	575.191	575.195	0.004	22	SD123	354454	VdC	Valentine-Dunday complex, 3 to 9 percent slopes	0.00	0.00	0.00								0.00		0.00	0.00	
Tripp	575.195	575.748	0.553	2,921	SD123	354387	DnC2	Dunday loamy fine sand, 3 to 9 percent slopes, eroded	0.01	0.01	0.54								0.54		0.01	0.01	
Tripp	575.748	575.953	0.205	1,080	SD123	354441	RoB	Ronson-Longline fine sandy loams, 0 to 6 percent slopes			0.16			0.00	0.00	0.00	0.00	0.00	0.01		0.07	0.00	
Tripp	575.953	576.110	0.157	829	SD123	354455	VnD	Valentine-Longline complex, 6 to 15 percent slopes	0.00	0.03	0.15								0.12		0.03	0.00	
Tripp	576.110	576.224	0.114	600	SD123	354387	DnC2	Dunday loamy fine sand, 3 to 9 percent slopes, eroded	0.00	0.00	0.11								0.11		0.00	0.00	
Tripp	576.224	576.406	0.182	962	SD123	354386	DmA	Doger-Elsmere complex, 0 to 3 percent slopes			0.10			0.00	0.00	0.00	0.00	0.01	0.10			0.01	
Tripp	576.406	576.444	0.038	201	SD123	354389	Em	Elsmere fine sandy loam			0.00			0.00	0.00	0.00	0.00	0.00	0.00		0.04	0.00	
Tripp	576.444	576.542	0.098	519	SD123	354386	DmA	Doger-Elsmere complex, 0 to 3 percent slopes	0.00	0.05	0.00			0.00	0.00	0.00	0.00	0.00	0.05			0.00	
Tripp	576.542	576.619	0.077	406	SD123	354389	Em	Elsmere fine sandy loam			0.00			0.00	0.00	0.00	0.00	0.00	0.00		0.08	0.00	
Tripp	576.619	576.778	0.159	837	SD123	354386	DmA	Doger-Elsmere complex, 0 to 3 percent slopes	0.00	0.00	0.08			0.00	0.00	0.00	0.00	0.00	0.08			0.00	
Tripp	576.778	576.882	0.104	549	SD123	354387	DnC2	Dunday loamy fine sand, 3 to 9 percent slopes, eroded	0.00	0.00	0.10								0.10		0.00	0.00	
Tripp	576.882	577.017	0.135	712	SD123	354440	RfA	Ronson fine sandy loam, 0 to 6 percent slopes			0.12			0.00	0.00	0.00	0.00	0.00	0.00			0.00	
Tripp	577.017	577.194	0.177	937	SD123	354388	AhC	Anselmo-Holt fine sandy loams, 3 to 9 percent slopes	0.00	0.00	0.08			0.00	0.00	0.00	0.00	0.00	0.00		0.01	0.18	
Tripp	577.194	577.287	0.092	488	SD123	354385	DgB	Doger loamy fine sand, 0 to 6 percent slopes			0.00			0.00	0.00	0.00	0.00	0.00	0.00		0.00	0.00	
Tripp	577.287	577.375	0.089	469	SD123	354385	Abb	Anselmo fine sandy loam			0.00			0.00	0.00	0.00	0.00	0.00	0.00		0.09	0.00	
Tripp	577.375	577.592	0.217	1,146	SD123	354389	Em	Elsmere fine sandy loam			0.01			0.01	0.01	0.01	0.01	0.01	0.01		0.09	0.00	
Tripp	577.592	577.634	0.041	218	SD123	354385	DgB	Doger loamy fine sand, 0 to 6 percent slopes	0.00	0.00	0.04			0.00	0.00	0.00	0.00	0.00	0.04		0.00	0.22	
Tripp	577.634	577.874	0.240	1,267	SD123	354388	AhC	Anselmo-Holt fine sandy loams, 3 to 9 percent slopes			0.11			0.00	0.00	0.00	0.00	0.00	0.00		0.01	0.24	
Tripp	577.874	577.917	0.043	228	SD123	354456	Vt	Vestal fine sandy loam	0.00	0.00	0.00			0.00	0.00	0.00	0.00	0.00	0.00		0.00	0.04	
Tripp	577.917	578.044	0.127	673	SD123	354385	DgB	Doger loamy fine sand, 0 to 6 percent slopes	0.00	0.00	0.12			0.00	0.00	0.00	0.00	0.00	0.00		0.00	0.00	
Tripp	578.044	578.114	0.070	367	SD123	354387	DnC2	Dunday loamy fine sand, 3 to 9 percent slopes, eroded	0.00	0.00	0.07								0.07		0.00	0.00	
Tripp	578.114	578.366	0.253	1,335	SD123	354388	AhC	Anselmo-Holt fine sandy loams, 3 to 9 percent slopes			0.11			0.00	0.00	0.00	0.00	0.00	0.00		0.01	0.25	
Tripp	578.366	578.417	0.050	265	SD123	354395	HbA	Holt-Anselmo fine sandy loams, 0 to 3 percent slopes	0.00	0.03	0.05								0.00		0.00	0.00	
Tripp	578.417	578.791	0.375	1,979	SD123	354387	DnC2	Dunday loamy fine sand, 3 to 9 percent slopes, eroded	0.00	0.00	0.36								0.36		0.00	0.00	
Tripp	578.791	578.884	0.093	489	SD123	354463	Wh	White Lake fine sandy loam	0.00	0.01	0.01			0.00	0.08	0.08	0.08	0.08	0.08		0.00	0.00	
Tripp	578.884	579.007	0.122	646	SD123	354385	DgB	Doger loamy fine sand, 0 to 6 percent slopes	0.00	0.00	0.12			0.00	0.00	0.00	0.00	0.00	0.00		0.00	0.00	
Tripp	579.007	579.189	0.182	963	SD123	354463	Wh	White Lake fine sandy loam	0.00	0.00	0.14			0.00	0.00	0.00	0.00	0.00	0.13		0.00	0.00	
Tripp	579.189	579.335	0.146	768	SD123	354385	DgB	Doger loamy fine sand, 0 to 6 percent slopes	0.00	0.00	0.01			0.02	0.03	0.06	0.06	0.06	0.06		0.00	0.00	
Tripp	579.335	579.403	0.069	364	SD123	354464	Wh	White Lake-Lute fine sandy loams			0.24			0.35					0.01		0.00	0.00	
Tripp	579.403	579.776	0.372	1,964	SD123	354395	HbA	Holt-Anselmo fine sandy loams, 0 to 3 percent slopes	0.00	0.20	0.01			0.00	0.00	0.00	0.00	0.00	0.20		0.00	0.00	
Tripp	579.776	579.993	0.217	1,145	SD123	354462	WgB	Wewela fine sandy loam, 3 to 6 percent slopes	0.00	0.00	0.04			0.00	0.00	0.00	0.00	0.00	0.00		0.00	0.00	
Tripp	579.993	580.051	0.058	307	SD123	354370	AWA	Anselmo-Vestal fine sandy loams, 0 to 3 percent slopes	0.00	0.22	0.01			0.00	0.00	0.00	0.00	0.00	0.22		0.00	0.00	
Tripp	580.051	580.294	0.243	1,284	SD123	354462	WgB	Wewela fine sandy loam, 3 to 6 percent slopes	0.00	0.13	0.01			0.00	0.00	0.00	0.00	0.00	0.00		0.00	0.00	
Tripp	580.294	580.447	0.153	808	SD123	354461	WgA	Wewela fine sandy loam, 0 to 3 percent slopes	0.00	0.03	0.00			0.00	0.00	0.00	0.00	0.00	0.00		0.00	0.00	
Tripp	580.447	580.479	0.032	166	SD123	354462	WgB	Wewela fine sandy loam, 3 to 6 percent slopes	0.00	0.03	0.00			0.00	0.00	0.00	0.00	0.00	0.03		0.00	0.00	
Tripp	580.479	580.531	0.053	277	SD123	354452	TrF	Longline-Rock outcrop complex, 15 to 40 percent slopes	0.02	0.04	0.03		0.05						0.00	0.05		0.00	0.04
Tripp	580.531	580.642	0.111	586	SD123	354385	DgB	Doger loamy fine sand, 0 to 6 percent slopes	0.00	0.00	0.11			0.00	0.00	0.00	0.00	0.00	0.10		0.00	0.00	
Tripp	580.642	580.828	0.186	983	SD123	354463	Wh	White Lake fine sandy loam	0.00	0.01	0.00			0.00	0.17	0.17	0.17	0.17	0.17		0.01	0.00	
Tripp	580.828	580.972	0.144	759	SD123	354464	Wh	White Lake-Lute fine sandy loams	0.00	0.03	0.04			0.07	0.12	0.12	0.12	0.12	0.12		0.01	0.00	
Tripp	580.972	581.008	0.037	194	SD123	354463	Wh	White Lake fine sandy loam	0.00	0.00	0.03			0.03	0.03	0.03	0.03	0.03	0.03		0.00	0.00	
Tripp	581.008	581.035	0.026	139	SD123	354464	Wh	White Lake-Lute fine sandy loams	0.00	0.01	0.01			0.01	0.02	0.02	0.02	0.02	0.02		0.00	0.00	
Tripp	581.035	581.237	0.202	1,067	SD123	354463	Wh	White Lake fine sandy loam	0.00	0.01	0.00			0.18	0.18	0.18	0.18	0.18	0.18		0.01	0.00	
Tripp	581.237	581.330	0.093	491	SD123	354385	DgB	Doger loamy fine sand, 0 to 6 percent slopes	0.00	0.00	0.09			0.00	0.00	0.00	0.00	0.00	0.00		0.00	0.00	
Tripp	581.330	581.476	0.145	768	SD123	354388	DuC	Dunday-Doger loamy fine sands, 3 to 9 percent slopes			0.14								0.09			0.00	
Tripp	581.476	581.853	0.378	1,994	SD123	354455	VnD	Valentine-Longline complex, 6 to 15 percent slopes	0.01	0.08	0.37								0.29		0.08	0.00	
Tripp	581.853	581.938	0.084	445	SD123	354385	DgB	Doger loamy fine sand, 0 to 6 percent slopes	0.00	0.00	0.08			0.00	0.00	0.00	0.00	0.00	0.00		0.00	0.00	
Tripp	581.938	581.982	0.045	236	SD123	354455	VnD	Valentine-Longline complex, 6 to 15 percent slopes	0.00	0.01	0.04								0.03		0.0		

Table 1: Soil Limitations Along the Pipeline Centerline Mileposted by Soil Map Unit (continued)

Tripp	582.852	582.960	0.108	570	SD123	354387	DnC2	Dunday loamy fine sand, 3 to 9 percent slopes, eroded	0.00	0.00	0.10							0.10				0.00	0.00		
Tripp	582.960	583.013	0.054	283	SD123	354454	VdC	Valentine-Dunday complex, 3 to 9 percent slopes	0.00	0.00	0.05								0.05				0.00	0.00	
Tripp	583.013	583.032	0.019	98	SD123	354385	DgB	Doger loamy fine sand, 0 to 6 percent slopes	0.00	0.00	0.02		0.00	0.00	0.00	0.00	0.00	0.00	0.02				0.00	0.00	
Tripp	583.032	583.108	0.076	399	SD123	354454	VdC	Valentine-Dunday complex, 3 to 9 percent slopes	0.00	0.00	0.07								0.07				0.00	0.00	
Tripp	583.108	583.281	0.173	914	SD123	354385	DgB	Doger loamy fine sand, 0 to 6 percent slopes	0.00	0.00	0.16		0.00	0.00	0.00	0.00	0.00	0.00	0.16				0.00	0.00	
Tripp	583.281	583.357	0.077	404	SD123	354454	VdC	Valentine-Dunday complex, 3 to 9 percent slopes	0.00	0.00	0.07								0.07				0.00	0.00	
Tripp	583.357	583.564	0.207	1,093	SD123	354387	DnC2	Dunday loamy fine sand, 3 to 9 percent slopes, eroded	0.00	0.00	0.20								0.20				0.00	0.00	
Tripp	583.564	583.646	0.082	431	SD123	354386	DmA	Doger-Elmora complex, 0 to 3 percent slopes	0.00	0.00	0.04		0.00	0.00	0.00	0.00	0.00	0.00	0.04				0.00	0.00	
Tripp	583.646	583.850	0.204	1,079	SD123	354388	DuC	Dunday-Doger loamy fine sands, 3 to 9 percent slopes			0.19								0.19				0.00	0.00	
Tripp	583.850	583.894	0.044	232	SD123	354440	RIa	Ronson fine sandy loam, 0 to 4 percent slopes		0.04	0.00		0.00	0.00	0.00	0.00	0.00	0.00	0.00				0.00	0.00	
Tripp	583.894	583.898	0.003	18	SD123	354388	DuC	Dunday-Doger loamy fine sands, 3 to 9 percent slopes			0.00								0.00				0.00	0.00	
Tripp	583.898	584.292	0.394	2,080	SD123	354385	DgB	Doger loamy fine sand, 0 to 6 percent slopes	0.00	0.00	0.37		0.00	0.00	0.00	0.00	0.00	0.00	0.36				0.00	0.00	
Tripp	584.292	584.411	0.119	630	SD123	354386	DmA	Doger-Elmora complex, 0 to 3 percent slopes			0.00	0.06		0.00	0.00	0.00	0.00	0.00	0.06				0.00	0.00	
Tripp	584.411	584.675	0.264	1,396	SD123	354387	DnC2	Dunday loamy fine sand, 3 to 9 percent slopes, eroded	0.00	0.00	0.26								0.26				0.00	0.00	
Tripp	584.675	584.854	0.178	942	SD123	354385	DgB	Doger loamy fine sand, 0 to 6 percent slopes	0.00	0.00	0.17		0.00	0.00	0.00	0.00	0.00	0.00	0.16				0.00	0.00	
Tripp	584.854	584.942	0.089	469	SD123	354395	HbA	Holt-Anselmo fine sandy loams, 0 to 3 percent slopes		0.06	0.08												0.00	0.00	
Tripp	584.942	585.017	0.074	392	SD123	354388	DuC	Dunday-Doger loamy fine sands, 3 to 9 percent slopes			0.07								0.07				0.00	0.00	
Tripp	585.017	585.305	0.289	1,524	SD123	354462	WgB	Wewela fine sandy loam, 3 to 6 percent slopes		0.26	0.01		0.00	0.00	0.00	0.00	0.00	0.26				0.00	0.00	0.00	
Tripp	585.305	585.308	0.002	13	SD123	354385	DgB	Doger loamy fine sand, 0 to 6 percent slopes	0.00	0.00	0.00		0.00	0.00	0.00	0.00	0.00	0.00	0.00				0.00	0.00	
Tripp	585.308	585.409	0.101	535	SD123	354368	AhC	Anselmo-Holt fine sandy loams, 3 to 9 percent slopes		0.00	0.05	0.10							0.04				0.01	0.10	0.00
Tripp	585.409	585.410	0.001	8	SD123	354385	DgB	Doger loamy fine sand, 0 to 6 percent slopes	0.00	0.00	0.00		0.00	0.00	0.00	0.00	0.00	0.00	0.00				0.00	0.00	
Tripp	585.410	585.543	0.133	700	SD123	354368	AhC	Anselmo-Holt fine sandy loams, 3 to 9 percent slopes		0.06	0.13								0.09				0.01	0.13	0.00
Tripp	585.543	585.646	0.103	545	SD123	354385	DgB	Doger loamy fine sand, 0 to 6 percent slopes	0.00	0.00	0.10		0.00	0.00	0.00	0.00	0.00	0.00	0.09				0.00	0.00	
Tripp	585.646	585.715	0.069	365	SD123	354386	DmA	Doger-Elmora complex, 0 to 3 percent slopes		0.00	0.04		0.00	0.00	0.00	0.00	0.00	0.00	0.04				0.00	0.00	
Tripp	585.715	585.853	0.137	725	SD123	354388	DuC	Dunday-Doger loamy fine sands, 3 to 9 percent slopes			0.13								0.13				0.00	0.00	
Tripp	585.853	585.937	0.084	445	SD123	354387	DnC2	Dunday loamy fine sand, 3 to 9 percent slopes, eroded	0.00	0.00	0.08								0.08				0.00	0.00	
Tripp	585.937	586.175	0.239	1,260	SD123	354388	DuC	Dunday-Doger loamy fine sands, 3 to 9 percent slopes			0.23								0.23				0.00	0.00	
Tripp	586.175	586.380	0.205	1,080	SD123	354385	DgB	Doger loamy fine sand, 0 to 6 percent slopes	0.00	0.00	0.19		0.00	0.00	0.00	0.00	0.00	0.00	0.19				0.00	0.00	
Tripp	586.380	586.633	0.253	1,337	SD123	354388	DuC	Dunday-Doger loamy fine sands, 3 to 9 percent slopes			0.24								0.24				0.00	0.00	
Tripp	586.633	587.126	0.492	2,600	SD123	354385	DgB	Doger loamy fine sand, 0 to 6 percent slopes	0.00	0.00	0.47		0.00	0.00	0.00	0.00	0.00	0.00	0.45				0.00	0.00	
Tripp	587.126	587.618	0.492	2,599	SD123	354368	AhC	Anselmo-Holt fine sandy loams, 3 to 9 percent slopes		0.22	0.47								0.02				0.00	0.48	0.00
Tripp	587.618	587.717	0.099	524	SD123	354395	HbA	Holt-Anselmo fine sandy loams, 0 to 3 percent slopes		0.06	0.09								0.00				0.00	0.00	
Tripp	587.717	588.197	0.480	2,534	SD123	354368	AhC	Anselmo-Holt fine sandy loams, 3 to 9 percent slopes		0.22	0.46								0.02				0.00	0.48	0.00
Tripp	588.197	588.215	0.018	95	SD123	354385	DgB	Doger loamy fine sand, 0 to 6 percent slopes	0.00	0.00	0.02		0.00	0.00	0.00	0.00	0.00	0.00	0.02				0.00	0.00	
Tripp	588.215	588.331	0.115	609	SD123	354386	DmA	Doger-Elmora complex, 0 to 3 percent slopes		0.00	0.00	0.06		0.00	0.00	0.00	0.00	0.00	0.06				0.00	0.00	
Tripp	588.331	588.418	0.087	460	SD123	354387	DnC2	Dunday loamy fine sand, 3 to 9 percent slopes, eroded	0.00	0.00	0.08								0.08				0.00	0.00	
Tripp	588.418	588.626	0.208	1,100	SD123	354441	RoB	Ronson-Longpine fine sandy loams, 0 to 6 percent slopes		0.17	0.10		0.00	0.00	0.00	0.00	0.00	0.00	0.01				0.00	0.00	
Tripp	588.626	588.750	0.124	655	SD123	354440	RIa	Ronson fine sandy loam, 0 to 4 percent slopes		0.11	0.01		0.00	0.00	0.00	0.00	0.00	0.00	0.00				0.00	0.00	
Tripp	588.750	588.789	0.039	207	SD123	354369	AID	Anselmo-Longpine fine sandy loams, 10 to 20 percent slopes	0.00	0.01	0.03	0.00						0.00	0.03				0.00	0.00	
Tripp	588.789	589.051	0.262	1,383	SD123	354410	MfE	Manter-Anselmo fine sandy loams, 15 to 30 percent slopes		0.03	0.23	0.24						0.03	0.26				0.01	0.01	
Tripp	589.051	589.176	0.125	662	SD123	354369	AID	Anselmo-Longpine fine sandy loams, 10 to 20 percent slopes	0.01	0.04	0.11	0.01						0.01	0.10				0.00	0.00	
Tripp	589.176	589.240	0.063	335	SD123	354395	HbA	Holt-Anselmo fine sandy loams, 0 to 3 percent slopes		0.04	0.06								0.00				0.00	0.00	
Tripp	589.240	589.336	0.096	509	SD123	354369	AID	Anselmo-Longpine fine sandy loams, 10 to 20 percent slopes	0.00	0.03	0.08	0.00						0.01	0.08				0.00	0.00	
Tripp	589.336	589.458	0.122	644	SD123	354395	HbA	Holt-Anselmo fine sandy loams, 0 to 3 percent slopes		0.08	0.11								0.00				0.00	0.00	
Tripp	589.458	589.554	0.096	506	SD123	354369	AID	Anselmo-Longpine fine sandy loams, 10 to 20 percent slopes	0.00	0.03	0.08	0.00						0.01	0.08				0.00	0.00	
Tripp	589.554	590.019	0.464	2,452	SD123	354409	MdB	Manter fine sandy loam, 3 to 9 percent slopes		0.02	0.44							0.00	0.01	0.08			0.00	0.46	0.00
Tripp	590.019	590.189	0.171	902	SD123	354369	AID	Anselmo-Longpine fine sandy loams, 10 to 20 percent slopes	0.01	0.05	0.14	0.01						0.00	0.02	0.13			0.00	0.14	0.00
Tripp	590.189	590.334	0.144	762	SD123	354409	MdB	Manter fine sandy loam, 3 to 9 percent slopes		0.01	0.14							0.00	0.00				0.00	0.14	0.00
Tripp	590.334	590.495	0.161	851	SD123	354462	WgB	Wewela fine sandy loam, 3 to 6 percent slopes		0.14	0.01		0.00	0.00	0.00	0.00	0.00	0.00	0.15				0.00	0.00	
Tripp	590.495	590.561	0.066	349	SD123	354410	MfE	Manter-Anselmo fine sandy loams, 15 to 30 percent slopes		0.01	0.18							0.01	0.06				0.00	0.00	
Tripp	590.561	590.756	0.195	1,031	SD123	354409	MdB	Manter fine sandy loam, 3 to 9 percent slopes		0.01	0.18							0.00	0.01	0.06			0.00	0.20	0.00
Tripp	590.756	590.867	0.110	582	SD123	354410	MfE	Manter-Anselmo fine sandy loams, 15 to 30 percent slopes		0.01	0.10	0.10						0.01	0.11				0.00	0.00	
Tripp	590.867	590.922	0.055	291	SD123	354458	Wb	Wann fine sandy loam		0.00	0.00			0.0											

Table 1: Soil Limitations Along the Pipeline Centerline Mileposted by Soil Map Unit (continued)

Tripp	592.799	592.839	0.040	213	SD123	354452	Trf	Longpine-Rock outcrop complex, 15 to 40 percent slopes	0.01	0.03	0.03	0.04						0.00	0.04	0.03				
Tripp	592.839	592.921	0.081	430	SD123	354374	BOD	Boyd-Oklaton association, 9 to 25 percent slopes		0.07	0.01	0.07	0.00					0.00	0.08	0.07		0.00		
Tripp	592.921	593.009	0.088	464	SD123	354452	Trf	Longpine-Rock outcrop complex, 15 to 40 percent slopes	0.03	0.07	0.06	0.08							0.00	0.08	0.07		0.00	
Tripp	593.009	593.113	0.104	550	SD123	354366	ABC	Anselmo fine sandy loam, 6 to 9 percent slopes		0.00	0.10								0.00	0.08		0.10	0.00	
Tripp	593.113	593.227	0.114	605	SD123	354410	MfE	Manter-Anselmo fine sandy loams, 15 to 30 percent slopes		0.01	0.10	0.11							0.01	0.08	0.11	0.01		0.00
Tripp	593.227	593.329	0.101	535	SD123	354366	ABC	Anselmo fine sandy loam, 6 to 9 percent slopes		0.00	0.10								0.00	0.08		0.10	0.00	
Tripp	593.329	593.451	0.123	648	SD123	354410	MfE	Manter-Anselmo fine sandy loams, 15 to 30 percent slopes		0.02	0.11	0.11							0.01	0.08	0.12	0.01		0.00
Tripp	593.451	593.490	0.039	206	SD123	354366	ABC	Anselmo fine sandy loam, 6 to 9 percent slopes		0.00	0.04								0.00	0.04		0.04	0.00	
Tripp	593.490	593.646	0.156	823	SD123	354410	MfE	Manter-Anselmo fine sandy loams, 15 to 30 percent slopes		0.02	0.14	0.14							0.02	0.05	0.15	0.01		0.00
Tripp	593.646	594.197	0.551	2,907	SD123	354369	AD	Anselmo-Longpine fine sandy loams, 10 to 20 percent slopes	0.02	0.17	0.48	0.02							0.03	0.05	0.43	0.13		0.00
Tripp	594.197	594.433	0.236	1,247	SD123	354410	MfE	Manter-Anselmo fine sandy loams, 15 to 30 percent slopes		0.03	0.21	0.22							0.03	0.05	0.23	0.02		0.00
Tripp	594.433	594.533	0.101	531	SD123	354433	RaB	Ree loam, 3 to 6 percent slopes		0.01			0.00	0.00					0.00	0.10		0.10	0.00	
Tripp	594.533	594.649	0.116	612	SD123	354408	MaA	Manter fine sandy loam, 0 to 3 percent slopes			0.11								0.00	0.10		0.01	0.12	0.00
Tripp	594.649	594.655	0.005	27	SD123	354433	RaB	Ree loam, 3 to 6 percent slopes		0.00			0.00	0.00					0.00	0.10		0.00	0.10	0.00
Tripp	594.655	594.679	0.024	127	SD123	354408	MaA	Manter fine sandy loam, 0 to 3 percent slopes			0.02								0.00	0.10		0.00	0.02	0.00
Tripp	594.679	594.715	0.037	155	SD123	354410	MfE	Manter-Anselmo fine sandy loams, 15 to 30 percent slopes		0.00	0.03	0.03							0.00	0.10		0.04	0.00	0.00
Tripp	594.715	595.143	0.428	2,258	SD123	354374	BOD	Boyd-Oklaton association, 9 to 25 percent slopes		0.36	0.03	0.38	0.00						0.00	0.40		0.39		0.00
Tripp	595.143	595.286	0.143	754	SD123	354410	MfE	Manter-Anselmo fine sandy loams, 15 to 30 percent slopes		0.02	0.13	0.13							0.02	0.14		0.14	0.01	0.00
Tripp	595.286	595.511	0.225	1,188	SD123	354374	BOD	Boyd-Oklaton association, 9 to 25 percent slopes		0.19	0.02	0.19	0.00						0.00	0.21		0.21		0.00
Tripp	595.511	595.588	0.078	409	SD123	354427	PvB	Promise clay, 3 to 6 percent slopes					0.08						0.08	0.08		0.08		0.00
Tripp	595.588	595.722	0.133	703	SD123	354376	Bt	Bridgeport complex, channeled			0.01			0.01					0.02	0.11		0.01		0.00
Tripp	595.722	595.860	0.138	730	SD123	354375	Bp	Bridgeport complex			0.00			0.02	0.00				0.04	0.14		0.14		0.00
Tripp	595.860	595.923	0.063	337	SD123	354427	PvB	Promise clay, 3 to 6 percent slopes					0.08						0.08	0.08		0.08		0.00
Tripp	595.923	596.079	0.156	822	SD123	354384	DdB	Dix soils, 9 to 18 percent slopes			0.15									0.15		0.14		0.00
Tripp	596.079	596.202	0.124	654	SD123	354370	AvA	Anselmo-Vetal fine sandy loams, 0 to 3 percent slopes		0.01	0.08		0.00	0.00	0.00	0.00	0.00	0.00		0.03		0.03	0.03	0.00
Tripp	596.202	596.232	0.029	155	SD123	354384	DdB	Dix soils, 9 to 18 percent slopes			0.03									0.03		0.03		0.00
Tripp	596.232	596.490	0.258	1,364	SD123	354370	AvA	Anselmo-Vetal fine sandy loams, 0 to 3 percent slopes		0.01	0.17		0.01	0.01	0.01	0.01	0.01	0.01		0.01		0.01		0.00
Tripp	596.490	596.610	0.120	634	SD123	354410	MfE	Manter-Anselmo fine sandy loams, 15 to 30 percent slopes		0.02	0.11	0.11							0.02	0.12		0.01		0.00
Tripp	596.610	596.645	0.035	186	SD123	354374	BOD	Boyd-Oklaton association, 9 to 25 percent slopes		0.03	0.00	0.03	0.00						0.00	0.03		0.03		0.00

Table 1: Soil Limitations Along the Pipeline Centerline Milepoeted by Soil Map Unit (continued)

Harding	CAR-090	1.810	1.826	0.016	83	SD063	355772	Pbe	Parolin-Bullock fine sandy loams, 2 to 9 percent slopes	0.02	0.01	0.00	0.00	0.01	0.01	0.01	0.00			
Harding	CAR-090	1.826	1.881	0.055	293	SD063	355723	BpB	Bullock-Parolin-Slickspots complex, 2 to 9 percent slopes	0.05	0.02			0.04	0.04	0.06	0.00			
Harding	CAR-090	1.881	1.953	0.071	376	SD063	355772	Pbe	Parolin-Bullock fine sandy loams, 2 to 9 percent slopes	0.07	0.04	0.00	0.00	0.06	0.06	0.07	0.01			
Harding	CAR-090	1.953	2.325	0.372	1,965	SD063	355723	BpB	Bullock-Parolin-Slickspots complex, 2 to 9 percent slopes	0.34	0.15			0.30	0.30	0.33	0.01			
Harding	CAR-090	2.325	2.482	0.157	830	SD063	355805	TyC	Twilight-Parolin fine sandy loams, 6 to 15 percent slopes	0.15	0.13	0.01	0.01	0.05	0.06	0.06	0.06			
Harding	CAR-090	2.482	2.486	0.004	22	SD063	355772	PbC	Parolin-Bullock fine sandy loams, 2 to 9 percent slopes	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00			
Perkins	CAR-066A	0.000	0.390	0.390	2,060	SD105	354607	AaB	Bullock-Parolin loams, 0 to 9 percent slopes	0.39	0.12			0.37	0.39	0.39	0.00			
Perkins	CAR-047	0.000	0.109	0.109	576	SD105	354666	TcD	Twilight-Marmarth-Parolin association, gently rolling	0.11	0.07	0.00	0.00	0.09	0.09	0.04	0.06			
Perkins	CAR-047	0.109	0.149	0.040	212	SD105	354615	BaB	Belfield-Marmarth complex, 0 to 8 percent slopes	0.02	0.00			0.03	0.03	0.04	0.03	0.04	0.00	
Perkins	CAR-047	0.149	0.496	0.347	1,831	SD105	354607	AaB	Bullock-Parolin loams, 0 to 9 percent slopes	0.35	0.10			0.33	0.33	0.36	0.04	0.00		
Perkins	CAR-047	0.496	0.857	0.400	2,114	SD105	354666	TcD	Twilight-Marmarth-Parolin association, gently rolling	0.40	0.26	0.02	0.01	0.11	0.13	0.23	0.12			
Perkins	CAR-047	0.857	1.277	0.380	2,006	SD105	354607	AaB	Bullock-Parolin loams, 0 to 9 percent slopes	0.36	0.11			0.36	0.36	0.38	0.00			
Perkins	CAR-047	1.277	1.386	0.110	579	SD105	354666	TcD	Twilight-Marmarth-Parolin association, gently rolling	0.11	0.07	0.00	0.00	0.03	0.04	0.06	0.03			
Perkins	CAR-047	1.386	1.421	0.035	185	SD105	354618	BhE	Blackhall-Cobbart complex, 15 to 40 percent slopes	0.03	0.00	0.03	0.01	0.00	0.02	0.02	0.03			
Perkins	CAR-047	1.421	1.511	0.090	475	SD105	354607	AaB	Bullock-Parolin loams, 0 to 9 percent slopes	0.09	0.03			0.09	0.09	0.09	0.00			
Perkins	CAR-047	1.511	1.649	0.138	730	SD105	354618	BhE	Blackhall-Cobbart complex, 15 to 40 percent slopes	0.13	0.01	0.11	0.01	0.01	0.07	0.06	0.12			
Perkins	CAR-047	1.649	1.973	0.323	1,707	SD105	354666	TcD	Twilight-Marmarth-Parolin association, gently rolling	0.32	0.21	0.01	0.01	0.09	0.11	0.19	0.10		0.00	
Perkins	CAR-047	1.973	2.104	0.131	694	SD105	354664	Ta	Trembles fine sandy loam	0.01			0.01						0.13	
Perkins	CAR-047	2.104	2.289	0.165	873	SD105	354663	Sh	Lohrer-Trembles complex	0.01			0.12		0.01				0.17	
Perkins	CAR-047	2.289	2.891	0.622	3,283	SD105	354618	BhE	Blackhall-Cobbart complex, 15 to 40 percent slopes	0.59	0.03	0.50	0.25	0.08	0.31	0.34	0.53	0.01	0.00	
Perkins	CAR-047	2.891	3.073	0.182	961	SD105	354608	AbC	Bullock-Slickspots complex, 0 to 15 percent slopes	0.18	0.01	0.01	0.01	0.15	0.16	0.17	0.02			
Perkins	CAR-047	3.073	3.221	0.148	780	SD105	354618	BhE	Blackhall-Cobbart complex, 15 to 40 percent slopes	0.14	0.01	0.12	0.06	0.01	0.07	0.06	0.13			
Perkins	CAR-048	0.000	0.042	0.042	223	SD105	354666	TcD	Twilight-Marmarth-Parolin association, gently rolling	0.04	0.03	0.00	0.00	0.01	0.01	0.02	0.01		0.00	
Perkins	CAR-048	0.042	0.341	0.299	524	SD105	354608	AbC	Bullock-Slickspots complex, 0 to 15 percent slopes	0.10	0.00	0.01	0.00	0.08	0.09	0.09	0.01			
Perkins	CAR-048	0.341	0.579	0.438	2,311	SD105	354607	AaB	Bullock-Parolin loams, 0 to 9 percent slopes	0.44	0.13			0.42	0.42	0.44				
Perkins	CAR-048	0.579	0.659	0.080	422	SD105	354608	AbC	Bullock-Slickspots complex, 0 to 15 percent slopes	0.08	0.00	0.01	0.00	0.07	0.07	0.07	0.01			
Perkins	CAR-048	0.659	0.711	0.052	276	SD105	354607	AaB	Bullock-Parolin loams, 0 to 9 percent slopes	0.05	0.02			0.05	0.05	0.05				
Perkins	CAR-048	0.711	1.090	0.379	1,999	SD105	354608	AbC	Bullock-Slickspots complex, 0 to 15 percent slopes	0.38	0.01	0.03	0.02	0.32	0.34	0.35	0.06			
Perkins	CAR-048	1.090	1.313	0.223	1,176	SD105	354607	AaB	Bullock-Parolin loams, 0 to 9 percent slopes	0.22	0.07			0.21	0.21	0.22				
Perkins	CAR-048	1.313	1.360	0.047	249	SD105	354608	AbC	Bullock-Slickspots complex, 0 to 15 percent slopes	0.05	0.00	0.00	0.00	0.04	0.04	0.04	0.01			
Perkins	CAR-048	1.360	1.661	0.301	1,588	SD105	354607	AaB	Bullock-Parolin loams, 0 to 9 percent slopes	0.30	0.09			0.29	0.30	0.30				
Perkins	CAR-048	1.661	2.215	0.554	2,926	SD105	354608	AbC	Bullock-Slickspots complex, 0 to 15 percent slopes	0.55	0.02	0.04	0.02	0.47	0.48	0.52	0.07			
Perkins	CAR-048	2.215	2.269	0.054	284	SD105	354607	AaB	Bullock-Parolin loams, 0 to 9 percent slopes	0.05	0.02			0.05	0.05	0.05				
Perkins	CAR-048	2.269	2.339	0.071	372	SD105	354608	AbC	Bullock-Slickspots complex, 0 to 15 percent slopes	0.07	0.00	0.01	0.00	0.06	0.06	0.07	0.01			
Perkins	CAR-048	2.339	2.661	0.322	1,702	SD105	354607	AaB	Bullock-Parolin loams, 0 to 9 percent slopes	0.32	0.10			0.31	0.31	0.32				
Perkins	CAR-048	2.661	2.740	0.079	415	SD105	354608	AbC	Bullock-Slickspots complex, 0 to 15 percent slopes	0.08	0.00	0.01	0.00	0.07	0.07	0.07	0.01			
Perkins	CAR-049A	0.000	0.144	0.144	761	SD105	354666	TcD	Twilight-Marmarth-Parolin association, gently rolling	0.14	0.09	0.01	0.00	0.04	0.05	0.08	0.04		0.00	
Perkins	CAR-049A	0.144	0.328	0.183	968	SD105	354607	AaB	Bullock-Parolin loams, 0 to 9 percent slopes	0.18	0.06			0.17	0.17	0.18				
Perkins	CAR-049A	0.328	0.361	0.034	179	SD105	354666	TcD	Twilight-Marmarth-Parolin association, gently rolling	0.03	0.02	0.00	0.00	0.01	0.01	0.02	0.01		0.00	
Perkins	CAR-049A	0.361	0.465	0.103	546	SD105	354607	AaB	Bullock-Parolin loams, 0 to 9 percent slopes	0.10	0.03			0.10	0.10	0.10				
Meade	CAR-077	0.179	0.071	0.893	4,714	SD601	355439	Ge	Gienberg fine sandy loam	0.07			0.06	0.06	0.07	0.06	0.07	0.89		
Meade	CAR-077	1.071	1.235	0.164	864	SD601	355451	Ld	Lohmiller silty clay loam	0.00			0.16	0.00	0.15	0.15	0.00		0.16	
Meade	CAR-077	1.235	1.374	0.139	734	SD601	355446	KyB	Kyle clay, 2 to 6 percent slopes	0.01			0.01	0.13	0.14	0.14	0.01		0.00	
Meade	CAR-078	0.000	0.041	0.041	219	SD601	355446	KyB	Kyle clay, 2 to 6 percent slopes	0.00			0.00	0.04	0.04	0.04	0.00		0.00	
Meade	CAR-078	0.041	0.167	0.125	662	SD601	355451	Ld	Lohmiller silty clay loam	0.00			0.11	0.00	0.12	0.12	0.00		0.13	
Meade	CAR-078	0.167	0.375	0.208	1,097	SD601	355452	Lg	Lohmiller silty clay loam, channelled	0.00			0.21	0.00	0.21	0.21	0.00		0.00	
Meade	CAR-078	0.375	0.452	0.077	408	SD601	355457	PeB	Pierre clay, 2 to 6 percent slopes	0.08			0.00	0.00	0.01	0.06	0.00		0.00	
Meade	CAR-078	0.452	0.579	0.127	670	SD601	355452	Lg	Lohmiller silty clay loam, channelled	0.00			0.13	0.00	0.13	0.13	0.00		0.00	
Meade	CAR-078	0.579	0.648	0.069	365	SD601	355445	KyA	Kyle clay, 0 to 2 percent slopes	0.00			0.01	0.06	0.07	0.07	0.00		0.00	
Meade	CAR-078	0.648	0.718	0.070	370	SD601	355452	Lg	Lohmiller silty clay loam, channelled	0.00			0.07	0.07	0.07	0.07	0.00		0.00	
Meade	CAR-078	0.718	1.382	0.664	3,505	SD601	355445	KyA	Kyle clay, 0 to 2 percent slopes	0.00			0.07	0.60	0.60	0.60	0.01		0.01	
Meade	CAR-078	1.382	1.575	0.193	1,018	SD601	355452	Lg	Lohmiller silty clay loam, channelled	0.00			0.18	0.00	0.18	0.18	0.00		0.00	
Meade	CAR-078	1.575	1.825	0.250	1,322	SD601	355451	Ld	Lohmiller silty clay loam	0.01			0.23	0.01	0.24	0.24	0.01		0.25	
Meade	CAR-078	1.825	2.004	0.180	948	SD601	355452	Lg	Lohmiller silty clay loam, channelled	0.00			0.18	0.00	0.18	0.18	0.00		0.00	
Meade	CAR-078	2.004	2.071	0.067	353	SD601	355446	KyB	Kyle clay, 2 to 6 percent slopes	0.00			0.01	0.06	0.07	0.07	0.00		0.00	
Meade	CAR-078	2.071	2.601	0.530	2,796	SD601	355452	Lg	Lohmiller silty clay loam, channelled	0.00			0.53	0.00	0.53	0.53	0.00		0.01	
Meade	CAR-078	2.601	2.694	0.092	488	SD601	355462	SnD	Samuel clay, 6 to 25 percent slopes	0.00		0.08	0.00	0.00	0.00	0.09	0.09	0.00		0.00
Haakon	CAR-052A	0.000	0.061	0.061	323	SD055	354131	OvA	Ottumwa silty clay, 0 to 3 percent slopes	0.00			0.00	0.00	0.00	0.06	0.00		0.06	
Haakon	CAR-052A	0.061	0.260	0.199	1,049	SD055	354101	KmB	Kirley-Ottumwa complex, 2 to 6 percent slopes	0.02			0.02	0.02	0.02	0.20	0.20		0.20	
Haakon	CAR-052A	0.260	0.745	0.486	2,564	SD055	354110	LbE	Lakoma-Vivian complex, 9 to 25 percent slopes	0.42	0.03	0.18		0.24	0.24	0.24	0.15		0.15	
Haakon	CAR-052A	0.745	0.780	0.034	180	SD055	354095	KeB												

Table 1: Soil Limitations Along the Pipeline Centerline Mileposted by Soil Map Unit (continued)

Lyman	CAR-08G	0.500	0.581	0.081	430	SO085	355578	LbO	Lakoma-Okaton silty clays, 6 to 15 percent slopes	0.07			0.01			0.01	0.08		0.08			0.00
Lyman	CAR-08D	0.581	0.640	0.058	308	SO085	355607	pg	7Hs, gravel		0.08	0.08	0.00			0.00	0.00		0.06	0.06		0.00
Lyman	CAR-08D	0.640	1.032	0.393	2,075	SO085	355619	SbE	Sansarc-Opal clays, 9 to 40 percent slopes	0.38			0.37	0.18		0.01	0.18	0.18	0.38	0.38		0.00
Lyman	CAR-08D	1.032	1.243	0.210	1,108	SO085	355562	BuA	Bullcreek clay, 0 to 6 percent slopes	0.01				0.20	0.19		0.20	0.21				0.00
Lyman	CAR-08D	1.243	1.288	0.045	241	SO085	355518	SbE	Sansarc-Opal clays, 9 to 40 percent slopes	0.04		0.04	0.02		0.00		0.02	0.04		0.04	0.00	0.00
Lyman	CAR-08D	1.288	1.402	0.114	609	SO085	355563	BuA	Bullcreek clay, 0 to 6 percent slopes	0.01				0.11	0.10		0.11	0.11				0.00
Lyman	CAR-08D	1.402	1.479	0.077	404	SO085	355608	PaA	Promise clay, 0 to 3 percent slopes	0.00			0.07	0.00			0.08	0.08				0.00
Lyman	CAR-08D	1.479	1.504	0.025	133	SO085	355595	Mr	Munroe fine sandy loam		0.02		0.00			0.00	0.00	0.00				0.00
Lyman	CAR-08D	1.504	1.658	0.154	814	SO085	355570	Hm	Hilmoe silty clay		0.01		0.14				0.14	0.15				0.00
Tripp	CAR-081	0.000	0.330	0.330	1,741	SD123	354431	RaA	Ree loam, 0 to 3 percent slopes				0.01	0.01	0.01		0.01	0.33				0.00
Tripp	CAR-081	0.330	0.399	0.070	367	SD123	354459	WeE	Westover loam, 9 to 25 percent slopes	0.00	0.07	0.07	0.00			0.00	0.01		0.07	0.07		0.00
Tripp	CAR-081	0.399	1.138	0.738	3,898	SD123	354419	ObE	Okaton-Lakoma association, 15 to 40 percent slopes	0.66	0.01	0.66	0.03			0.03	0.72		0.73	0.01		0.01
Tripp	CAR-081	1.138	1.443	0.306	1,614	SD123	354445	SAE	Sansarc-Opal association, 15 to 40 percent slopes	0.28	0.02	0.29	0.01			0.01	0.26		0.30	0.02		0.00
Tripp	CAR-081	1.443	1.692	0.249	1,313	SD123	354450	Sw	Bullcreek clay				0.25	0.22			0.25	0.26				0.00
Tripp	CAR-081	1.692	2.004	0.312	1,650	SD123	354445	SAE	Sansarc-Opal association, 15 to 40 percent slopes	0.28	0.02	0.30	0.01			0.01	0.29		0.30	0.02		0.00
Tripp	CAR-081	2.004	2.099	0.095	499	SD123	354419	ObE	Okaton-Lakoma association, 15 to 40 percent slopes	0.09	0.00	0.09	0.00			0.00	0.09		0.09	0.00		0.00
Tripp	CAR-081	2.099	2.141	0.043	225	SD123	354459	WeE	Westover loam, 9 to 25 percent slopes	0.00	0.04	0.04	0.00			0.00	0.00		0.04	0.04		0.00
Tripp	CAR-082	0.000	0.045	0.045	237	SD123	354432	RaA	Ree loam, 0 to 3 percent slopes				0.00	0.00	0.00		0.00	0.04				0.00
Tripp	CAR-082	0.045	0.176	0.131	693	SD123	354459	WeE	Westover loam, 9 to 25 percent slopes	0.01	0.12	0.13	0.00			0.00	0.01		0.13	0.12		0.00
Tripp	CAR-082	0.176	0.233	0.057	303	SD123	354432	RaA	Ree loam, 0 to 3 percent slopes				0.00	0.00	0.00		0.00	0.06				0.00
Tripp	CAR-091	0.000	0.256	0.256	1,352	SD123	354434	RaC	Ree loam, 6 to 9 percent slopes	0.01	0.01	0.01	0.00			0.01	0.28		0.29	0.01	0.26	0.01
Tripp	CAR-091	0.256	0.579	0.323	1,703	SD123	354406	LoD	Lakoma-Okaton silty clays, 9 to 15 percent slopes	0.27	0.01	0.02	0.02			0.02	0.31		0.31	0.01		0.00
Tripp	CAR-091	0.579	0.845	0.266	1,405	SD123	354433	RaB	Ree loam, 3 to 6 percent slopes	0.02			0.01	0.01			0.01		0.01			0.00
Tripp	CAR-091	0.845	0.923	0.078	411	SD123	354406	LoD	Lakoma-Okaton silty clays, 9 to 15 percent slopes	0.07	0.00	0.00				0.00	0.07		0.07	0.00		0.00

Table 1: Soil Limitations Along the Pipeline Centerline Mileposted by Soil Map Unit (continued)

Keystone XL Steele City Segment
South Dakota Soils Summary
Prepared: 2009-08-14

Centerline Summary

County	Length (mi)	Shallow Bedrock (mi)	Percent of County	All Shallow Rooted Layers (mi)	Percent of County	Drought Prone (mi)	Percent of County	Shoaly Sloping (mi)	Percent of County	Saline (mi)	Percent of County	Sodic (mi)	Percent of County	Saline-Sodic (mi)	Percent of County	Low or High pH (mi)	Percent of County	Low Regeneration Potential (mi)	Percent of County	Compaction Prone (mi)	Percent of County	Severe Wind Eroddle (mi)	Percent of County	Severe Water Eroddle (mi)	Percent of County	Stony or Ruddy (mi)	Percent of County	Prime Farmland (mi)	Percent of County	Hydric (mi)	Percent of County
Harding	72.38	0.96	1.3%	58.19	80.5%	24.15	33.4%	8.4	11.5%	1.73	2.4%	2.77	3.8%	31.17	43.1%	0.0%	0.0%	36.54	50.5%	44.87	62.0%	3.94	5.3%	20.81	28.8%	1.88	2.6%	4.26	5.9%	0.52	0.7%
Perkins	15.24	0.0%	0.0%	13.61	89.3%	4.10	26.9%	1.27	8.3%	1.54	10.1%	0.52	3.4%	8.68	57.0%	0.0%	0.0%	10.46	68.6%	11.99	78.6%	0.15	1.0%	2.99	19.6%	0.39	2.5%	1.61	10.5%	0.00	0.0%
Meade	52.72	0.0%	0.0%	31.82	60.4%	4.00	7.6%	6.83	13.0%	20.33	38.6%	1.12	2.1%	12.52	23.8%	0.0%	0.0%	32.93	62.5%	48.56	92.1%	0.21	0.4%	19.62	37.2%	0.83	1.6%	20.74	39.3%	0.14	0.3%
Pennington	0.38	0.0%	0.0%	0.0%	0.0%	0.28	72.7%	0.0%	0.0%	0.06	14.8%	0.00	0.0%	0.01	1.4%	0.00	0.0%	0.06	15.5%	0.06	15.5%	0.28	71.7%	0.0%	0.0%	0.03	7.0%	0.06	15.5%	0.28	71.7%
Haakon	58.94	0.0%	0.0%	22.28	37.8%	4.06	6.9%	5.49	9.3%	4.30	7.3%	0.08	0.1%	4.23	7.2%	0.08	0.1%	6.77	11.5%	57.54	97.6%	0.0%	0.0%	19.93	33.8%	1.95	3.3%	31.36	53.2%	1.58	2.7%
Jensen	60.09	0.0%	0.0%	23.41	38.9%	0.0%	0.0%	1.90	3.2%	4.7%	7.8%	0.0%	0.0%	3.33	5.5%	0.0%	0.0%	20.40	33.9%	39.13	65.2%	0.0%	0.0%	20.87	34.8%	0.89	1.5%	14.47	24.1%	1.19	2.0%
Lynn	11.90	0.0%	0.0%	2.46	20.7%	0.0%	0.0%	1.42	11.9%	8.95	75.2%	0.0%	0.0%	0.83	7.0%	0.0%	0.0%	8.48	71.1%	11.77	98.9%	0.00	0.0%	3.15	27.3%	0.05	0.4%	7.83	65.8%	0.15	1.2%
Tripp	58.73	0.21	0.4%	14.53	24.8%	30.69	52.1%	7.72	13.2%	16.32	27.8%	0.83	1.4%	3.52	5.9%	0.98	1.6%	17.53	29.8%	36.53	62.2%	9.83	16.5%	19.27	32.8%	2.46	4.2%	25.81	43.7%	0.94	1.6%
Grand Total	314.13	1.17	0.4%	167.85	53.4%	63.88	20.3%	34.81	11.1%	74.18	23.6%	5.37	1.7%	65.97	21.0%	1.06	0.3%	135.75	43.2%	252.14	80.3%	15.60	5.0%	107.79	34.3%	9.34	2.9%	106.13	33.8%	5.17	1.6%

Access Road Summary

County	Length (mi)	Shallow Bedrock (mi)	Percent of County	All Shallow Rooted Layers (mi)	Percent of County	Drought Prone (mi)	Percent of County	Shoaly Sloping (mi)	Percent of County	Saline (mi)	Percent of County	Sodic (mi)	Percent of County	Saline-Sodic (mi)	Percent of County	Low or High pH (mi)	Percent of County	Low Regeneration Potential (mi)	Percent of County	Compaction Prone (mi)	Percent of County	Severe Wind Eroddle (mi)	Percent of County	Severe Water Eroddle (mi)	Percent of County	Stony or Ruddy (mi)	Percent of County	Prime Farmland (mi)	Percent of County	Hydric (mi)	Percent of County
Harding	10.64	0.26	2.4%	8.50	82.2%	4.15	38.7%	1.54	14.2%	0.44	4.0%	0.41	3.8%	5.73	52.9%	0.0%	0.0%	6.58	60.7%	8.10	74.7%	0.22	2.1%	2.96	27.3%	0.54	5.0%	0.58	5.4%	0.08	0.7%
Perkins	6.82	0.0%	0.0%	6.44	94.5%	1.73	25.4%	0.92	13.5%	0.16	2.3%	0.46	6.7%	4.45	65.3%	0.0%	0.0%	5.07	74.4%	5.82	82.4%	0.01	0.2%	1.34	19.7%	0.03	0.4%	0.34	4.9%	0.01	0.2%
Meade	1.89	0.0%	0.0%	0.17	4.5%	0.09	2.3%	0.08	2.1%	2.05	52.6%	0.0%	0.0%	0.91	23.3%	0.0%	0.0%	2.95	73.9%	3.02	77.7%	0.09	2.3%	0.10	2.6%	0.00	0.1%	1.43	34.8%	0.03	0.7%
Haakon	1.70	0.0%	0.0%	0.85	50.0%	0.18	10.7%	0.73	43.0%	0.36	21.4%	0.00	0.0%	0.05	3.0%	0.00	0.0%	0.37	21.8%	1.39	81.7%	0.0%	0.0%	1.04	61.5%	0.32	18.7%	0.84	38.0%	0.02	1.5%
Lynn	1.46	0.0%	0.0%	0.83	56.9%	0.09	5.7%	0.80	54.8%	0.99	68.5%	0.0%	0.0%	0.32	21.7%	0.0%	0.0%	1.02	69.2%	1.55	95.7%	0.00	0.1%	0.89	52.9%	0.08	4.6%	0.43	25.9%	0.02	1.7%
Tripp	1.30	0.0%	0.0%	1.68	112.0%	0.31	8.5%	1.58	121.5%	0.36	27.7%	0.0%	0.0%	0.28	21.7%	0.0%	0.0%	0.38	29.2%	3.00	231.0%	0.0%	0.1%	2.18	167.3%	0.11	8.5%	0.35	26.9%	0.07	2.0%
Grand Total	28.20	0.28	0.9%	18.88	67.0%	6.56	23.4%	5.45	19.3%	4.95	17.4%	0.87	3.1%	11.71	41.5%	0.00	0.0%	16.33	57.9%	32.68	80.4%	0.33	1.2%	8.61	30.3%	1.36	4.8%	4.38	15.5%	0.28	0.9%

Facilities Summary

Type	County	Milepost	Shallow Bedrock (mi)	Percent of County	All Shallow Rooted Layers (mi)	Percent of County	Drought Prone (mi)	Percent of County	Shoaly Sloping (mi)	Percent of County	Saline (mi)	Percent of County	Sodic (mi)	Percent of County	Saline-Sodic (mi)	Percent of County	Low or High pH (mi)	Percent of County	Low Regeneration Potential (mi)	Percent of County	Compaction Prone (mi)	Percent of County	Severe Wind Eroddle (mi)	Percent of County	Severe Water Eroddle (mi)	Percent of County	Stony or Ruddy (mi)	Percent of County	Prime Farmland (mi)	Percent of County	Hydric (mi)	Percent of County
CC	Adair	80.04	0.0%	0.0%	2.70	3.4%	0.53	0.7%	0.0%	0.0%	69.51	86.6%	0.0%	0.0%	5.54	6.9%	0.0%	0.0%	70.25	86.6%	79.49	99.3%	0.0%	0.0%	7.54	9.5%	0.55	0.7%	82.04	100.0%	1.05	1.3%
	Total	80.04	0.0%	0.0%	2.70	3.4%	0.53	0.7%	0.0%	0.0%	69.51	86.6%	0.0%	0.0%	5.54	6.9%	0.0%	0.0%	70.25	86.6%	79.49	99.3%	0.0%	0.0%	7.54	9.5%	0.55	0.7%	82.04	100.0%	1.05	1.3%
	Harding	30.10	0.0%	0.0%	28.57	94.9%	8.94	29.7%	0.41	1.3%	6.41	21.3%	0.41	1.3%	24.80	82.4%	0.0%	0.0%	25.21	83.8%	27.29	91.7%	0.51	1.7%	12.40	41.2%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%
CY	Haakon	30.35	0.0%	0.0%	27.41	90.3%	5.47	18.0%	1.87	6.2%	0.13	0.4%	2.06	6.8%	19.73	65.0%	2.81	9.3%	21.53	72.3%	23.28	76.7%	0.0%	0.0%	4.40	14.5%	0.47	1.5%	0.0%	0.0%	0.13	0.4%
	Total	30.35	0.0%	0.0%	27.41	90.3%	5.47	18.0%	1.87	6.2%	0.13	0.4%	2.06	6.8%	19.73	65.0%	2.81	9.3%	21.53	72.3%	23.28	76.7%	0.0%	0.0%	4.40	14.5%	0.47	1.5%	0.0%	0.0%	0.13	0.4%
	Perkins	0.08	0.0%	0.0%	0.03	100.0%	0.01	30.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%
MLV	Meade	0.88	0.0%	0.0%	0.02	20.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%
	Haakon	0.06	0.0%	0.0%	0.03	48.0%	0.0%	47.5%	0.0%	1.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%
	Total	0.94	0.0%	0.0%	0.05	48.0%	0.0%	47.5%	0.0%	1.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%
PS	Tripp	12.80	0.0%	0.0%	11.85	92.6%	14.45	113.6%	4.87	37.9%	7.14	55.7%	2.50	19.5%	44.84	345.5%	2.84	21.4%	48.03	373.0%	74.15	578.6%	0.52	4.1%	39.83	308.6%	7.11	55.2%	0.78	6.1%	0.78	6.1%
	Meade	5.83	0.0%	0.0%	1.28	21.9%	0.0%	0.0%	0.0%	0.0%	3.23	55.4%	0.0%	0.0%	1.34	22.8%	0.0%	0.0%	3.87	66.6%	5.01	86.3%	0.0%	0.0%	0.28	4.8%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%
	Haakon	4.99	0.0%	0.0%	1.50	30.0%	0.0%	0.0%	0.0%	0.0%	0.10	2.0%	0.0%	0.0%	0.20	4.0%	0.0%	0.0%	0.20	4.0%	4.99	100.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%
PF	Tripp	35.33	0.0%	0.0%	1.85	5.2%	4.89	13.8%	0.88	2.5%	3.47	9.8%	0.0%	0.0%	0.07	0.2%	0.0%	0.0%	3.74	10.6%	8.04	22.8%	0.0%	0.0%	7.08	19.8%	0.28	0.8%	5.05	13.5%	0.26	0.7%
	Meade	57.79	0.0%	0.0%	73.55	127.3%	28.21	48.8%	10.57	18.3%	1.70	2.9%	2.20	3.8%	24.56	42.5%	0.0%	0.0%	28.46	49.3%	40.37	69.9%	3.49	6.0%	23.93	41.5%	0.31	0.5%	28.99	48.4%	0.26	0.4%
	Haakon	60.49	0.0%	0.0%	2.27	3.7%	0.0%	0.0%	0.0%	0.0%	0.72	1.2%	0.0%	0.0%	7.54	12.5%	0.0%	0.0%	7.57	12.5%	60.49	100.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%
SA	Tripp	264.17	0.29	0.1%	85.63	32.4%	36.42	13.8%	16.97	6.4%	78.14	29.3%	2.38	0.9%	46.79	17.3%	0.0%	0.0%	114.13	43.2%	188.79	70.3%	31.20	11.8%	55.29	20.9%	27.73	10.5%	28.22	10.7%	48.78	18.1%
	Meade	5.03	0.0%	0.0%	4.84	97.2%	2.44	48.7%	0.14	2.8%	0.0%	0.0%	0.14	2.8%	4.08	81.4%	0.0%	0.0%	4.22	84.3%	4.58	91.5%	0.0%	0.0%	0.57	11.3%	0.0%	0.0%	0.0%	0.0%		
	Haakon	4.09	0.0%	0.0%	1.49	36.4%	0.0%	0.0%	0.0%	0.0%	1.34	32.7%	0.0%	0.0%	3.33	81.2%	0.0%	0.0%	4.55	111.5%	4.90	120.0%	0.0%	0.0%	1.14	27.7%	0.0%	0.0%	1.14	27.7%	0.0%	0.0%
Grand Total	449.43	0.29	0.1%	150.12	33.4%	68.13	15.1%	16.94	3.8%	142.83	31.8%	5.38	1.2%	115.59	25.7%	2.07	0.5%	364.21	81.0%</													

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Data Request:

Provide definitions of the soil limitations discussed in the application. The definitions should identify the soil properties and ranges in properties used to place soils within a certain limitation category (e.g., slight, moderate, and severe limitations due to slope, ranges in electrical conductivity for salinity, and Sodium Adsorption Ratio for sodicity).

Response:

The soil assessment for the proposed project is based on SSURGO database review and analyses. As noted in DR 3-23, a table generated from GIS for the updated centerline (2/15/09) provided soil limitation information. The following soil limitation categories provided in the application are:

Severe Wind Erodible Soils - Includes all soils in WEG of 1, 2, 3.

Severe Water Erodible Soils - Slopes >8% with a Kw>0.24 and all slope greater than 15%

Low Reclamation Potential Soils - pH less than 3.5 (very acidic) greater than 8.5 (very alkaline)

Criteria	Saline	Sodic	Saline-Sodic
EC (mmhos/cm)	> 4	< 4	> 4
SAR	< 13	> 13	> 13

Prime Farmland - Includes land listed by the NRCS (2007) as potential prime farmland if adequate protection from flooding and adequate drainage are provided.

Hydric Soils - As designated by the NRCS (yes/no)

Compaction Prone Soils- Includes soils that have clay loam or finer textures

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Stony/Rocky Soils - Includes soils that have either: 1) a cobbly, stony, bouldery, gravelly, channery, flaggy, or shaly modifier to the textural class, or 2) have >five percent (weight basis) of stones larger than three inches in the surface layer.

Shallow Bedrock - Includes soils that have lithic bedrock within 60 inches of the soil surface.

Droughty Soils - Includes coarse-textured soils (sandy loams and coarser) that are well drained or excessively drained.

These interpretations were based on data available within the SSURGO database. SSURGO data were downloaded for each county crossed and run in GIS for the proposed project locations. Soil characteristics, identified above, for each soil component within a map unit were then identified within the Access database. The Soil Data Viewer extension for SSURGO only allows limited analysis and can get as specific as the Access data base (not able to pull out information on minor components), and therefore was not used for this in-depth analysis.