Exhibit C

BURNS McDONNELL

Sound Study

Prevailing Wind Park

Prevailing Wind Park, LLC

Prevailing Wind Park
Project No. 105644

Revision 7b
3/29/2019

Exhibit C

Sound Study

prepared for

Prevailing Wind Park, LLC

Prevailing Wind Park
Bon Homme/Charles Mix/Hutchinson Counties, SD

Project No. 105644

Revision 7b
3/29/2019

prepared by

Burns & McDonnell Engineering Company, Inc.

Kansas City, Missouri

TABLE OF CONTENTS

Page No.

LIST OF TABLES

Page No.

LIST OF FIGURES

Page No.

LIST OF ABBREVIATIONS

<u>Abbreviation</u>	<u>Term/Phrase/Name</u>
ANSI	American National Standards Institute
Burns & McDonnell	Burns & McDonnell Engineering Company, Inc.
CadnaA	Computer Aided Design for Noise Abatement
dB	Decibel
dBA	A-weighted decibels
DEM	Digital Elevation Model
Developer	Prevailing Wind Park, LLC
GE	General Electric
Hz	Hertz
ISO	International Organization for Standardization
L_{10}	10-percent exceedance sound level
L_{90}	90-percent exceedance sound level
L_{eq}	equivalent-continuous sound level
LWES	Large Wind Energy System
L_x	exceedance sound level
MP	measurement point
Project	Prevailing Wind Park
SDPUC	South Dakota Public Utility Commission
The Act	The Noise Control Act of 1972
USDA	U.S. Department of Agriculture
USGS	U.S. Geological Survey

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REVISION HISTORY

Rev	Issue Date	Release Notes
0	03-Apr-2018	Original release
1	09-Apr-2018	Revised wind turbine layout, incorporated client comments
2	11-Apr-2018	Added REC-138
3	16-Apr-2018	Revised wind turbine layout
4	27-Apr-2018	Revised wind turbine layout
5	14-May-2018	Incorporated client comments
6	10-Oct-2018	Revised layout, added new receptors, updated hub height, removed Vestas turbine option
7	15-Mar-2019	Revised wind turbine layout
7a	19-Mar-2019	Incorporated client comments

1.0 EXECUTIVE SUMMARY

Prevailing Wind Park, LLC (Developer) is proposing to construct the Prevailing Wind Park near Avon, South Dakota, in Bon Homme, Hutchinson, and Charles Mix Counties (Project). The Project will consist of 61 wind turbines with a maximum nameplate capacity of up to 219.6 megawatts (MW), although output at the point of interconnection will be limited to a maximum of 200 MW. For the purposes of this study, a total of 62 wind turbine sites were analyzed for the General Electric (GE) 3.8-137 turbine model. However, only up to 61 wind turbine sites will be installed. This sound assessment was completed to determine if the Project can operate in compliance with the applicable sound regulations.

Burns & McDonnell Engineering Company, Inc. (Burns & McDonnell) conducted an ambient sound survey and sound modeling study for the proposed Project. There were several objectives in this study, which included:

- Identification of any applicable county, city, state, or federal noise ordinances and other applicable sound guidelines;
- Measure ambient sound levels at noise-sensitive receivers;
- Estimation of the operational sound levels from the hypothetical Project layout using the three-dimensional sound modeling program Computer Aided Noise Abatement (CadnaA); and
- Determination if the wind farm can operate in compliance with the identified applicable regulatory standards.

There are no federal or state noise regulations that apply to this Project. Therefore, only local regulations or specific public utility commission limits would apply. Bon Homme County has adopted a zoning ordinance that pertains to large wind energy systems (LWES), which limits LWES to 45 dBA, average A-weighted sound pressure at the perimeter of occupied residences existing at the time the permit application is filed." Charles Mix County and Hutchinson County do not provide numeric noise ordinance limits applicable to the Project. In addition to the identified Bon Homme County ordinance, the South Dakota Public Utility Commission ("SDPUC") requires the Project limit noise at any non-participating residence to 40 dBA and 45 dBA at any participating residence. Therefore, the design criteria for the Project is 40 dBA at non-participating residences and 45 dBA at participating residences.

The wind turbines were modeled using manufacturer-specified sound power levels. Sound pressure levels were predicted at all identified receivers within and surrounding the Project area. There are no expected exceedances of the identified SDPUC limits due to operation of any of the proposed wind turbine locations of the Project.

2.0 ACOUSTICAL TERMINOLOGY

The term “sound level” is often used to describe two different sound characteristics: sound power and sound pressure. Every source that produces sound has a sound power level. The sound power level is the acoustical energy emitted by a sound source and is an absolute number that is not affected by the surrounding environment. The acoustical energy produced by a source propagates through media as pressure fluctuations. These pressure fluctuations, also called sound pressure, are what human ears hear and microphones measure.

Sound is physically characterized by amplitude and frequency. The amplitude of sound is measured in decibels (dB) as the logarithmic ratio of a sound pressure to a reference sound pressure (20 microPascals). The reference sound pressure corresponds to the typical threshold of human hearing. To the average listener, a 3-dB change in a continuous broadband sound is generally considered “just barely perceptible”; a 5-dB change is generally considered “clearly noticeable”; and a 10-dB change is generally considered a doubling (or halving, if the sound is decreasing) of the apparent loudness.

Sound waves can occur at many different wavelengths, also known as the frequency. Frequency is measured in hertz (Hz) and is the number of wave cycles per second that occur. The typical human ear can hear frequencies ranging from approximately 20 to 20,000 Hz. Normally, the human ear is most sensitive to sounds in the middle frequencies (1,000 to 8,000 Hz) and is less sensitive to sounds in the lower and higher frequencies. As such, the A-weighting scale was developed to simulate the frequency response of the human ear to sounds at typical environmental levels. The A-weighting scale emphasizes sounds in the middle frequencies and de-emphasizes sounds in the low and high frequencies. Any sound level to which the A-weighting scale has been applied is expressed in A-weighted decibels, or dBA. For reference, the A-weighted sound pressure level and subjective loudness associated with some common sound sources are listed in Table 2-1.

Table 2-1: Typical Sound Pressure Levels Associated with Common Noise Sources

Sound Pressure Level (dBA)[a]	Subjective Evaluation	Environment	
		Outdoor	Indoor
140	Deafening	Jet aircraft at 75 feet	--
130	Threshold of pain	Jet aircraft during takeoff at a distance of 300 feet	--
120	Threshold of feeling	Elevated train	Hard rock band
110		Jet flyover at 1,000 feet	Inside propeller plane
100	Very loud	Power mower, motorcycle at 25 feet, auto horn at 10 feet, crowd noise at football game	--
90	--	Propeller plane flyover at 1,000 feet, noisy urban street	Full symphony or band, food blender, noisy factory
80	Moderately loud	Diesel truck (40 mph)[a] at 50 feet	Inside auto at high speed, garbage disposal
70	Loud	B-757 cabin during flight	Close conversation, vacuum cleaner
60	Moderate	Air-conditioner condenser at 15 feet, near highway traffic	General office
50	Quiet	--	Private office
40	--	Farm field with light breeze, birdcalls	Soft stereo music in residence
30	Very quiet	Quiet residential neighborhood	Bedroom, average residence (without TV and stereo)
20	--	Rustling leaves	Quiet theater, whisper
10	Just audible	--	Human breathing
0	Threshold of hearing	--	--

Source: Adapted from *Architectural Acoustics*, M. David Egan, 1988 and *Architectural Graphic Standards*, Ramsey and Sleeper, 1994.
(a) dBA = A-weighted decibels; mph = miles per hour

Sound metrics have been developed to quantify fluctuating environmental sound levels. These metrics include the exceedance sound level. The exceedance sound level, L_x, is the sound level exceeded during "x" percent of the sampling period and is also referred to as a statistical sound level. L_{90} and L_{10} levels are exceedance sound levels referenced throughout this study. The L_{90} is a common L_x value and is regarded as the most accurate tool for measuring relatively constant background noise and for minimizing the influence of isolated spikes in sound levels (i.e., barking dog, door slamming). The L_{10} metric is the sound level exceeded for 10 percent of the measurement period and represents the top 10 percent of sound levels measured during a given measurement period.

3.0 REGULATIONS

Federal, state, and county regulations were reviewed to determine the applicable overall sound level limits for the Project.

The Noise Control Act of 1972 (the Act) (U.S.C. 4901) mandated a national policy "to promote an environment for all Americans free from noise that jeopardizes their health or welfare, to establish a means for effective coordination of Federal research activities in noise control, to authorize the establishment of Federal noise emission standards for products distributed in commerce, and to provide information to the public respecting the noise emission and noise reduction characteristics of such products."

As required by the Act, the EPA established criteria for protecting the public health and wellbeing. However, these criteria do not constitute enforceable federal regulations or standards. The EPA has since delegated regulatory authority to local entities. Therefore, there are no federal noise regulations that apply to this Project.

Bon Homme County has adopted a zoning ordinance that pertains to large wind energy systems (LWES). The ordinance limits "noise levels produced by the LWES to 45 dBA, average A-weighted sound pressure at the perimeter of occupied residences existing at the time the permit application is filed, unless a signed waiver or easement is obtained from the owner of the residence." Charles Mix County is zoned at the township level and, because no turbines are sited in organized townships, there are no zoning requirements for the Project within Charles Mix County. Hutchinson County has no numeric noise ordinance.

In addition to the identified Bon Homme County ordinance, the SDPUC requires, "the Project, exclusive of all unrelated background noise, shall not generate a long-term sound pressure level (L_{10}), as measured over a period of at least two weeks, defined by commission staff, that includes all integer wind speeds from cut in to full power, of more than 40 dBA within 25 feet of any non-participating residence unless the owner of the residence has signed a waiver, and 45 dBA of any participating residence unless the owner of the residence has signed a waiver." Therefore, the design criteria for the Project is 40 dBA at any non-participating residence and 45 dBA at any participating residence.

4.0 AMBIENT SOUND SURVEY

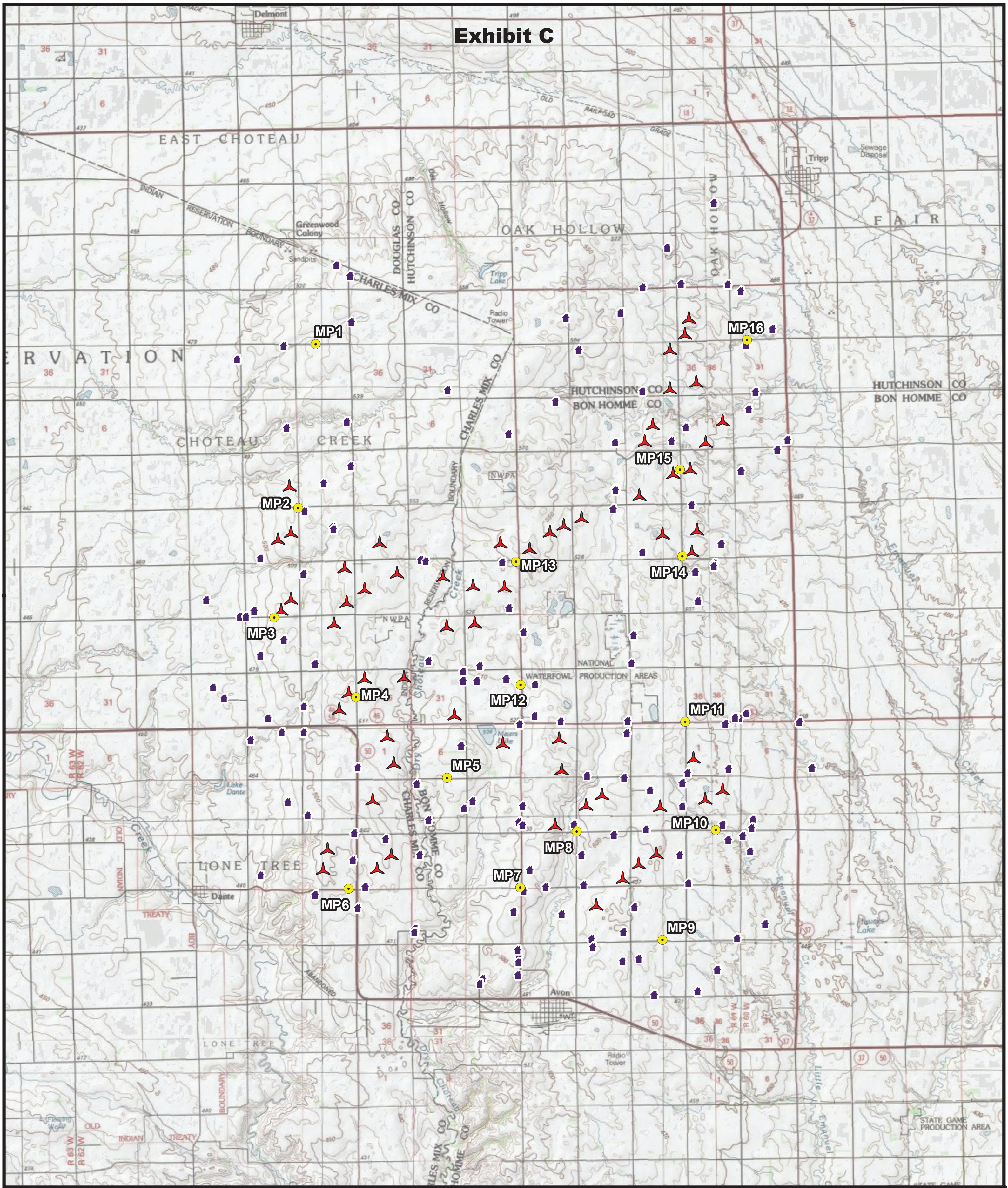
Burns & McDonnell personnel conducted an ambient sound survey of surrounding Project areas on March 12 and 13, 2018.

Measurements were taken using American National Standards Institute (ANSI) S1.4 type 1 sound level meters (Larson David Model 831). The sound level meters were calibrated at the beginning and end of each set of measurements. None of the calibration level changes exceeded ± 0.5 dB. Windscreens were used at all times on the microphone, and the meters were mounted on tripods. Certificates of calibration for the equipment used are available upon request. The microphones were located approximately 5 feet above ground level with the microphones directed towards the closest proposed wind turbine location and angled per the manufacturer's recommendation. All measurements were taken when meteorological conditions were favorable for conducting ambient sound measurements, per ANSI standards (low wind, moderate temperatures, humidity, and no precipitation).

Ambient far-field measurements were made at 16 locations, labeled measurement point (MP) MP1 through MP16, as shown in Figure 4-1. The measurement points were selected because they were accessible and representative of existing ambient sound levels in the vicinity of noise-sensitive receivers.

The far-field sound level measurements were 5 minutes in duration, and measured values were logged by the sound meter at each measurement point. The sound levels varied at each measurement point due to the extraneous sounds that occurred during the respective measurement. The overall A-weighted L_{eq} and L_{90} sound levels collected during the ambient far-field measurements are shown below in Table 4-1. Sound levels measured were in the range of 21.5 dBA to 45.0 dBA L_{90}.

Exhibit C



LEGEND

- Wind Turbine
- Receptor
- Measurement Points

REFERENCE

0 1.5 3
MILES

0 1.5 3
KILOMETERS

N

Figure 4-1
PREVAILING WIND PARK
Ambient Measurement Locations

LOCATION:	Charles Mix/Bonne Homme/Hutchinson Cty, SD
CLIENT:	Prevailing Wind Park, LLC
PROJ. NO.:	105644
CREATED:	03/19/2019

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Path: Z:\Clients\BTS\SPowerDC\105644_PrvWindStudies\Studies\Permitting\Modeling\Noise\GIS\Figure 4-1 - Far-Field Measurement Locations V7x.mxd • Coordinate System: NAD 1983 UTM Zone 14N • Units: Meter

Table 4-1: Ambient Measurements Data

Measurement Location	Sound Pressure Level (dBA)					
	Ambient (5:00 PM on 03/12/18)		Ambient (12:00 AM on 03/13/18)		Ambient (10:00 AM on 03/13/18)	
	L_{eq}	L_{90}	L_{eq}	L_{90}	L_{eq}	L_{90}
MP1	34.6	26.0	40.4	30.0	35.2	25.1
MP2	36.5	29.6	35.7	28.6	39.0	30.2
MP3	37.7	29.2	32.6	22.3	41.0	28.0
MP4	39.6	29.1	33.7	24.3	35.0	28.9
MP5	36.9	28.0	34.6	22.6	35.4	25.4
MP6	47.9	33.4	34.7	26.3	40.0	31.8
MP7	38.3	31.0	30.2	24.0	42.6	37.7
MP8	34.8	28.4	28.6	22.7	47.7	27.9
MP9	35.7	27.0	35.3	29.5	33.2	24.4
MP10	37.4	30.6	39.4	35.2	35.0	27.1
MP11	62.7	45.0	35.6	31.6	69.1	28.1
MP12	39.5	32.6	37.1	21.5	40.6	29.4
MP13	36.3	27.1	38.9	32.1	59.5	28.4
MP14	35.7	28.8	34.1	27.4	35.1	28.9
MP15	33.8	28.4	35.7	28.7	35.0	29.3
MP16	49.8	36.9	39.0	29.8	35.0	28.8

Extraneous sounds during the measurement periods included high speed traffic, birds, wind noise, and farm equipment. The measured sound levels and noise sources are presented in Appendix A.

5.0 SOUND MODELING

5.1 Wind Turbine and Transformer Sound Characteristics

The sound commonly associated with a wind turbine is described as a rhythmic "whoosh" caused by aerodynamic processes. This sound is created as air flow interacts with the surface of rotor blades. As air flows over the rotor blade, turbulent eddies form in the surface boundary layer and wake of the blade. These eddies are where most of the "whooshing" sound is formed. Additional sound is generated from vortex shedding produced by the tip of the rotor blade. Air flowing past the rotor tip creates alternating low-pressure vortices on the downstream side of the tip, causing sound generation to occur. Older wind turbines, built with rotors which operate downwind of the tower (downwind turbines), often have higher aerodynamic impulse sound levels. This is caused by the interaction between the aerodynamic lift created on the rotor blades and the turbulent wake vortices produced by the tower. Modern wind turbine rotors are mostly built to operate upwind of the tower (upwind turbines). Upwind wind turbines are not impacted by wake vortices generated by the tower and, therefore, overall sound levels can be as much as 10 dBA less. The rhythmic fluctuations of the overall sound level are less perceivable the farther one gets from the turbine. Additionally, multiple turbines operating at the same time will create the whooshing sound at different times. These non-synchronized sounds will blend together to create a more constant sound to an observer at most distances from the turbines. Another phenomenon that reduces perceivable noise from turbines is the wind itself. Higher wind speed produces noise in itself that tends to mask (or drown out) the sounds created by wind turbines.

Advancement in wind turbine technology has reduced pure tonal emissions of modern wind turbines. Manufacturers have reduced distinct tonal sounds by reshaping turbine blades and adjusting the angle at which air contacts the blade. Pitching technology allows the angle of the blade to adjust when the maximum rotational speed is achieved, which allows the turbine to maintain a constant rotational velocity. Therefore, sound emission levels remain constant as the velocity remains the same.

Wind turbines can create noise in other ways as well. Wind turbines have a nacelle where the mechanical portions of the turbine are housed. The current generation of wind turbines uses multiple techniques to reduce the noise from this portion of the turbine: vibration isolating mounts, special gears, and acoustic insulation. In general, all moving parts and the housing of the current generation wind turbines have been designed to minimize the noise they generate.

5.2 Model Inputs and Settings

Predicted sound levels were modeled using industry-accepted sound modeling software. The program used to model the turbines was the CadnaA, Version 2019, published by DataKustik, Ltd., Munich, Germany. The CadnaA program is a scaled, three-dimensional program that accounts for air absorption, terrain, ground absorption, and ground reflection for each piece of noise-emitting equipment and predicts downwind sound pressure levels. The model calculates sound propagation based on International Organization for Standardization (ISO) 9613-2:1996, General Method of Calculation. ISO 9613, and therefore CadnaA, assesses the sound pressure levels based on the Octave Band Center Frequency range from 31.5 to 8,000 Hz. Compliance with the regulations for all turbines operating should equate to compliance for any combination of the turbines operating.

5.2.1 Project Layout

Prevailing Wind's hypothetical layout contains 62 wind turbine sites, including alternatives. Predictive modeling was conducted to determine the impacts at the occupied residences shown in the Project layout figure included in Appendix B. The coordinates of each turbine location are also included in Appendix B.

It is noted that Revision 7 of the Study includes three (3) wind turbine movements relative to the previous Revision 6: turbine 4B.52 moved approximately 248 feet to the south; turbine 4B.53 moved approximately 248 feet to the north; and turbine 4B.54 moved approximately 248 feet to the south-southeast. No other turbines were moved from the previous revision.

5.2.2 Terrain and Vegetation

Terrain and attenuation from ground absorption can have a significant impact on sound transmission. U.S. Geological Survey (USGS) Digital Elevation Model (DEM) contours were imported into the model to account for topographic variations around the Project. The contours were overlaid onto high resolution, digital orthoimagery obtained from the U.S. Department of Agriculture (USDA). The terrain around the proposed Project is mostly rural with few minor changes in elevation. The land is primarily used for agricultural purposes. As such, vegetation is mostly low-lying with some small areas of trees. Therefore, vegetation was excluded from the analysis to maintain conservativeness in the model. Ground attenuation is expected to be fairly high, due to the "soft ground" of the surrounding areas; however, a conservative value was used in the model.

5.2.3 Sound Propagation and Directivity

CadnaA calculates downwind sound propagation using ISO 9613 standards, which use omnidirectional downwind sound propagation and worst-case directivity factors. In other words, the model assumes that each turbine propagates its maximum sound level in all directions at all times. While this may seem to over-predict upwind sound levels, this approach has been validated by field measurements. Under most normal circumstances, wind turbine noise is not significantly directional, but tends to radiate uniformly in all directions.

5.2.4 Atmospheric Conditions

Atmospheric conditions were based on program defaults. Layers in the atmosphere often form where temperature increases with height (temperature inversions). Sound waves can reflect off of the temperature inversion layer and return to the surface of the earth. This process can increase sound levels at the surface, especially if the height of the inversion begins near the surface of the earth. Temperature inversions tend to occur mainly at night when winds are light or calm, usually when wind turbines are not operating. CadnaA calculates the downwind sound in a manner which is favorable for propagation (worst-case scenario) by assuming a well-developed moderate ground-based temperature inversion such as can occur at night. Therefore, predicted sound level results tend to be higher than would actually occur.

The atmosphere does not flow smoothly and tends to have swirls and eddies, also known as turbulence. Turbulence is basically formed by two processes: thermal turbulence and mechanical turbulence. Thermal turbulence is caused by the interaction of heated air rapidly rising from the heated earth's surface, with cooler air descending from the atmosphere. Mechanical turbulence is caused as moving air interacts with objects such as trees, buildings, and wind turbines. Turbulent eddies generated by wind turbines and other objects can cause sound waves to scatter, which in turn, provides sound attenuation between the wind turbine and the receiver. The acoustical model assumes laminar air flow, which minimizes sound attenuation that would occur in a realistic inhomogeneous atmosphere. This assumption also causes the predicted sound levels to be higher than would actually occur.

5.2.5 Sound Emission Data

Acoustical modeling was conducted for the entire Project. Wind turbine heights and acoustical emissions were input into the model. The expected worst-case sound power levels for the GE 3.8-137 turbines were contained in documents provided by GE and were based on various wind speeds. The sound emissions data supplied was developed using the International Electrotechnical Commission 61400-11 acoustic measurement standards. The expected sound power level and modeled heights for the turbines are displayed in Table 5-1. The Project also contains one substation step-up transformer. The estimated transformer overall sound power level is provided in Table 5-1.

Table 5-1: Wind Turbine and Substation Transformer Sound Power Levels

Source/ Turbine	Height (m)	Sound Power Level (dBA)									
		31.5	63	125	250	500	1000	2000	4000	8000	A-wt.[a]
GE 3.8-137	111.5	78.5	86.8	92.6	96.4	99.4	102.1	102.0	93.7	79.2	**107.0**
Transformer[b]	3.1	-	-	-	-	-	-	-	-	-	**102.4**

(a) A-wt. = A-weighted decibels
(b) Estimated sound level based on National Electrical Manufacturers Association rating

A point source at the hub was used to model sound emissions from the wind turbines, and a point source at the transformer location was used to model sound emissions from the substation transformer. This approach is appropriate for simulating wind turbine noise emissions due to the large distances between the turbines and the receivers as compared to the dimensions of the wind turbines. The corresponding sound levels from the table above were applied to every point source.

Figure 4-1 shows the entire wind farm layout. Locations of receivers and wind turbines around the Project area were provided by the developer and are shown in Appendix B. Each receiver was assumed to have a height of 1.52 meters (5.0 feet) above ground level. Compliance with the SDPUC limit was assessed at the physical residence (each receiver).

The following assumptions were made to maintain the inherent conservativeness of the model and to estimate the worst case modeled sound levels:

- Attenuation was not included for sound propagation through wooded areas, existing barriers, and shielding
- All turbines were assumed to be operating at maximum power output (and therefore, maximum sound levels) at all times to represent worst-case noise impacts from the wind farm as a whole

5.3 Acoustical Modeling Results

Sound pressure levels were predicted for the identified receivers in the CadnaA noise modeling software using the manufacturer-specified sound power levels at each frequency and the assumptions listed above. CadnaA modeling results have been demonstrated in previous studies to conservatively approximate real-life measured noise from a source when extraneous noises are not present. For modeling purposes, it is assumed the turbines are operating at a constant maximum sound level for an extended period of time. As such, the L_{eq} and L_{10} sound levels would be equal, since the turbines are not fluctuating in sound level nor are background sounds considered in the model.

As previously mentioned, decibels are a logarithmic ratio of a sound pressure to a reference sound pressure. Therefore, they must be logarithmically added to determine a cumulative impact (i.e., logarithmically adding 50 dBA and 50 dBA results in 53 dBA). Logarithmically adding each of the individual turbine's impacts together at each receiver provides an overall Project impact at each receiver.

The maximum model-predicted L_{eq}/L_{10} sound pressure levels at each receiver (the logarithmic addition of sound levels from each frequency from every turbine) are included in Appendix C. These values represent only the constant noise emitted by the wind turbines and do not include any extraneous noises (traffic, etc.) that could be present during physical noise measurements. There are no expected exceedances of the SDPUC 40-dBA noise limit at any non-participating residence or 45-dBA noise limit at any participating residence due to operation of the proposed wind turbine locations of the Project. Extraneous sounds (grain dryers, traffic, etc.) may make the overall sound level higher than the limits in some circumstances, but the turbines alone are not expected to cause that to happen.

Appendix D contains graphical representation of the Project's impact on the surrounding area for the GE turbines. The figure depicts the sound level propagation attributable to the new turbines and substation transformer.

6.0 CONCLUSION

Burns & McDonnell conducted a predictive sound assessment study for the proposed Prevailing Wind Park. The study included identification of applicable sound regulations and predictive modeling to estimate Project-related sound levels in the surrounding community.

Sound pressure levels were predicted at occupied receivers within and surrounding the Project area using manufacturer-specified sound power levels for each wind turbine and estimated sound levels for the substation transformer. A number of conservative assumptions were applied to provide worst-case predicted sound pressure levels. Those results were then compared to the identified SDPUC noise limits at all participating and non-participating residences. There are no expected exceedances of the SDPUC noise limits due to operation of any of the proposed wind turbine locations of the Project.

Exhibit C

APPENDIX A - AMBIENT MEASUREMENT DATA

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Appendix A - Ambient Measurement Data

Prevailing Winds

Point Number	***LAeq***	***LA90***	***Notes***
03/12/18 - 5:00PM to 7:00PM			**Meter1 Calibration before: 114.11 Meter2 Calibration before: 114.05**
36°F, 60% hm, 31°F dp, 4-9mph , clear skies			**Meter1 Calibration after: 113.91 Meter2 Calibration after: 113.91**
MP1	34.6 dBA	26.0 dBA	Distant traffic, light wind, existing wind farm not audible
MP2	36.5 dBA	29.6 dBA	Distant traffic, birds, light wind, fan noise from nearby business
MP3	37.7 dBA	29.2 dBA	Birds, light wind, distant traffic including large trucks, very distant airplane
MP4	39.6 dBA	29.1 dBA	Birds, light wind, distant traffic
MP5	36.9 dBA	28.0 dBA	Highway traffic, birds
MP6	47.9 dBA	33.4 dBA	Highway traffic dominant, paused for local traffic
MP7	38.3 dBA	31.0 dBA	Highway traffic, birds
MP8	34.8 dBA	28.4 dBA	Birds, distant high speed traffic
MP9	35.7 dBA	27.0 dBA	Nearby high speed traffic (409th Street), birds
MP10	37.4 dBA	30.6 dBA	Distant high speed traffic, birds, horns
MP11	62.7 dBA	45.0 dBA	Birds dominant, two high speed car passbys
MP12	39.5 dBA	32.6 dBA	Birds, farm equipment, slight wind
MP13	36.3 dBA	27.1 dBA	Slight wind
MP14	35.7 dBA	28.8 dBA	Slight wind, distant high speed traffic
MP15	33.8 dBA	28.4 dBA	Slight wind, distant birds, distant high speed traffic, backup alarm
MP16	49.8 dBA	36.9 dBA	Birds dominant, slight wind

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Appendix A - Ambient Measurement Data

Prevailing Winds

Point Number	*LAeq*	*LA90*	*Notes*	
03/13/18 - 12:00AM to 2:00AM			**Meter1 Calibration before: 114.19**	**Meter2 Calibration before: 113.87**
29°F, 74% hm, 21°F dp, 6-9 mph , clear skies			**Meter1 Calibration after: 113.83**	**Meter2 Calibration after: 114.20**
MP1	40.4 dBA	30.0 dBA	Wind turbines audible, light winds	
MP2	35.7 dBA	28.6 dBA	Wind turbines audible, light winds, sheep noise	
MP3	32.6 dBA	22.3 dBA	Very quiet, faint traffic	
MP4	33.7 dBA	24.3 dBA	Very quiet, faint traffic	
MP5	34.6 dBA	22.6 dBA	Distant traffic, large trucks, bull snort	
MP6	34.7 dBA	26.3 dBA	Traffic	
MP7	30.2 dBA	24.0 dBA	Traffic	
MP8	28.6 dBA	22.7 dBA	Distant high speed traffic	
MP9	35.3 dBA	29.5 dBA	Distant high speed traffic	
MP10	39.4 dBA	35.2 dBA	Slight wind	
MP11	35.6 dBA	31.6 dBA	Slight wind	
MP12	37.1 dBA	21.5 dBA	Distant high speed traffic	
MP13	38.9 dBA	32.1 dBA	Slight wind	
MP14	34.1 dBA	27.4 dBA	Slight wind	
MP15	35.7 dBA	28.7 dBA	Slight wind, distant high speed traffic	
MP16	39.0 dBA	29.8 dBA	Distant high speed traffic	

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Appendix A - Ambient Measurement Data

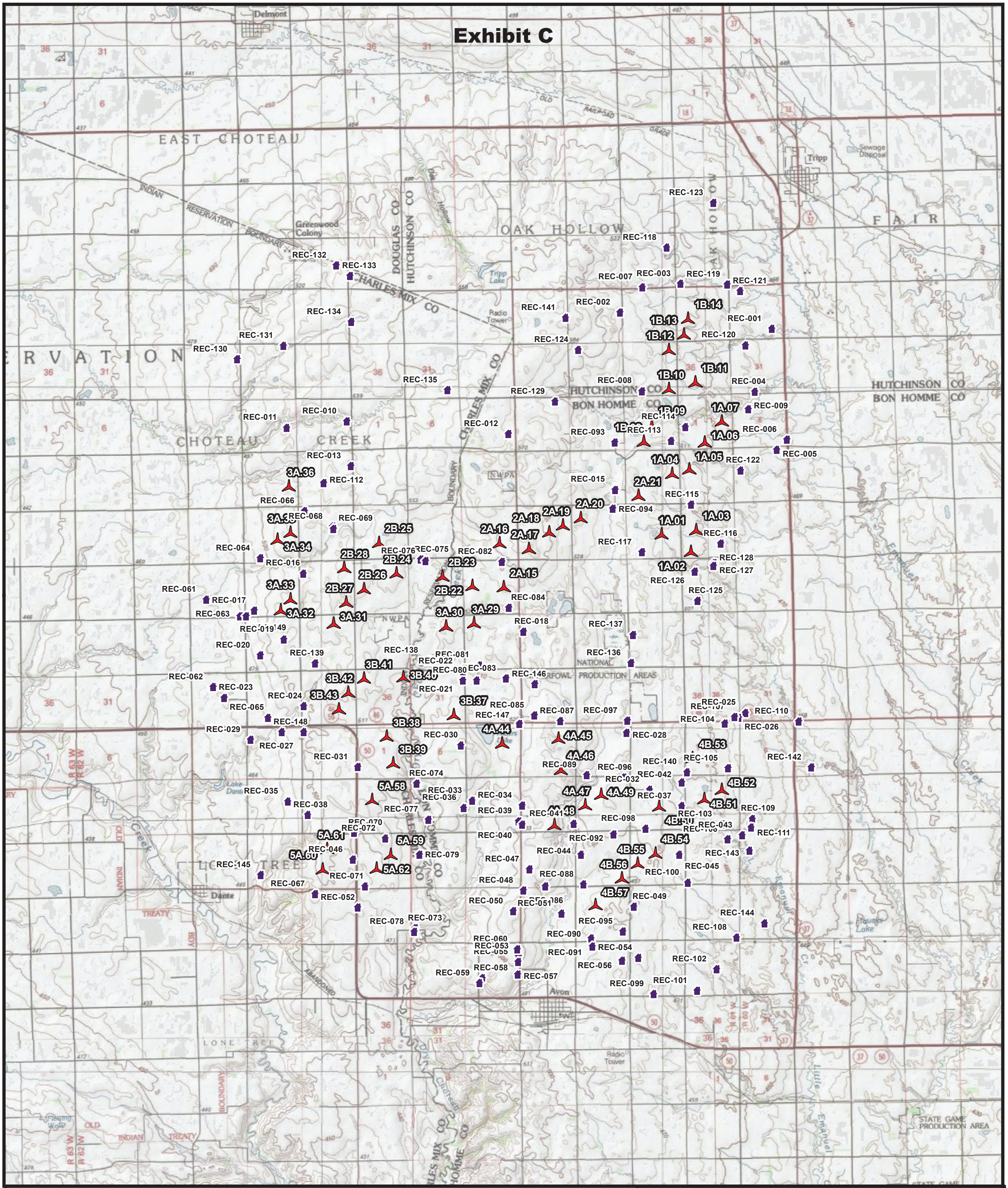
Prevailing Winds

Point Number	*LAeq*	*LA90*	*Notes*	
03/13/18 - 10:00AM to 12:00PM			**Meter1 Calibration before: 114.24**	**Meter2 Calibration before: 114.04**
30°F, 62% hm, 19°F dp, 3-4 mph , clear skies			**Meter1 Calibration after: 113.82**	**Meter2 Calibration after: 113.97**
MP1	35.2 dBA	25.1 dBA	Distant traffic, distant plane, wind turbines barely audible	
MP2	39.0 dBA	30.2 dBA	Birds, wind turbines barely audible, tractor distant loading/unloading Birds,	
MP3	41.0 dBA	28.0 dBA	distant traffic, wind	
MP4	35.0 dBA	28.9 dBA	Birds, distant traffic, wind, distant airplane	
MP5	35.4 dBA	25.4 dBA	Birds, wind, distant traffic	
MP6	40.0 dBA	31.8 dBA	Birds, highway traffic	
MP7	42.6 dBA	37.7 dBA	Birds, distant traffic, paused for local traffic	
MP8	47.7 dBA	27.9 dBA	Owl, birds, distant high speed traffic, woman speaking (very end) Birds	
MP9	33.2 dBA	24.4 dBA	Birds, dog barking, distant high speed traffic	
MP10	35.0 dBA	27.1 dBA	High speed car passing	
MP11	69.1 dBA	28.1 dBA	Farm equipment, cows	
MP12	40.6 dBA	29.4 dBA	Birds, one car passing	
MP13	59.5 dBA	28.4 dBA	Distant constant high speed traffic, birds	
MP14	35.1 dBA	28.9 dBA	Birds, distant high speed traffic	
MP15	35.0 dBA	29.3 dBA	Distant birds, distant high speed traffic	
MP16	35.0 dBA	28.8 dBA		

Exhibit C

APPENDIX B - SITE LAYOUT AND TURBINE LOCATIONS

Exhibit C



LEGEND

- Wind Turbine
- Receptor

REFERENCE

0 — 1.5 — 3 MILES

0 — 1.5 — 3 KILOMETERS

N

LOCATION:	Charles Mix/Bonne Homme/Hutchinson Cty, SD
CLIENT:	Prevailing Wind Park, LLC
PROJ. NO.:	105644
CREATED:	03/29/2019

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Path: Z:\Clients\BTS\SPowerDC\105644_PrvWindStudies\Studies\Permitting\Modeling\Noise\GIS\Figure B-1 - Project Layout V7x.mxd • Coordinate System: NAD 1983 UTM Zone 14N • Units: Meter

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Appendix B - Turbine Locations

GE 3.8-137, 111.5 m

Tubine Number (Construction)	*Tubine Number (Other)*	*Coordinates* Easting (m)	Northing (m)
1A.01	21	579956	4775946
1A.02	33	580807	4775443
1A.03	54	580970	4776074
1A.04	36	580259	4777725
1A.05	50	580759	4777855
1A.06	46	581221	4778640
1A.07	47	581719	4779255
1B.08	18	579428	4778668
1B.09	20	579671	4779153
1B.10	25	580170	4780211
1B.11	51	580939	4780407
1B.12	30	580170	4781359
1B.13	56	580604	4781811
1B.14	55	580727	4782275
2A.15	5	575324	4774400
2A.16	3	575201	4775693
2A.17	1	576064	4775521
2A.18	2	576650	4776014
2A.19	6	577060	4776210
2A.20	4	577580	4776426
2A.21	13	579275	4777079
2B.22	7	574404	4774437
2B.23	12	573519	4774711
2B.24	9	572179	4774804
2B.25	8	571662	4775700
2B.26	15	571219	4774346
2B.27	22	570700	4773949
2B.28	16	570639	4774959
3A.29	17	574452	4773338
3A.30	29	573634	4773249
3A.31	23	570336	4773327
3A.32	48	568781	4773724
3A.33	57	569071	4774045
3A.34	40	568691	4775793
3A.35	32	569074	4775995
3A.36	26	569026	4777349
3B.37	24	573856	4770651
3B.38	41	571896	4770015
3B.39	45	572076	4769232
3B.40	37	572380	4771753

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Appendix B - Turbine Locations

GE 3.8-137, 111.5 m

Tubine Number (Construction)	*Tubine Number (Other)*	*Coordinates*	
		Easting (m)	*Northing (m)*
3B.41	39	571220	4771721
3B.42	58	570763	4771308
3B.43	49	570487	4770821
4A.44	28	575275	4769819
4A.45	10	576925	4769963
4A.46	11	576997	4769043
4A.47	34	577718	4768001
4A.48	14	576805	4767428
4A.49	31	578173	4768318
4B.50	27	579886	4767974
4B.51	52	581200	4768190
4B.52	53	581716	4768461
4B.53	35	580861	4769386
4B.54	42	579772	4766595
4B.55	44	579255	4766296
4B.56	43	578787	4765862
4B.57	38	578011	4765079
5A.58	60	571464	4768160
5A.59	61	572004	4766553
5A.60	62	570006	4766129
5A.61	63	570143	4766716
5A.62	64	571597	4766151

Notes:

[1] All coordinates presented in UTM NAD83 Zone 14N (meters)

[2] All coordinates provided by Developer in "PWIND - 62x_GE38137_111p5m_v181126-02 For Noise Flicker.kml" on 3/11/2019

[3] "Turbine Number (Construction)" indicates turbine identifiers expected to be used during Project construction

[4] "Turbine Number (Other)" indicates turbine numbers identified on Exhibit A14-2 (Revised Layout) and I29 Attachment 4-2

Exhibit C

APPENDIX C - MODELING RESULTS

Exhibit C

Appendix C - Modeling Results

GE 3.8-137, 111.5 m

Receiver	Status	Coordinates Easting (m)	Coordinates Northing (m)	Base Elevation (m)	Modeled LAeq	Limit Value	Exceed? (Y/N)
REC-001	Non-participating	583178.93	4781949.36	473.94	24.7	40	N
REC-002	Participating	578731.00	4782428.97	540.99	29.1	45	N
REC-003	Non-participating	580506.89	4783273.92	505.27	33.7	40	N
REC-004	Non-participating	582678.66	4780104.52	480.03	32.4	40	N
REC-005	Non-participating	583326.78	4778396.84	476.81	27.5	40	N
REC-006	Non-participating	583615.28	4778695.43	471.94	26.2	40	N
REC-007	Non-participating	579386.45	4783171.84	519.65	29.7	40	N
REC-008	Non-participating	579364.54	4780122.78	515.18	38.2	40	N
REC-009	Non-participating	582485.70	4779597.03	481.47	35.1	40	N
REC-010	Non-participating	570706.40	4779232.69	531.85	20.3	40	N
REC-011	Non-participating	568954.92	4779049.93	516.88	23.1	40	N
REC-012	Non-participating	575450.96	4778869.67	571.47	-	40	N
REC-013	Non-participating	570834.43	4777923.92	539.22	27.4	40	N
REC-014	Non-participating	578568.31	4777265.47	526.35	38.1	40	N
REC-015	Non-participating	578578.94	4777228.45	526.13	38.3	40	N
REC-016	Participating	569437.95	4774776.35	523.53	38.9	45	N
REC-017	Non-participating	567999.72	4773683.50	489.60	36.8	40	N
REC-018	Participating	575893.85	4773069.05	525.25	32.7	45	N
REC-019	Participating	568870.35	4772837.61	510.51	36.3	45	N
REC-020	Non-participating	568170.58	4772373.09	491.63	30.5	40	N
REC-021	Participating	574122.73	4771641.66	507.46	34.9	45	N
REC-022	Non-participating	574117.98	4771913.43	508.31	34.5	40	N
REC-023	Non-participating	567115.19	4771132.04	470.89	-	40	N
REC-024	Non-participating	569455.79	4770885.60	499.55	34.2	40	N
REC-025	Participating	582409.59	4770691.28	486.10	26.3	45	N
REC-026	Non-participating	582205.90	4770538.43	489.18	27.7	40	N
REC-027	Non-participating	569450.78	4770122.57	499.25	32.0	40	N
REC-028	Participating	578915.96	4770106.59	519.65	30.6	45	N
REC-029	Non-participating	567890.47	4769896.98	472.42	19.1	40	N
REC-030	Non-participating	574057.84	4769738.20	530.58	35.4	40	N
REC-031	Non-participating	571038.40	4769099.63	510.51	36.6	40	N
REC-032	Participating	579594.58	4768433.69	507.46	40.2	45	N
REC-033	Non-participating	574388.42	4768112.11	502.26	28.9	40	N
REC-034	Non-participating	575856.91	4767968.51	509.35	34.0	40	N
REC-035	Non-participating	568988.11	4768088.17	487.50	27.6	40	N
REC-036	Non-participating	574139.54	4767903.27	507.06	28.0	40	N
REC-037	Participating	580534.75	4767955.77	497.42	40.6	45	N
REC-038	Non-participating	569570.52	4767693.73	493.87	33.1	40	N
REC-039	Non-participating	575753.59	4767511.52	511.25	33.3	40	N
REC-040	Non-participating	575853.92	4767408.85	513.56	34.2	40	N
REC-041	Participating	577365.54	4767429.45	496.85	41.4	45	N
REC-042	Non-participating	580534.93	4768649.62	501.93	39.6	40	N
REC-043	Non-participating	582314.18	4767105.01	476.98	31.0	40	N
REC-044	Participating	577581.91	4766535.38	501.37	35.6	45	N
REC-045	Participating	580459.53	4766528.35	495.27	38.2	45	N
REC-046	Participating	570892.00	4766384.10	500.34	39.9	45	N
REC-047	Non-participating	576071.91	4766099.10	511.58	28.5	40	N
REC-048	Non-participating	575888.47	4765484.03	507.46	26.2	40	N
REC-049	Non-participating	579136.06	4765003.57	501.37	36.3	40	N
REC-050	Participating	575594.26	4764877.78	513.56	22.9	45	N
REC-051	Participating	577014.96	4764806.12	483.08	32.7	45	N
REC-052	Non-participating	571034.71	4764976.49	483.08	32.4	40	N
REC-053	Non-participating	575751.76	4763553.72	504.89	18.1	40	N
REC-054	Non-participating	579261.02	4763508.83	493.92	26.2	40	N
REC-055	Non-participating	575738.19	4763383.18	501.37	18.7	40	N
REC-056	Non-participating	578784.40	4763423.45	495.27	26.7	40	N
REC-057	Non-participating	575728.70	4763020.56	496.19	-	40	N
REC-058	Non-participating	574689.98	4762905.51	489.18	-	40	N
REC-059	Non-participating	574608.88	4762765.31	484.23	-	40	N
REC-060	Non-participating	575719.36	4763758.78	507.46	19.6	40	N
REC-061	Non-participating	566590.17	4774005.26	470.89	25.5	40	N
REC-062	Non-participating	566794.52	4771446.01	467.84	-	40	N
REC-063	Non-participating	567575.59	4773523.26	480.49	32.1	40	N
REC-064	Non-participating	568169.85	4775221.75	493.83	37.4	40	N

Appendix C - Modeling Results

GE 3.8-137, 111.5 m

Receiver	Status	Coordinates Easting (m)	Coordinates Northing (m)	Base Elevation (m)	Modeled LAeq	Limit Value	Exceed? (Y/N)
REC-065	Non-participating	568402.45	4770548.21	483.08	24.8	40	N
REC-066	Participating	569474.73	4776605.15	525.75	39.0	45	N
REC-067	Non-participating	569782.41	4765373.88	493.98	36.0	40	N
REC-068	Non-participating	570301.18	4776152.11	533.82	35.8	40	N
REC-069	Non-participating	570320.63	4776086.07	530.62	36.0	40	N
REC-070	Non-participating	570930.65	4767169.47	502.79	37.7	40	N
REC-071	Non-participating	571246.87	4765598.42	488.81	38.5	40	N
REC-072	Participating	571847.73	4767001.23	507.46	41.7	45	N
REC-073	Non-participating	572712.41	4764371.30	476.98	25.2	40	N
REC-074	Non-participating	572760.45	4768609.65	494.96	35.3	40	N
REC-075	Participating	572875.14	4775183.93	528.80	39.1	45	N
REC-076	Non-participating	573023.77	4775137.74	528.80	39.6	40	N
REC-077	Non-participating	573104.39	4767558.79	488.61	31.1	40	N
REC-078	Non-participating	572689.83	4764269.58	472.84	24.7	40	N
REC-079	Participating	572840.24	4766532.05	483.08	35.8	45	N
REC-080	Participating	574527.24	4771635.20	508.86	33.7	45	N
REC-081	Participating	574606.23	4772084.46	513.56	33.9	45	N
REC-082	Participating	575265.41	4775117.32	552.59	41.9	45	N
REC-083	Participating	575384.42	4771695.61	513.56	34.9	45	N
REC-084	Participating	575459.57	4773771.95	533.47	39.3	45	N
REC-085	Participating	576210.31	4770611.18	524.57	35.2	45	N
REC-086	Participating	576537.52	4765598.06	498.89	30.2	45	N
REC-087	Participating	576971.43	4770447.24	531.85	40.6	45	N
REC-088	Participating	577659.69	4765661.22	489.18	38.1	45	N
REC-089	Participating	577747.37	4768859.92	513.80	40.5	45	N
REC-090	Non-participating	577878.24	4764078.53	490.80	32.8	40	N
REC-091	Non-participating	577915.85	4763844.06	489.18	30.5	40	N
REC-092	Participating	578531.67	4767119.28	501.56	37.6	45	N
REC-093	Participating	578575.67	4778618.52	525.75	36.7	45	N
REC-094	Participating	578514.65	4776677.36	519.65	37.9	45	N
REC-095	Non-participating	578804.05	4764274.93	501.37	32.8	40	N
REC-096	Non-participating	578827.98	4768793.31	520.74	37.4	40	N
REC-097	Non-participating	578943.49	4770454.51	519.65	29.0	40	N
REC-098	Non-participating	579475.34	4767289.07	507.32	39.8	40	N
REC-099	Participating	579720.64	4762441.83	480.38	-	45	N
REC-100	Non-participating	580720.17	4765706.10	489.18	32.6	40	N
REC-101	Non-participating	580991.94	4762540.89	476.98	-	40	N
REC-102	Non-participating	581560.41	4763175.20	470.14	-	40	N
REC-103	Participating	581721.12	4767420.32	484.05	36.1	45	N
REC-104	Non-participating	581794.35	4770381.50	494.21	30.3	40	N
REC-105	Non-participating	581890.50	4769063.10	495.27	39.1	40	N
REC-106	Participating	581882.94	4766984.50	478.66	32.3	45	N
REC-107	Non-participating	582089.90	4770568.08	488.75	28.0	40	N
REC-108	Participating	582148.44	4764102.27	470.89	-	45	N
REC-109	Non-participating	582609.65	4767582.94	483.08	31.8	40	N
REC-110	Non-participating	583963.39	4770430.23	460.42	17.9	40	N
REC-111	Non-participating	582577.80	4767332.36	480.99	30.9	40	N
REC-112	Non-participating	570034.28	4777428.88	531.85	33.7	40	N
REC-113	Participating	580225.65	4778670.25	516.61	41.3	45	N
REC-114	Participating	580643.69	4779065.86	510.51	40.5	45	N
REC-115	Participating	580812.98	4776797.89	507.54	39.5	45	N
REC-116	Participating	581676.22	4775653.66	495.49	37.4	45	N
REC-117	Participating	579367.75	4775404.23	525.75	36.8	45	N
REC-118	Non-participating	580095.28	4784336.60	507.46	25.3	40	N
REC-119	Non-participating	581867.73	4783246.46	489.52	29.7	40	N
REC-120	Non-participating	582410.57	4781467.20	486.13	30.9	40	N
REC-121	Non-participating	582256.16	4783054.99	483.20	28.4	40	N
REC-122	Participating	582261.38	4777793.15	487.45	33.8	45	N
REC-123	Non-participating	581460.71	4785645.95	483.97	-	40	N
REC-124	Non-participating	577505.30	4781336.06	557.16	19.3	40	N
REC-125	Non-participating	580995.88	4773976.31	501.99	29.4	40	N
REC-126	Participating	580915.69	4774830.29	502.29	38.6	45	N
REC-127	Participating	581473.61	4775075.61	495.27	37.0	45	N
REC-128	Participating	581468.21	4774997.26	495.27	36.4	45	N

Appendix C - Modeling Results

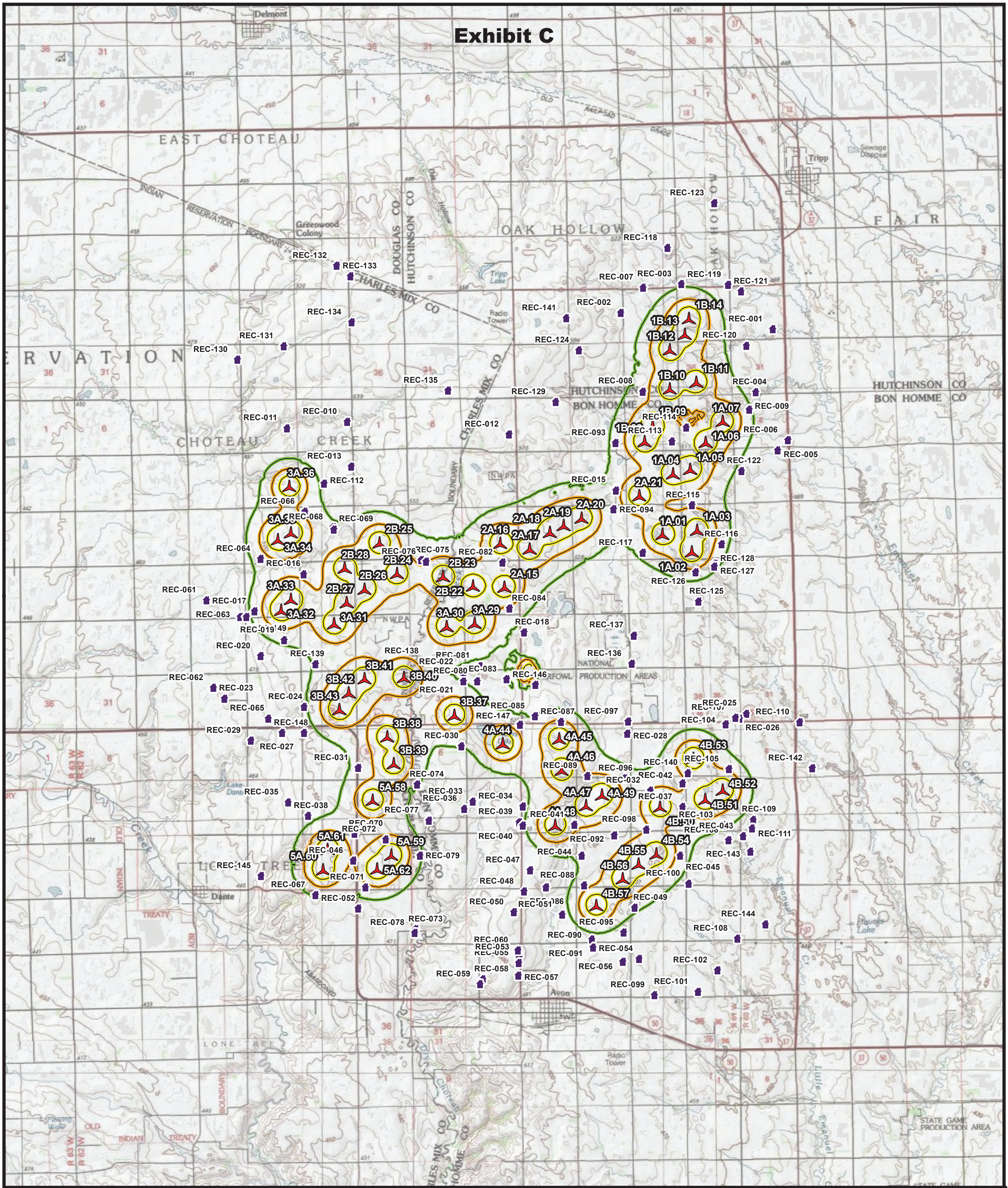
GE 3.8-137, 111.5 m

Receiver	Status	Coordinates Easting (m)	Northing (m)	Base Elevation (m)	Modeled LAeq	Limit Value	Exceed? (Y/N)
REC-129	Non-participating	576815.58	4779814.18	556.23	21.4	40	N
REC-130	Non-participating	567502.00	4781060.00	502.37	-	40	N
REC-131	Non-participating	568850.00	4781446.00	523.04	-	40	N
REC-132	Non-participating	570408.00	4783811.00	527.44	-	40	N
REC-133	Non-participating	570806.00	4783497.00	538.25	-	40	N
REC-134	Non-participating	570845.00	4782153.00	543.29	-	40	N
REC-135	Non-participating	573665.00	4780153.00	564.37	-	40	N
REC-136	Non-participating	579049.00	4772150.00	519.65	11.1	40	N
REC-137	Non-participating	579104.00	4772978.00	519.65	17.9	40	N
REC-138	Participating	573105.45	4772224.12	513.56	37.1	45	N
REC-139	Non-participating	569781.24	4772133.60	510.51	35.5	40	N
REC-140	Cemetery	580689.30	4768952.27	507.46	41.9	45	N
REC-141	Non-participating	577129.69	4782270.05	574.52	-	40	N
REC-142	Non-participating	584339.55	4769092.88	460.78	19.3	40	N
REC-143	Non-participating	582521.68	4766643.44	470.89	27.6	40	N
REC-144	Non-participating	582964.12	4764513.68	462.13	-	40	N
REC-145	Non-participating	568186.44	4765929.46	457.18	26.7	40	N
REC-146	Participating	576220.57	4771526.69	525.75	34.4	45	N
REC-147	Participating	575778.28	4770360.98	519.65	37.3	45	N
REC-148	Non-participating	568806.39	4770128.32	487.99	27.0	40	N
REC-149	Non-participating	567762.65	4773526.07	484.31	33.8	40	N
REC-150	Cemetery	580103.67	4778313.74	519.33	42.2	45	N
REC-151	Cemetery	580517.96	4778645.61	510.57	41.3	45	N
REC-152	Cemetery	570875.38	4779853.57	541.88	-	45	N
REC-153	Cemetery	567543.25	4779387.97	500.63	20.3	45	N

"-" represents no expected impacts at the receiver location

APPENDIX D - SOUND LEVEL CONTOURS

Exhibit C



LEGEND

- Wind Turbine
- Receptor
- 35 dBA Contour
- 40 dBA Contour
- 45 dBA Contour

REFERENCE

0 1.5 3
MILES

0 1.5 3
KILOMETERS

N

LOCATION:	Charles Mix/Bonne Homme/Hutchinson Cty, SD
CLIENT:	Prevailing Wind Park, LLC
PROJ. NO.:	105644
CREATED:	03/29/2019

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Path: Z:\Clients\BTS\SPowerDC\105644_PrvWindStudies\Studies\Permitting\Modeling\Noise\GIS\Figure D-1 - Sound Level Contours V7x.mxd • Coordinate System: NAD 1983 UTM Zone 14N • Units: Meter

Exhibit C

BURNS & McDONNELL

CREATE AMAZING.

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